

NASA-CR-197811

NASA

CONTINUATION OF SPACE SHUTTLE  
PROBABILISTIC RISK ASSESSMENT, PHASE 3  
SAIC DOCUMENT NO. SAICNY95-02-25

# PROBABILISTIC RISK ASSESSMENT

OF THE

SPACE SHUTTLE

A STUDY OF THE POTENTIAL OF  
LOSING THE VEHICLE

DURING NOMINAL OPERATION

VOLUME IV: SYSTEM MODELS AND DATA ANALYSIS

PREPARED FOR

US NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

HEADQUARTERS OFFICE OF SPACE FLIGHT (CODE M)

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BY

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(NASA-CR-197811) PROBABILISTIC  
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# SSME/MPIS Initiator Equivalent Flight Occurrences Evaluation

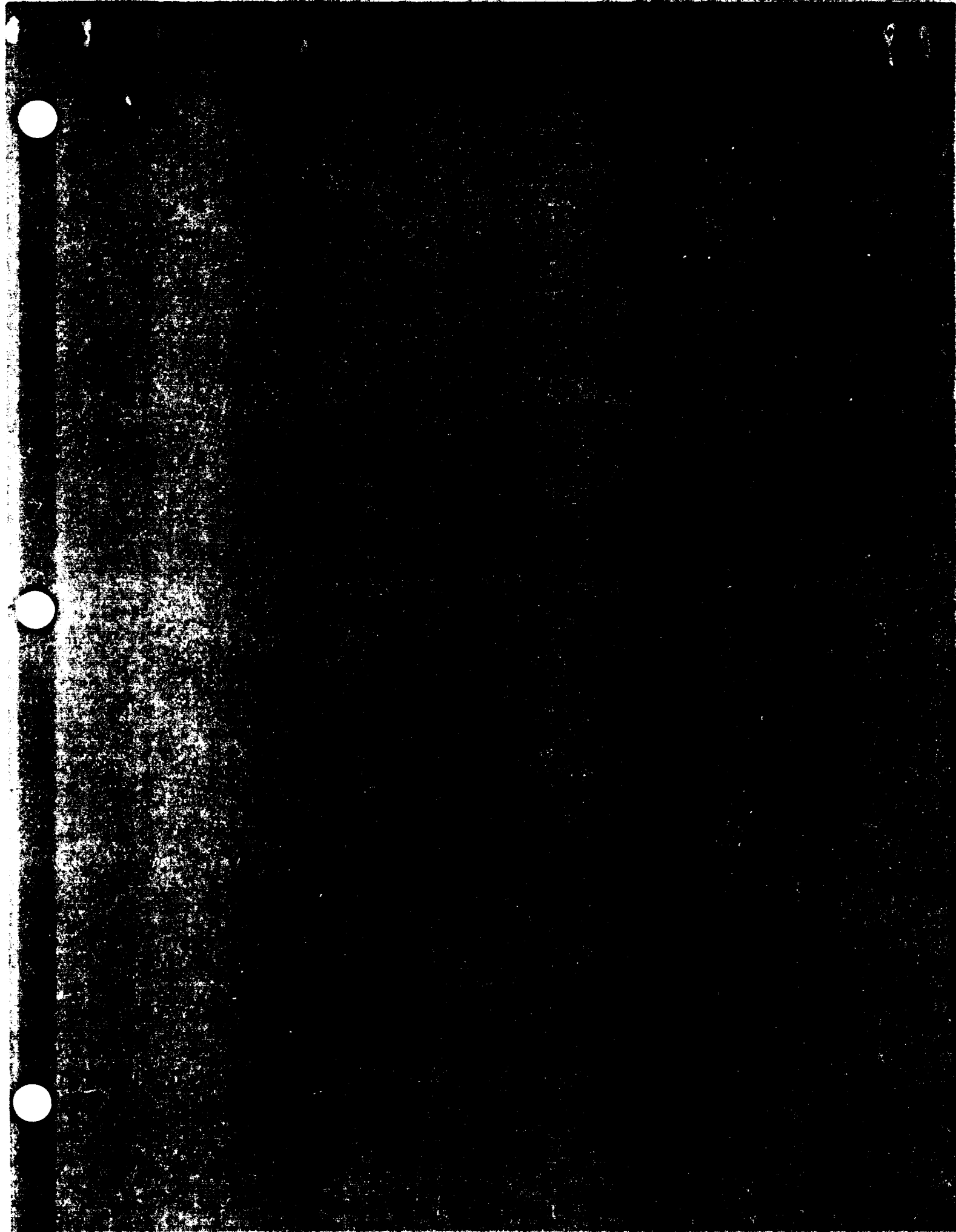
Record Type/ Source Study Initiator	Record/ Source ID	Date	System Element	Failure Description from Record	Analysis Comments	Engine #	Test/Flight	Redline Activation	Engine Configuration	Configuration Applicability	Event Priority Factor	Weighting Factor	Equivalent Flight Failure for Total Exposure Time
<b>Loss of MCC Pressure</b>													
SSMEPO													4.00
UCR	A020446	24-Jul-88	SYSTEM	CROSS FEED GAIN BAD AT HIGH VLV POSITIONS	THROTTLE DOWN IN THRUST LIMIT +200F	0211	801.578	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FPLPH2	1	1	1	
UCR	A015716	25-Jul-87	SYSTEM	HPOTP TURB TEMP EXCD RL	1500 PRELIFT OFF RL - CHANGED TO 1000	0210	750.284	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FPLPH2	1	1	1	
UCR	A016031	2-Sep-81	MINU	SEVERE EROSION OF PRIMING FACE PLATES	MINU BLURIN OUT/REPLACED MINU	0110	750.144	HPOTP TURBINE DISCHARGE TEMPERATURE	4 FPL	0.75	1	0.75	
UCR	A013786	15-Jul-81	MINU	SEVERE DAMAGED TO THE PRIMING FACE PLATES	MINU BLURIN OUT EXT DAM	2104	801.331	HPOTP TURBINE DISCHARGE TEMPERATURE	4 FPL	0.75	1	0.75	
UCR	A017544	25-Jul-80	MINU	RL CO. HPOT TURB DISC TEMP MAIN INU	SOLE IN INLETS POST FAIL	2004	802.186	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	
<b>Loss of Gross H2 Flow</b>													
SSMEPH													0.50
UCR	A011289	16-Apr-80	HPFTP	H2 FUEL TURB DISC TEMP VOTING LOGIC CO	TURBROUND MAIN COLLAPSED	2003	SF0001.8	HPFTP TURBINE DISCHARGE TEMPERATURE	2 MPFA	0.25	1	0.25	
UCR	A003243	10-Jul-78	HPFTP	EXTREME BUILDUP IN TURBROUND MANIFOLD	BULGE IN TURBINE TURB MANIFOLD	0101	802.118	HPFTP TURBINE DISCHARGE TEMPERATURE	2 MPFA	0.25	1	0.25	
<b>High Mixture Ratio in Oxidizer Preburner</b>													
SSMEPO													0.25
UCR	A018563	26-Jun-81	SYSTEM	PREMATURE CUTOFF/OPON POSITION	OPON LIMIT RESET MCF	0007	750.119		2 MPFA	0.25	1	0.25	
MSFC PRACA	A006247	17-Jun-81	HYDRAULICS	ACT CHECK-OUT MODULE FAILURE	OPON POSITION FAILURE		Field			1	0	0	
<b>High Mixture Ratio in Fuel Preburner</b>													
SSMEPH													0.25
UCR	A018563	26-Jun-81	SYSTEM	PREMATURE CUTOFF/OPON POSITION	OPON LIMIT RESET MCF	0007	750.119		2 MPFA	0.25	1	0.25	
MSFC PRACA	A006247	17-Jun-81	HYDRAULICS	ACT CHECK-OUT MODULE FAILURE	OPON POSITION FAILURE		Field			1	0	0	
<b>Loss of Fuel to Both Preburners</b>													
SSMEPH													6.25
UCR	A021548	2-Mar-88	FAM KI	H2 PREDICTION NOT PER WATER FLOW	OFF MAP-DUE TO BAD FLOWMETER CONSTANT	2107	802.465	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FPLPH2	1	1	1	
UCR	A006918	11-Dec-86	SAW KI	PREMATURE CO. USED TURB TEMP RL	INCORRECT FLOWMETER CONSTANT	2028	802.348	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FPLPH2	1	1	1	
UCR	A014574	24-Jul-86	SYSTEM	PREM CO. HPOTP TURB DISC TEMP	HIGH EFF HPOTP TURB/2 NO2 TUBE RUPT	2108	801.445	HPOTP TURBINE DISCHARGE TEMPERATURE	5 FPLPH2	1	1	1	
UCR	A006844	14-Apr-83	FAM KI	FAM CALIBRATION CONSTANT ESTIMATE LOW	HIGH MIXTURE RATIO DUE TO KI	2011	802.308	HPOTP TURBINE DISCHARGE TEMPERATURE	4 FPL	0.75	1	0.75	
UCR	A015678	9-Nov-80	NOZZLE	TURBINE 125 THRU 148 BLOWN INWARD	NOZZLE TUBE RUPTURES	2003	SF1101.8	HPOTP TURBINE DISCHARGE TEMPERATURE	2 MPFA	0.25	1	0.25	
UCR	A016555	22-Sep-78	SYSTEM	CO-LOSS TURBINE TEMP EXCEEDED REDLINE	OVERSHOOT AT THROTTLE DOWN	0105	750.047	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	
UCR	A018565	13-Jul-78	NOZZLE	NOZZLE TUBE RUPTURES-HPOT RL	TUBE RUPTURE (12) DOBBY DOORS	2004	802.182	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	
UCR	A006345	22-May-79	NOZZLE	NUMEROUS TUBE LEAKS	TUBE LEAKS (13)	2004	802.158	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	
UCR	A006466	14-May-79	NOZZLE	HPFT OVERTEMP REDLINE CUTOFF	NOZZLE STEERING FAILED	0201	750.041	HPFTP TURBINE DISCHARGE TEMPERATURE	2 MPFA	0.25	1	0.25	
UCR	A006316	10-May-79	NOZZLE	NOZZLE TUBE SP. ITS COOLANT LOSS	COLD WALL TUBE LEAKS (3)	2004	802.157	HPOTP TURBINE DISCHARGE TEMPERATURE	3 FMOF	0.5	1	0.5	
<b>Failure to Maintain Proper Propellant Valve Position</b>													
SSMEYP													0.25
UCR	A018563	26-Jun-81	SYSTEM	PREMATURE CUTOFF/OPON POSITION	OPON LIMIT RESET MCF	0007	750.119		2 MPFA	0.25	1	0.25	
MSFC PRACA	A006247	17-Jun-81	HYDRAULICS	ACT CHECK-OUT MODULE FAILURE	OPON POSITION FAILURE		Field			1	0	0	
<b>HPFTP Coolant Line Overpressure</b>													
SSMELO													0.40
MSFC PRACA	A00162	22-Apr-81	TURBOMACHINERY	COOLANT LINE PRESS HAD ABNORMAL OSCILL	HPFTP COOLANT LINE OSCILLATIONS (SMALL OVERPRESSURE) - NO EFFECT SID		Field			1	0.1	0.1	
MSFC PRACA	A00660	16-Oct-81	TURBOMACHINERY	COOLANT LINE PRESSURE INCREASED	COOLANT LINE PRESSURE LIMIT (115 PSI) EXCEEDED - 270 PSI MARGIN TO DELTA EXCEEDED - 270 PSI MARGIN TO REDLINE (51 PSI) (SEE SFC 28-E 4.1)		Field			1	0.1	0.1	
MSFC PRACA	A11878	28-Sep-84	TURBOMACHINERY	PRESS OSCILL OF HPFTP COOLANT LINE - FA	COOLANT LINE PRESSURE LIMIT (115 PSI) EXCEEDED - 270 PSI MARGIN TO REDLINE (51 PSI) (SEE SFC 28-E 4.1)		Field			1	0.1	0.1	
MSFC PRACA	A15403	25-Apr-88	TURBOMACHINERY	SPKED BELOW 300 PSID DURING STS 55 (FA	HPFTP COOLANT LINE PRESSURE LIMIT (115 PSI) EXCEEDED - 270 PSI MARGIN TO REDLINE (51 PSI) (SEE SFC 28-E 4.1)		Field			1	0.1	0.1	

SSME/MPs Initiator Equivalent Flight Occurrences Evaluation												
SMEST	Critical Structural Failure of SSME Component											
Record Type	Record #	Date	System Element	NCA Nomenclature	NCA Part #	Failure Description from Record	Analyst Comments	Type	Configuration Applicability	Event Potentiality Factor	Weighting Factor	Equip. Flight Failure for Total Time
ANMCP8PRMPLPOTP												
MSFC PRACA	A13505	1-Dec-86	TURBOMACHNERY	LPOTP UN 4306	RS007801-191	LPOTP UN 4306 HIGH BREAK AWAY IN VIOLATION OF OMROD, ENGINE # 2012	LPOTP HIGH SHAFT TORQUE, BEARING DAMAGED	Field	1	0.02	0.02	0.06
MSFC PRACA	A14010	1-Aug-87	TURBOMACHNERY	LPOTP UN 2028	RS007801-191	LPOTP UN 2028, HIGH BREAK AWAY TORQUE		Field	1	0.02	0.02	
MSFC PRACA	A14393	23-Nov-87	TURBOMACHNERY	LPOTP UN 2030	RS007801-191	LPOTP UN 2030 SHAFT SEIZED		Field	1	0.02	0.02	
ANMPS8PRMPLPOTB												
							COOLANT UNDER PRESSURE DROPPED AT C/O & 4 SEC. HPFTP SPEED ROSE AT C/O (DAMAGE TO HPFTP, EXCESSIVE SHAFT TRAVEL, EXCESSIVE WEAR DUE TO IMBALANCE)					0.08
MSFC PRACA	A08739	17-Oct-80	TURBOMACHNERY	RING, LOW PR ORRICE	RS007559-009			Field	1	0.02	0.02	
MSFC PRACA	A08145	11-Apr-80	TURBOMACHNERY	IMPELLER	RS007556-013-25	EXCESSIVE WEAR, CRACKING, & RAISED MATL. IMPELLER CRACK	HPFTP IMPELLER CRACK - NO EFFECT	Field	1	0.02	0.02	
							HPFTP IMPACT DAMAGE ON PUMP BORE, UNKNOWN CONTAMINATION - SEEMED TO HAVE NO EFFECT BUT SOUNDED SERIOUS					
MSFC PRACA	A10076	27-May-82	TURBOMACHNERY	DIFFUSER	RS007532-091	IMPACT DAMAGE ON VANES	HPFTP DIFFUSER NO 9 VANE DENTED BY IMPACT DAMAGE OF UNKNOWN CONTAMINATION - NO APPARENT EFFECT	Field	1	0.02	0.02	
MSFC PRACA	A10203	10-Jul-82	TURBOMACHNERY	DIFFUSER	RS007527-061	DIFFUSER NO 9 VANE DENTED		Field	1	0.02	0.02	0.1
ANMBS8PRMPLPOTB												
MSFC PRACA	A14130	1-Aug-87	TURBOMACHNERY	HPFTP 1ST STG BLD9	RO010921-035	400790 HPFTP 1ST STAGE BLADE STOP FAILURE, ENGINE #012		Field	1	0.02	0.02	
MSFC PRACA	A08076	27-Mar-80	TURBOMACHNERY	DISC 1ST STAGE ROTOR	RS007517-025	AU PLATE MISSING, CRACKS IN FRITREE ROOTS	CRACKS IN FRITREE ROOTS, HPFTP DISCH FIRST STAGE ROTOR	Field	1	0.02	0.02	
MSFC PRACA	A09265	26-Jun-81	TURBOMACHNERY	BLADE 1ST STAGE	RO010921-013	CRACK IN FRITREE LOBBES, 1ST STAGE BLADE HPFTP, DISABLY INSP, CANOGA	CRACK IN FIRST STAGE BLADES - SOME INFO ON CRACKS FROM 79-80	Field	1	0.02	0.02	
MSFC PRACA	A09461	21-Aug-81	TURBOMACHNERY	BLADE 1ST STAGE	RO010921-025	CRACK IN FRITREE LOBBES, 1ST STAGE BLADE HPFTP, DISABLY INSP, CANOGA	CRACK IN FIRST STAGE BLADES - SOME INFO ON CRACKS FROM 79-80	Field	1	0.02	0.02	
MSFC PRACA	A02869	4-May-77	TURBOMACHNERY	HPFTP	RS007501-261	TIP SEAL/NOZ VANES & SHOULDER EROSION		Field	1	0.02	0.02	0.06
ANMHOCDPRMPLPOTD												
MSFC PRACA	A10062	1-May-82	TURBOMACHNERY	INLET VANE	RS007743-037	CAVITATION DAMAGE, INLET VANE	CAVITATION OF HPOTP - NO REDLINE, HIGHER THAN NORMAL HEAT LOSS	Field	1	0.02	0.02	
MSFC PRACA	A10069	26-May-82	TURBOMACHNERY	SEALS	RS007773-013	CAVITATION DAMAGE	CAVITATION OF HPOTP - NO REDLINE, HIGHER THAN NORMAL HEAT LOSS	Field	1	0.02	0.02	
MSFC PRACA	A10073	29-May-82	TURBOMACHNERY	IMPELLER	RS007719-043	CAVITATION DAMAGE	CAVITATION OF HPOTP - NO REDLINE, HIGHER THAN NORMAL HEAT LOSS	Field	1	0.02	0.02	
MSFC PRACA	A12023	19-Jan-85	TURBOMACHNERY	VANE, R.H.	RS007741-037	CAVITATION DAMAGE ON R.H. VANE, HPOTP		Field	1	0.02	0.02	0.06
ANMOTS8PRMPLPOTB												
MSFC PRACA	A08530	19-Sep-81	TURBOMACHNERY	HPOTP UN 2018R3	RS007701-301	METAL PIECE LODGED IN 1ST STAGE NOZZLE	SHEET METAL SPOT WELD FAILURE, WEDGED IN	Field	1	0.02	0.02	
MSFC PRACA	A01035						CRACK IN FRITREE SHAFT, 1ST STAGE BLADES HPO	Field	1	0.02	0.02	
MSFC PRACA	A12198	14-Apr-85	TURBOMACHNERY	TIP SEAL RETAINER	RS007813	TURBINE BLADE TIP SEAL GAP EXCEEDS SPEC, HPOTP UN 4106R1	HPOTP TIP SEAL RETAINER - GAP REQ. EXCEEDED	Field	1	0.02	0.02	0.04
ANMOTLCP8PRMPLPOTB												
MSFC PRACA	A08751	22-Jun-79	TURBOMACHNERY	STRUT TURB DISCHARGE	RS007779-021	LET PARTIALLY OBSTRUCTED	HPFTP CONTAMINATION LOSS OF COOLANT, LET PARTIALLY OBSTRUCTED - NO EFFECT	Field	1	0.02	0.02	
MSFC PRACA	A12733	14-Feb-86	TURBOMACHNERY	ECCENTRIC RING	RS007879-005	ECCENTRIC RING FOUND CRUSHED POST STB-32	HPOTP ECCENTRIC RING FOUND CRUSHED, POST STB-32 LOSS OF H2 COOLANT TO TURBINES POSSIBLE	Field	1	0.02	0.02	0.02
ANMBS8PRMPLPOTB												
MSFC PRACA	A13928	3-Apr-87	TURBOMACHNERY	RING, ASSY OF	RO019213-001	HPFTP THRUST BALL CRACKED POST STB-37, NO EFFECT	HPFTP THRUST BALL CRACKED POST STB-37, NO EFFECT	Field	1	0.02	0.02	0.02
ANMKS8PRMPLPONZ												
MSFC PRACA	A11642	29-Jul-84	TURBOMACHNERY	NOZZLE, 2ND STAGE	RO016027-21	2ND STAGE NOZZLE CRACKS IN TURNING VANES, HPOTP UN 1000R2		Field	1	0.02	0.02	0.06
ANMRR8PRMPLPORR												
MSFC PRACA	A10074	29-May-82	TURBOMACHNERY	WASHER	RS007873-003	CRACKED CUPWASHER, HPOTP, DISASSEMBLY	HPOTP CRACKED CUPWASHER, RECURRING PROBLEM AS PER REPORT BUT CONSEQUENCES UNKNOWN	Field	1	0.01	0.01	

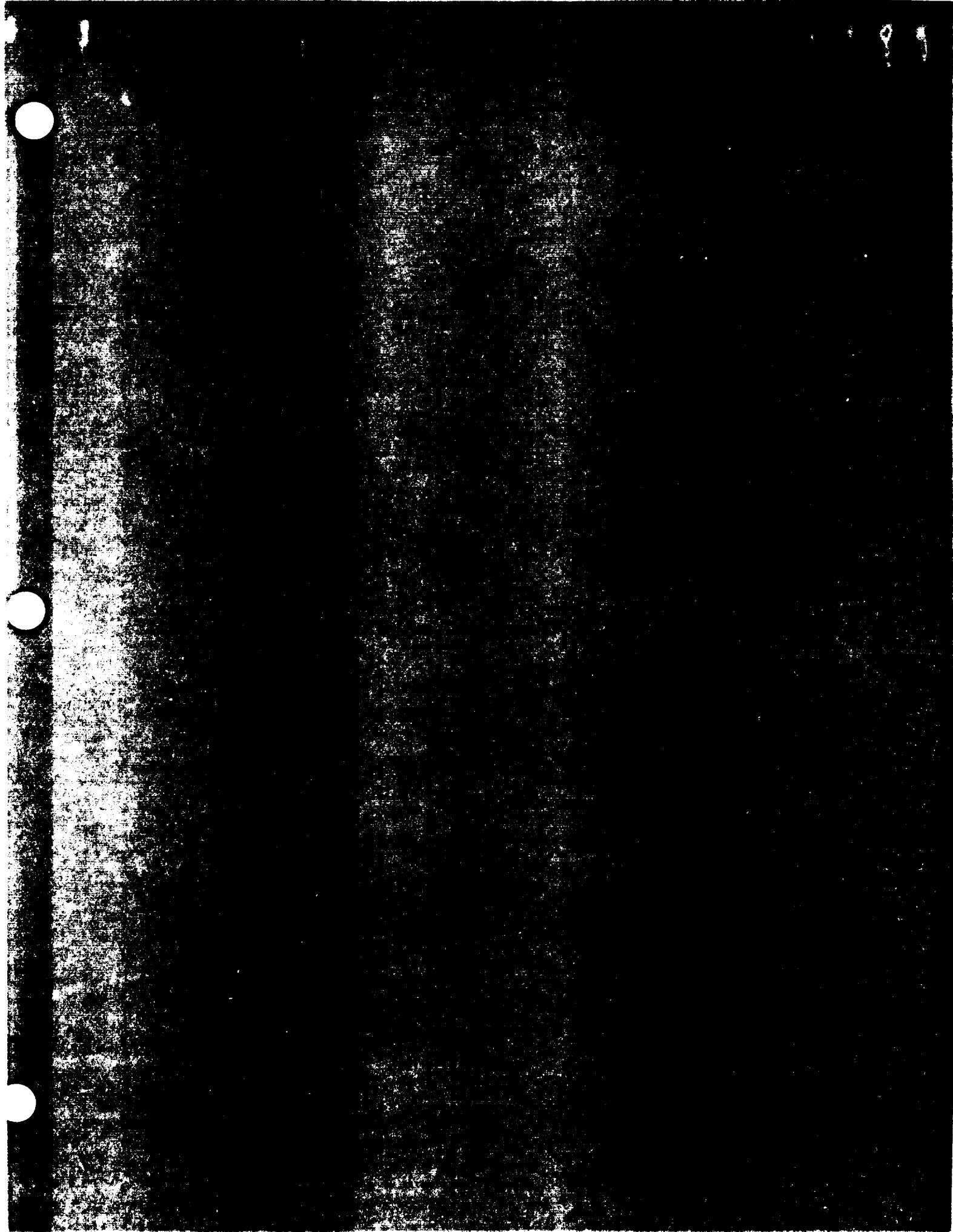


SSME/MPs Initiator Equivalent Flight Occurrences Evaluation												
SME/ST		Critical Structural Failure of SSME Component										
Record Type	Record #	Date	System Element	NCA Nomenclature	NCA Part #	Failure Description from Record	Analyst Comments	Type	Configuration Applicability	Event Potentiality Factor	Weighting Factor	Est. Flight Failure for Total Time
Cause ID	Initiator/Cause Description											
MSFC PRACA	A10157	2-Jul-82	TURBOMACHINERY	CUPWASHER	RS007704-003	BROKEN CUPWASHER. HPOTP DISASSEMBLY	HPOTP CRACKED CUPWASHER. DEBRIS PEANS THE SURFACE OF THE MAIN IMPELLER OUTER SHROUD. RETAINERS RING AND SILVER SEAL AT THE PRESSURE SENSING ORIFICE AREA	Field	1	0.01	0.01	
MSFC PRACA	A10157	2-Jul-82	TURBOMACHINERY	CUPWASHER	RS007704-003	BROKEN CUPWASHER. HPOTP DISASSEMBLY	HPOTP CRACKED CUPWASHER. DEBRIS PEANS THE SURFACE OF THE MAIN IMPELLER OUTER SHROUD. RETAINERS RING AND SILVER SEAL AT THE PRESSURE SENSING ORIFICE AREA	Field	1	0.01	0.01	
MSFC PRACA	A12196	19-Apr-85	TURBOMACHINERY	CUPWASHERS	R032220-3	CUPWASHER (2) ROTATED DURING HOT FIRE. HPOTP UN 222R1, ENGINE 2022	3 ROTATED CUPWASHERS IN HPOTP	Field	1	0.01	0.01	
MSFC PRACA	A12197	19-Apr-85	TURBOMACHINERY	CUPWASHERS	R032220-3	CUPWASHER (2) ROTATED DURING HOT FIRE. HPOTP UN 210R1, ENGINE 2028	3 ROTATED CUPWASHERS	Field	1	0.01	0.01	
ANM088FPRMHPPOEV												0.18
MSFC PRACA	A11825	17-Dec-84	TURBOMACHINERY	TURBINE END #3 BRNG	RS007955-301	NO. 3 BEARING INNER RACE CRACK. HPOTP UN 910R1		Field	1	0.02	0.02	
MSFC PRACA	A05502	28-Aug-78	TURBOMACHINERY	HPOTP UN 0007R2	RS007701-271	SPALLED BALLS AND SURFACE DISTRESS/RACES	SPALLED BALLS & SURFACE DISTRESS OF RACES CALUSED SUB SYN VIB - MAYBE STRUCTURAL	Field	1	0.02	0.02	
MSFC PRACA	A05502	28-Aug-78	TURBOMACHINERY	HPOTP UN 0007R2	RS007701-271	SPALLED BALLS AND SURFACE DISTRESS/RACES		Field	1	0.02	0.02	
MSFC PRACA	A05503	28-Aug-78	TURBOMACHINERY	HPOTP UN 0007R2	RS007701-271	SURFACE DISTRESS ON RACES		Field	1	0.02	0.02	
MSFC PRACA	A05344	3-Apr-79	TURBOMACHINERY	HPOTP UN 2404	33DRS007701-171	SPALLED BALLS AND GAGE DELAMINATION		Field	1	0.02	0.02	
							HPOTP #2, 4 BEARING (TURBINE END) INNER RACE FAILURE - PUMP OPERATED W/ HIGH SYNCHRONOUS VIBRATION DURING STS-27 ECP 1048 REDISION					
MSFC PRACA	A11825	17-Dec-84	TURBOMACHINERY	TURBINE END #3 BRNG	RS007955-301	NO. 3 BEARING INNER RACE CRACK. HPOTP UN 910R1		Field	1	0.02	0.02	
							HPOTP #2, 4 BEARING (TURBINE END) INNER RACE FAILURE - PUMP OPERATED W/ HIGH SYNCHRONOUS VIBRATION DURING STS-27 ECP 1048 REDISION					
MSFC PRACA	A11989	20-Jan-85	TURBOMACHINERY	BEARING #4	RS007955-301	CRACKS IN #4 TURBINE END BEARING RACE. HPOTP UN 910R1		Field	1	0.02	0.02	
MSFC PRACA	A14156	1-Aug-87	TURBOMACHINERY	HPOTP UN 400R3	RS007701-531	HPOTP UN 400R3 STRAIN GAGE DATA DISCREPANCY. BEARING WEAR		Field	1	0.02	0.02	
MSFC PRACA	A14782	23-Mar-88	TURBOMACHINERY	HPOTP UN 400R2	RS007701-531	HPOTP UN 400R2 BEARING GAGE FREQUENCIES		Field	1	0.02	0.02	
ANM088FPRMHPPOEV												0.02
MSFC PRACA	A15189	12-Jan-89	TURBOMACHINERY	HPOTP	RS007701-591	HIGH SYNCHRONOUS VIBRATIONS ON HPOTP UN 8409, STS-44		Field	1	0.02	0.02	
ANM1P5FPRMAM												0.06
MSFC PRACA	A05916	16-Dec-78	COMBUSTION	MAIN INJECTOR	RS009122-391	SLIGHT LOX POST EROSION		Field	1	0.02	0.02	
MSFC PRACA	A08769	22-Oct-80	COMBUSTION	RETAINER	RS009133-011	RETAINER BURN THRU & GALLING		Field	1	0.02	0.02	
MSFC PRACA	A08173	3-May-81	COMBUSTION	MAIN INJECTOR	RS009122-801	#8 RETAINER DAMAGE		Field	1	0.02	0.02	
ANM088FPRMAM												0.02
MSFC PRACA	D0707A087C	7-Oct-80	COMBUSTION	BAFFLE ELEMENT	R0019527-091	INNER COPPER JACKET BURN THROUGH		Field	1	0.02	0.02	
ANM1FAERPRMPPAS												0.02
MSFC PRACA	A07144	29-Aug-79	ENGINE	FPB AS LOX LINE	RS007001-061	FPB AS LOX LINE RUPTURED		Field	1	0.02	0.02	
ANM1F8FPRMPPBFP												0.06
MSFC PRACA	A04577	18-Apr-78	COMBUSTION	FPB INJECTOR	RS009020-501	INJECTOR FACE EROSION		Field	1	0.02	0.02	
MSFC PRACA	A06546	25-Nov-81	COMBUSTION	FPB INJECTOR	RS009020-821	EROSION ON INJECTOR FACE PLATE		Field	1	0.02	0.02	
MSFC PRACA	A06917	28-Jan-82	COMBUSTION	FPB INJECTOR	RS009020-771	EROSION AND SLAG ON INJECTOR FACE PLATE		Field	1	0.02	0.02	

SSME/MPS Initiator Equivalent Flight Occurrences Evaluation			Nominal Ope
Initiator ID	Cause ID	Description	Source
SMEST		Structural Failure of SSME Components Leading to LOV	
	ANMHWSPRPMCCMW	MCC MANIFOLD WELD FAILURE	MCC PRA
	ANMEDBPRPMEDNCO	FAILURE IN EDNI LINER CLOSEOUT STRUCTURE	MCC PRA
	ANMHWCRPRPMCCCHW	MCC HOT GAS WALL FAILURE DUE TO UNSTABLE CRACK GROWTH	MCC PRA
	ANMFRBTPRPMFRI	FAILURE OF FLOW RECIRCULATION INHIBITOR	MCC PRA
	ANMCCCRPRPMCCCC	FAILURE OF MCC COOLANT CHANNEL DUE TO UNSTABLE CRACK GROWTH	MCC PRA
	ANMBSFPRPMCCBP	MCC MULTIPLE BOLT FAILURE DUE TO INADEQUATE PRELOAD	MCC PRA
	ANMHWFPRPMHGMWF	HGM TRANSFER TUBE WELD FAILURE	WELD STUDY
SMEHL		Hydraulic Lock-up Required	PRA APU Analysis
SMELP		Propellant Management System And/Or SSME Combustible Leakage	Lockheed PRA
SMELH		Helium System Leakage	Lockheed PRA
SMEPG		Failure To Provide Helium Pogo Charge	NPRD-3
SMEPV		Failure To Maintain Propellant Supply System Valve Positions	MPS F.R.D., NPRD91
SMEDS		Simultaneous Dual SSME Shutdown	See Fault Tree in Next Section
SMECD		Nominal MECO & Dump; No Mainstage Initiators	PRA Preliminary Results



SSME/MPs Initiator Frequency Summary						
Initiator ID	Initiator Description	Total Exposure Time		621491	sec	Percent of Non-nominal Initiators
		Equivalent Flight Occurrences for Total Exposure Time	One Engine Initiator Freq (per mission)	Cluster Initiator Freq (per mission)	Mean # of Missions Between Occurrences	
SMEFO	Loss of MCC Pressure	4.00	3.35E-03	1.00E-02	100	25.87%
SMEFH	Loss of Gross H2 Flow	0.50	4.18E-04	1.25E-03	797	3.24%
SMEMO	High Mixture Ratio in Oxidizer Preburner	0.25	2.09E-04	6.27E-04	1594	1.62%
SMEMF	High Mixture Ratio in Fuel Preburner	0.25	2.09E-04	6.27E-04	1594	1.62%
SMEPB	Loss of Fuel to Both Preburners	6.25	5.23E-03	1.56E-02	64	40.34%
SMEVP	Failure to Maintain Proper SSME Propellant Valve Position	0.25	2.09E-04	6.27E-04	1594	1.62%
SMELO	HPFTP Coolant Liner Overpressure	0.40	3.35E-04	1.00E-03	898	2.59%
SMEST	Critical Structural Failure of SSME Components	1.13	9.53E-04	2.85E-03	350	7.38%
SMEHL	Hydraulic Lock-up Required	1.59	1.33E-03	4.00E-03	250	10.34%
SMELP	Propellant Management System And/Or SSME Combustible Leakage	0.32	2.65E-04	7.96E-04	1256	2.06%
SME LH	Helium System Leakage	0.26	2.15E-04	6.46E-04	1548	1.67%
SMEPG	Failure To Provide Helium Pogo Charge	0.24	2.02E-04	6.05E-04	1653	1.56%
SMEPV	Failure To Maintain Propellant Supply System Valve Positions	0.01		1.89E-05	52910	0.05%
SMEDS	Simultaneous Dual SSME Shutdown	0.00		1.00E-05	100000	0.03%
SMECD	Nominal MECO & Dump; No Mainstage Initiators	376		9.43E-01	1,060	





TRANSFER	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
HIGH MIXTURE RATIO IN OPB	HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEFO/SMEMO	OR	EH				
2.30E-05 SMEFO/SMEMO	1.50E-04 PAGE 13	1.16E-06 PAGE 3	2.30E-05 2.67E-11 3.45E-09	OK abort LOV LOV	MO/EH MO/OR	1 2 3

INITIATOR	PROTECTIVE EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#	TRANSFER TO
LOSS OF GROSS H2 FLOW	CONTROLLER INCREASES O2 FLOW TO FPB					
SMEFH	OF					
SMEFH		1.25E-03	TRANSFER		1	SMEMF EVENT TREE
	PAGE 9	1.25E-07	TRANSFER	FH/OF	2	SMEPB EVENT TREE

LOSS OF GROSS H2 FLOW EVENT TREE 2 REV. 1



TRANSFER	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
HIGH MIXTURE RATIO IN FPB	HPFTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEFH/SMEMF	FR	EH				
1.25E-03 SMEFH/SMEMF	1.50E-04 PAGE 13	1.16E-06 PAGE 3	1.25E-03 1.45E-09 1.88E-07	OK abort LOV LOV	MF/EH MF/FR	1 2 3

TRANSFER	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
LOSS OF FUEL TO BOTH PREBURNERS	HPFTP OR HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEFH/SMEPB	TR	EH				
1.25E-07			1.25E-07	OK abort		1
SMEFH/SMEPB		1.16E-06 PAGE 3	1.45E-13	LOV	PB/EH	2
	2.25E-08 PAGE 13		2.81E-15	LOV	PB/TR	3

LOSS OF FUEL TO BOTH PREBURNERS EVENT TREE 2B REV. 1

INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
HIGH MIXT. RATIO IN OPB	HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEMO	OR	EH				
6.27E-04			6.27E-04	OK abort		1
SMEMO			7.27E-10	LOV	MO/EH	2
			9.41E-08	LOV	MO/OR	3

INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
HIGH MIXTURE RATIO IN FPB	HPFTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEF	FR	EH				
SMEF	PAGE 13	PAGE 3	6.27E-04	OK abort		1
			7.27E-10	LOV	MF/EH	2
			9.41E-08	LOV	MF/FR	3

INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
LOSS OF FUEL TO BOTH PREBURNERS	HPFTP OR HPOTP DT REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEPB	TR	EH				
SMEPB	PAGE 13	PAGE 3	1.56E-02	OK abort		1
			1.81E-08	LOV	PB/EH	2
			3.51E-10	LOV	PB/TR	3

LOSS OF FUEL TO BOTH PREBURNERS EVENT TREE 5 REV. 1

INITIATOR	MITIGATING EVENTS		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#	TRANSFER TO
FAILURE TO MAINTAIN SSME VALVE POSITIONS	FAIL-SAFE SERVOSWITCH WORKS	EMERGENCY PNEUMATIC SHUTDOWN					
SMEVP	HL	EP					
6.27E-04 SMEVP			6.27E-04	TRANSFER		1	SMEHL EVENT TREE
	2.10E-06 PAGE 8	1.41E-04 PAGE 5	1.32E-09	OK abort		2	
			1.86E-13	LOV	VP/HL/EP	3	



INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
COOLANT LINER OVERPRESSURE.	REDLINE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMELO	OP	EH				
SMELO	PAGE 18	PAGE 3	1.00E-03	OK abort		1
			1.16E-09	LOV	LO/EH	2
			1.50E-07	LOV	LO/OP	3



INITIATOR	PROTECTIVE EVENT		MITIGATING EVENT	SYSTEM EVENTS		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
HYDRAULIC LOCK-UP REQUIRED	BY-PASS VALVE FAILS TO MOVE	NO VALVE DRIFT	EMERGENCY PNEUMATIC SHUTDOWN	MAIN ENGINE CUT-OFF	PROPELLANT DUMP				
SMEHL	BL	ND	EP	ME	PM				
SMEHL						3.20E-03	OK		1
						5.28E-10	LOV	HL/PM	2
						4.58E-07	LOV	HL/ME	3
						8.00E-04	OK abort		4
						1.13E-07	LOV	HL/ND/EP	5
					9.28E-09	LOV	HL/BL		

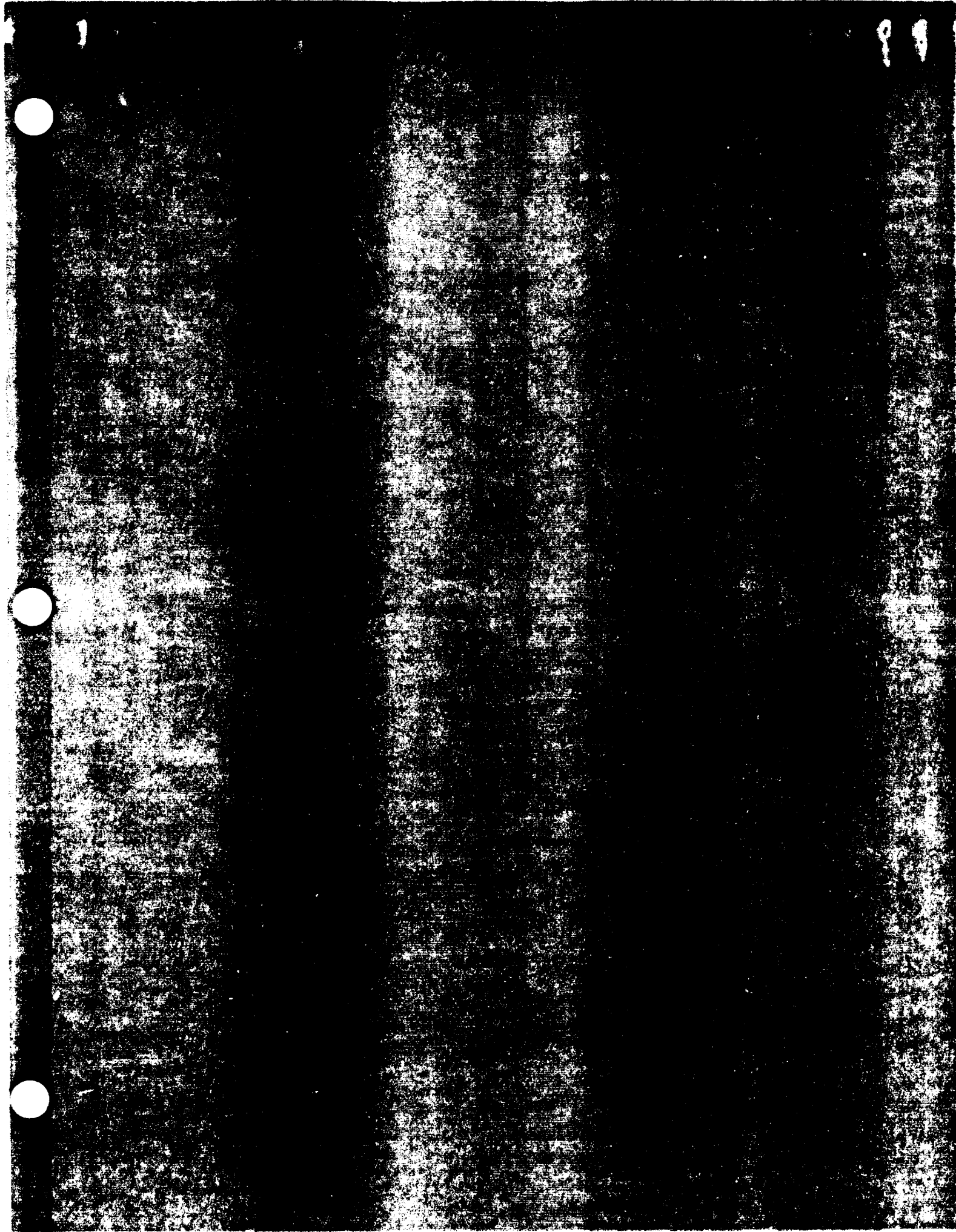


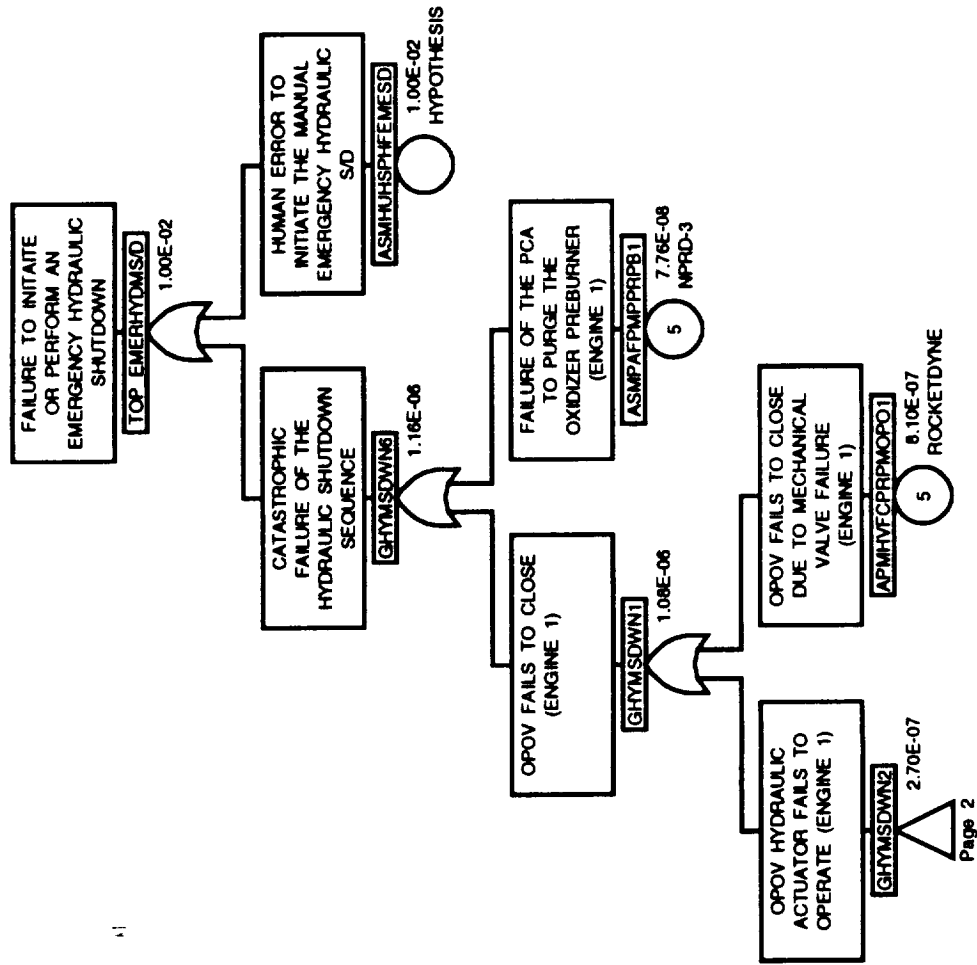
INITIATOR	PROTECTIVE EVENT	MITIGATING EVENT	SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
FAILURE TO PRECHARGE POGO ACC.	LOW POGO PRESSURE DETECTED	EMERGENCY HYDRAULIC SHUTDOWN				
SMEPG	PP	EH				
SMEPG	BASIC EVENT	PAGE 3	6.05E-04	OK abort		1
			7.02E-10	LOV	PG/EH	2
			9.08E-08	LOV	PG/PP	3

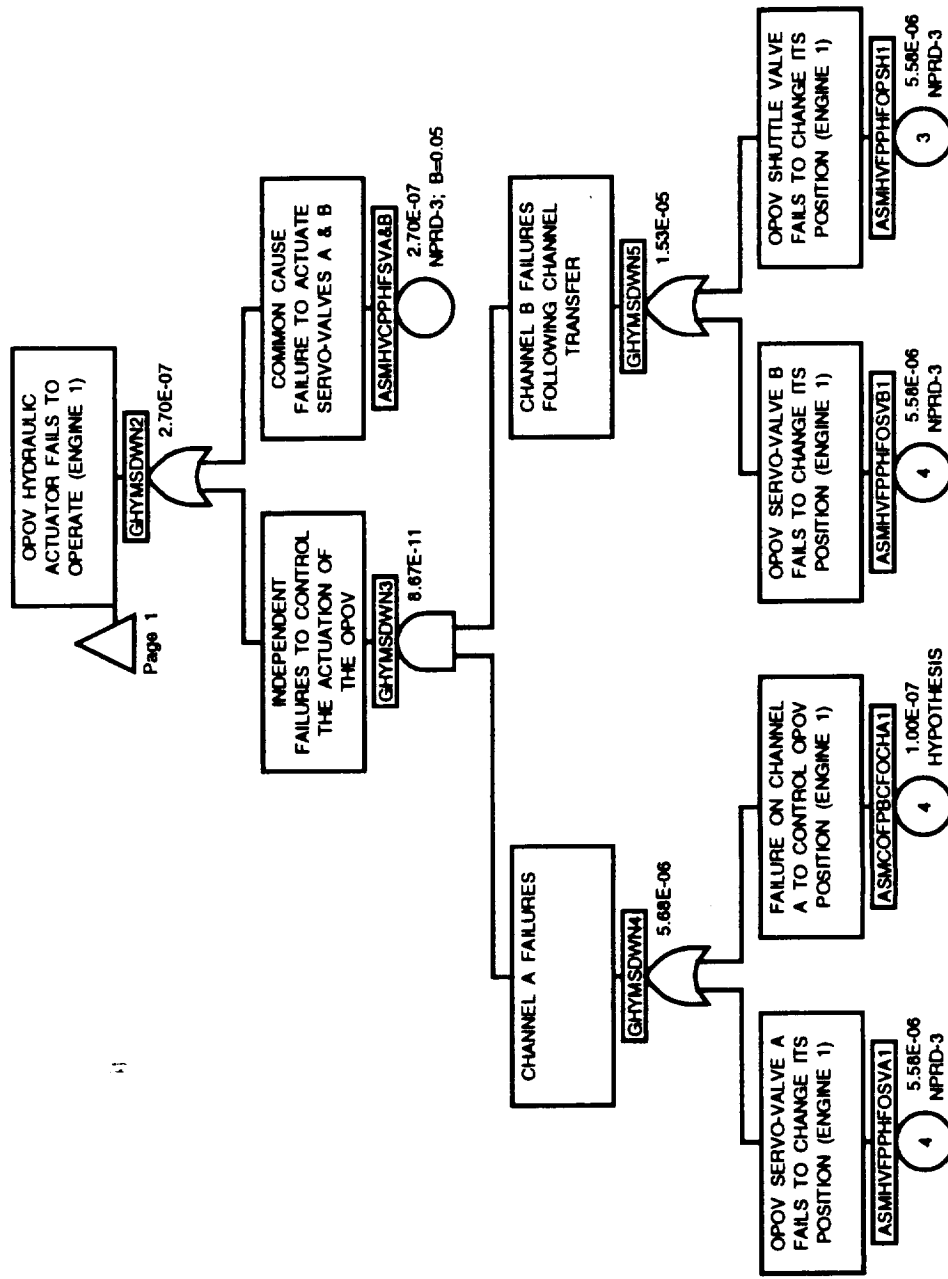
INITIATOR	MITIGATIVE EVENT		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
DUAL SSME PREMATURE SHUTDOWN	DUAL SSME PREMATURE S/D BEFORE LIFT-OFF	DUAL SSME PREMATURE S/D AFTER DROOP(109)				
SMEDS	BL	AC				
1.00E-05 SMEDS			0.00E+00	OK abort		1
	1.0		3.54E-06	OK abort		2
	BASIC EVENT	.65 BASIC EVENT	6.46E-06	LOV	DS/BL/AC	3

INITIATOR	SYSTEM EVENT		SEQ.PROB.	CLASS	SEQUENCE DESCRIPTION	#
NOMINAL MECO AND PROPELLANT DUMP REQUIRED	MECO PERFORMED	PROPELLANT DUMP PERFORMED				
SMECD	MN	PD				
.94 SMECD			9.43E-01	OK		1
			1.65E-07 PAGE 40	LOV	CD/PD	2
			2.46E-06 PAGE 30	LOV	CD/MN	3

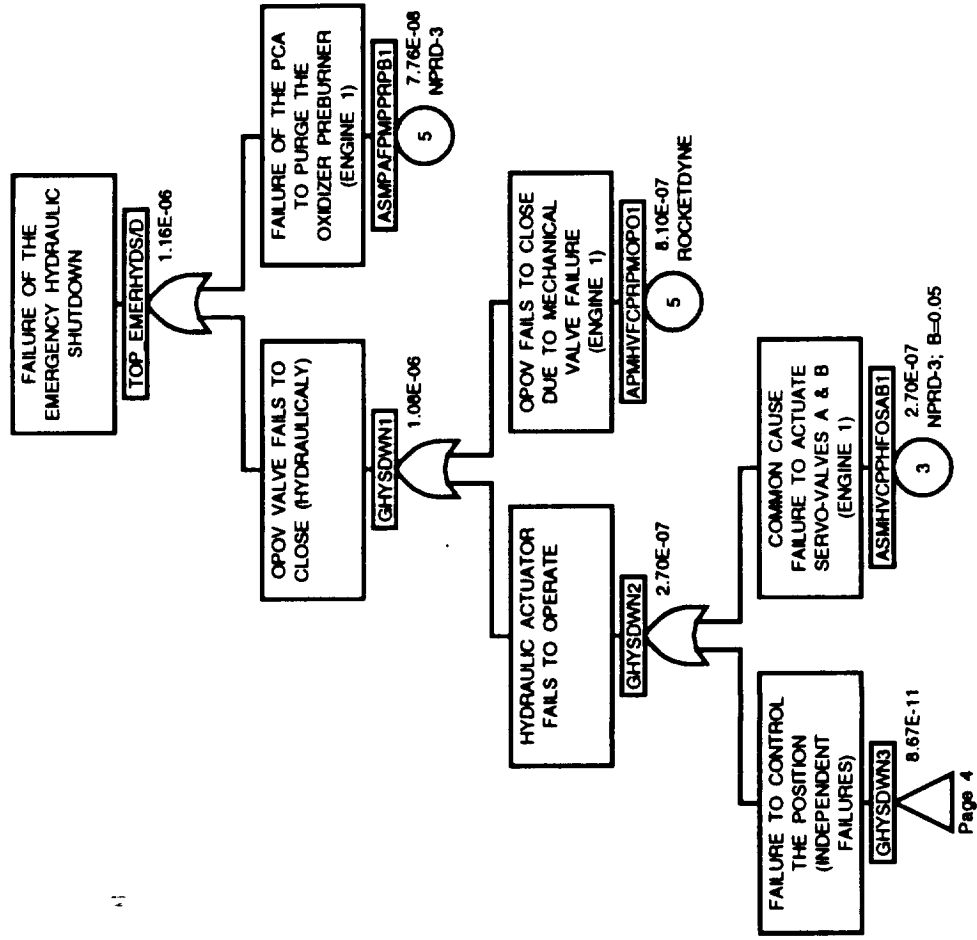
FAILURE TO PERFORM NOMINAL MECO & PROPELLANT DUMP EVENT TREE 12 REV. 1

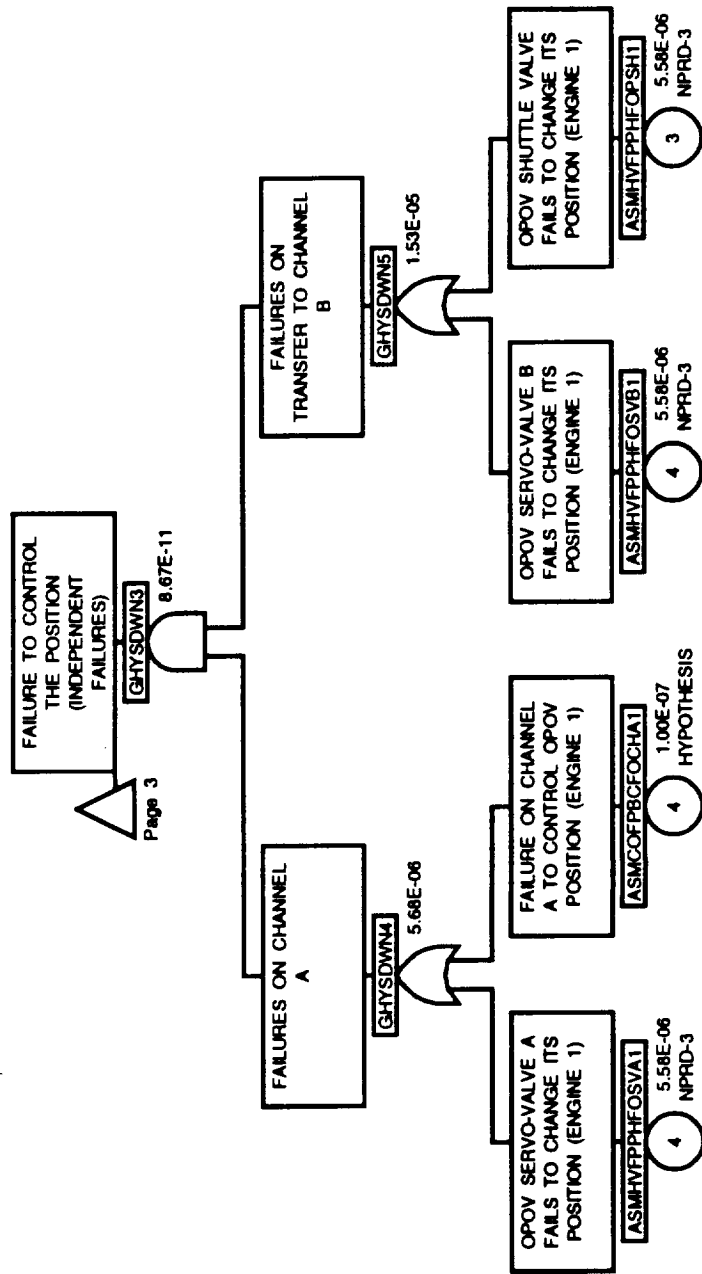




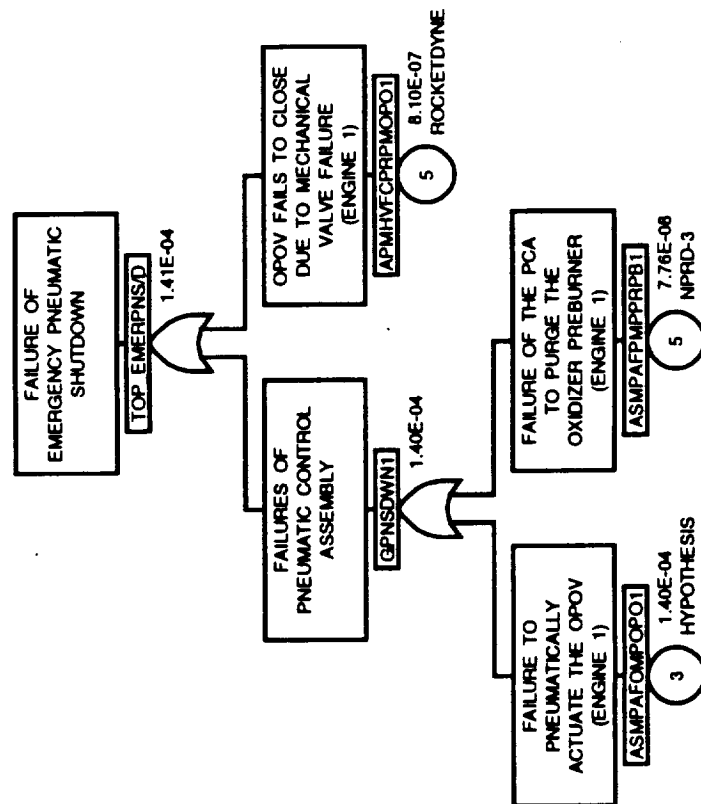


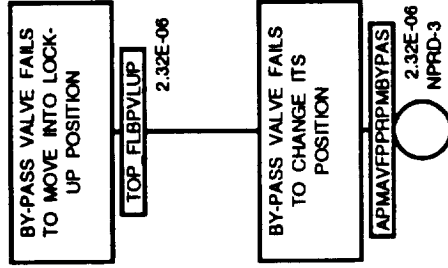


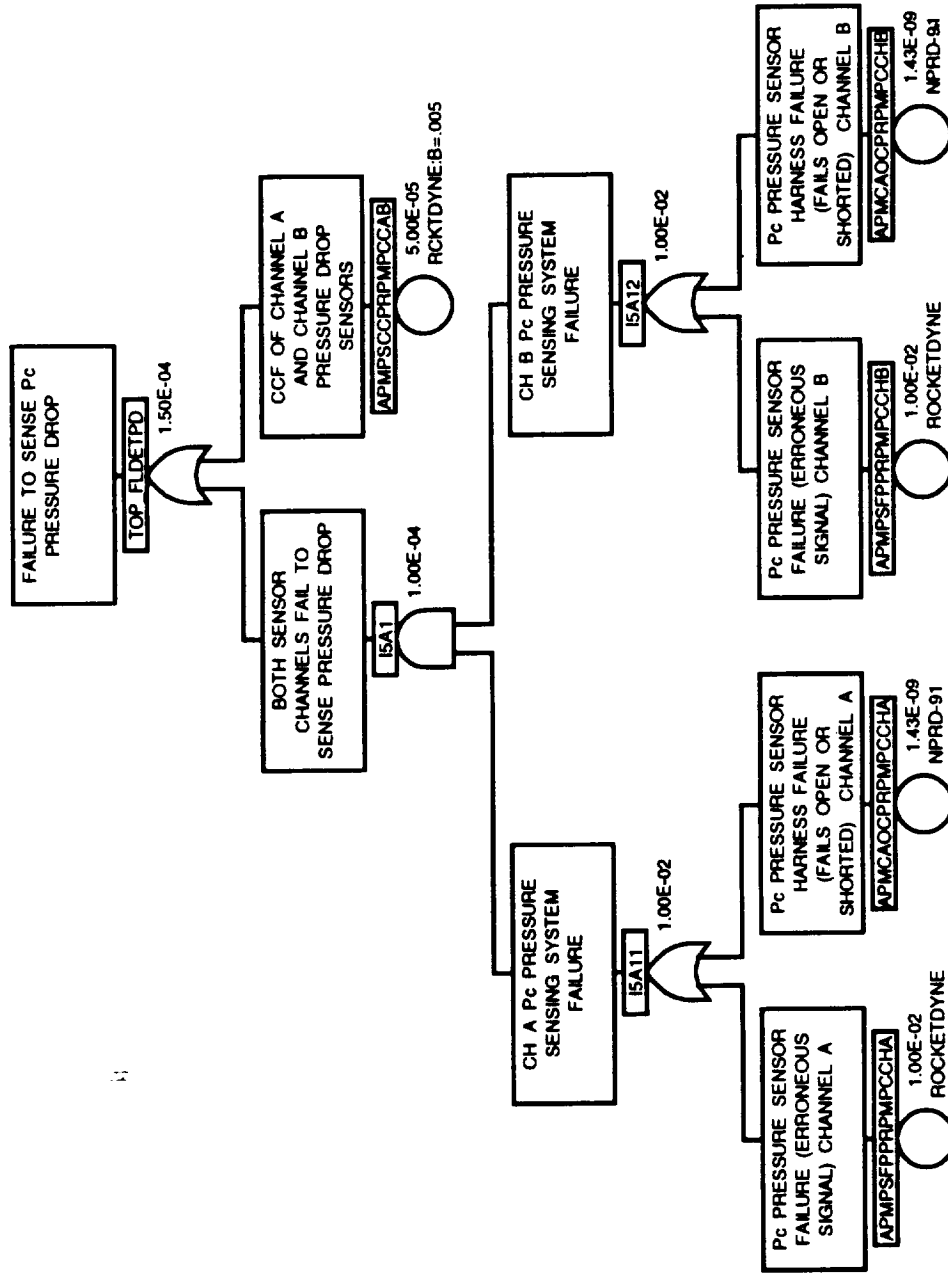


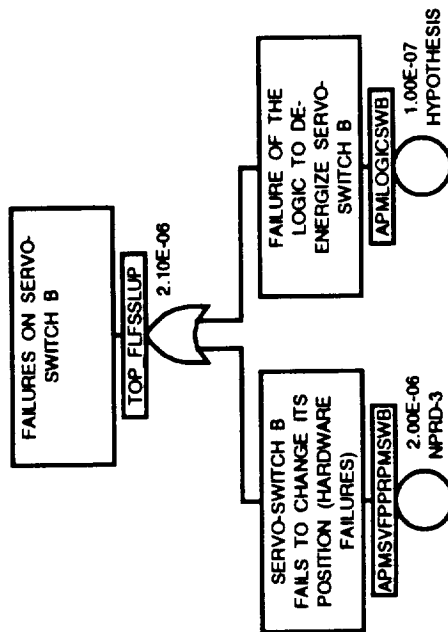


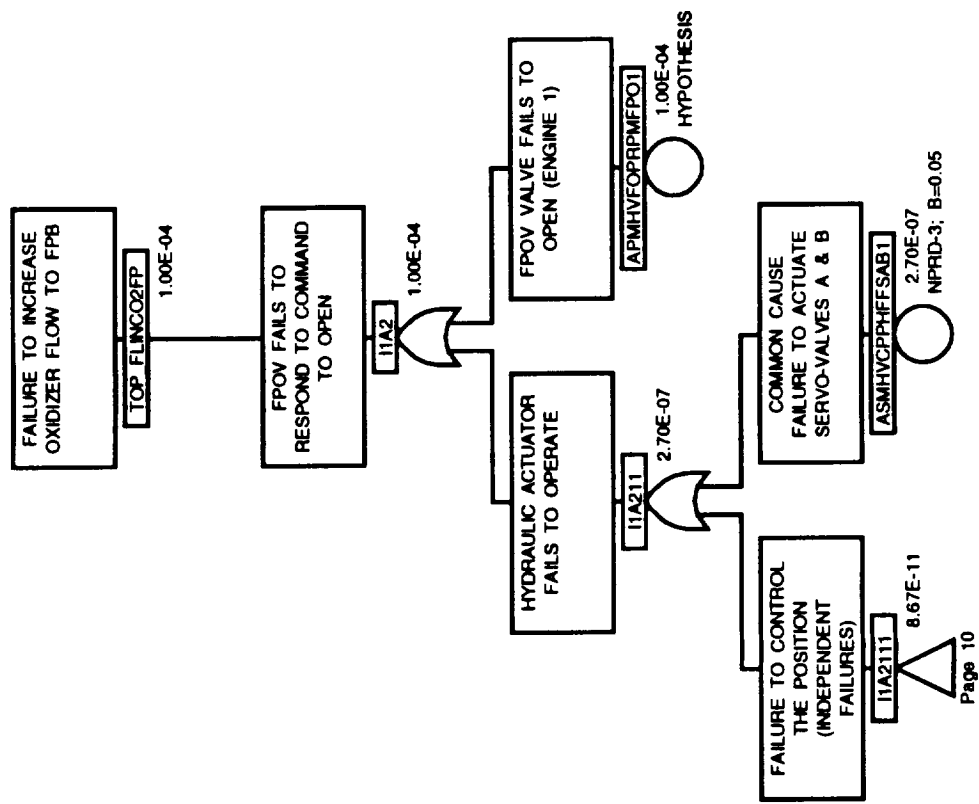
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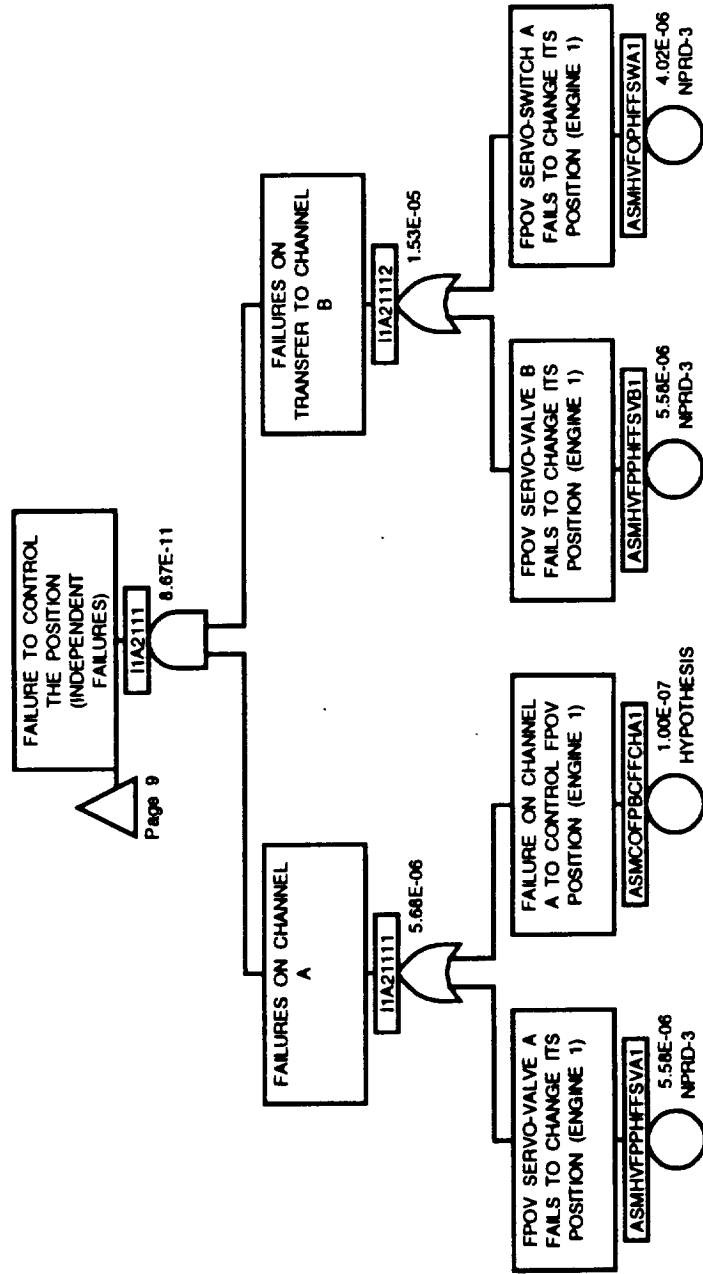




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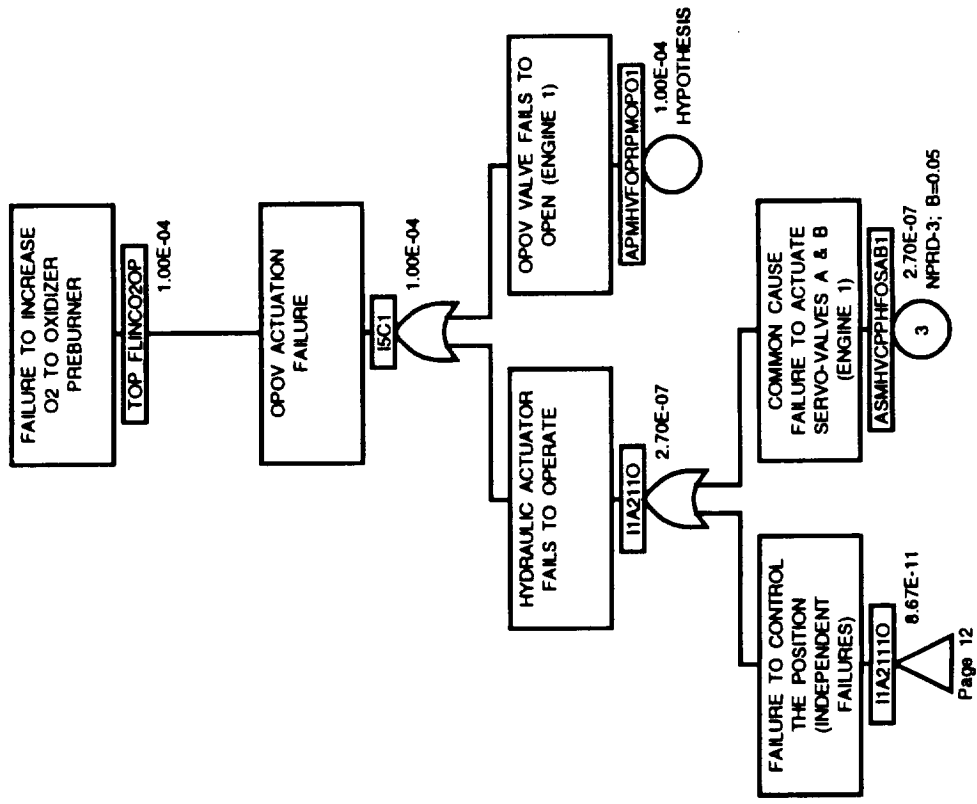
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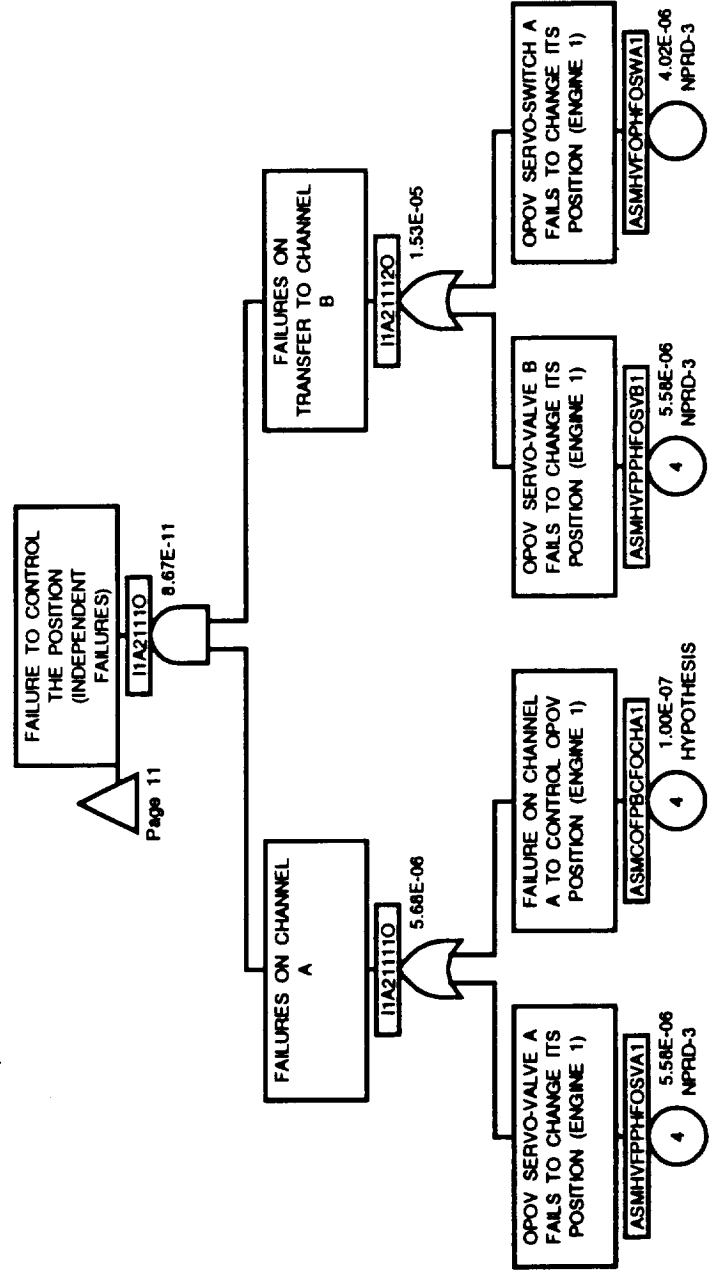
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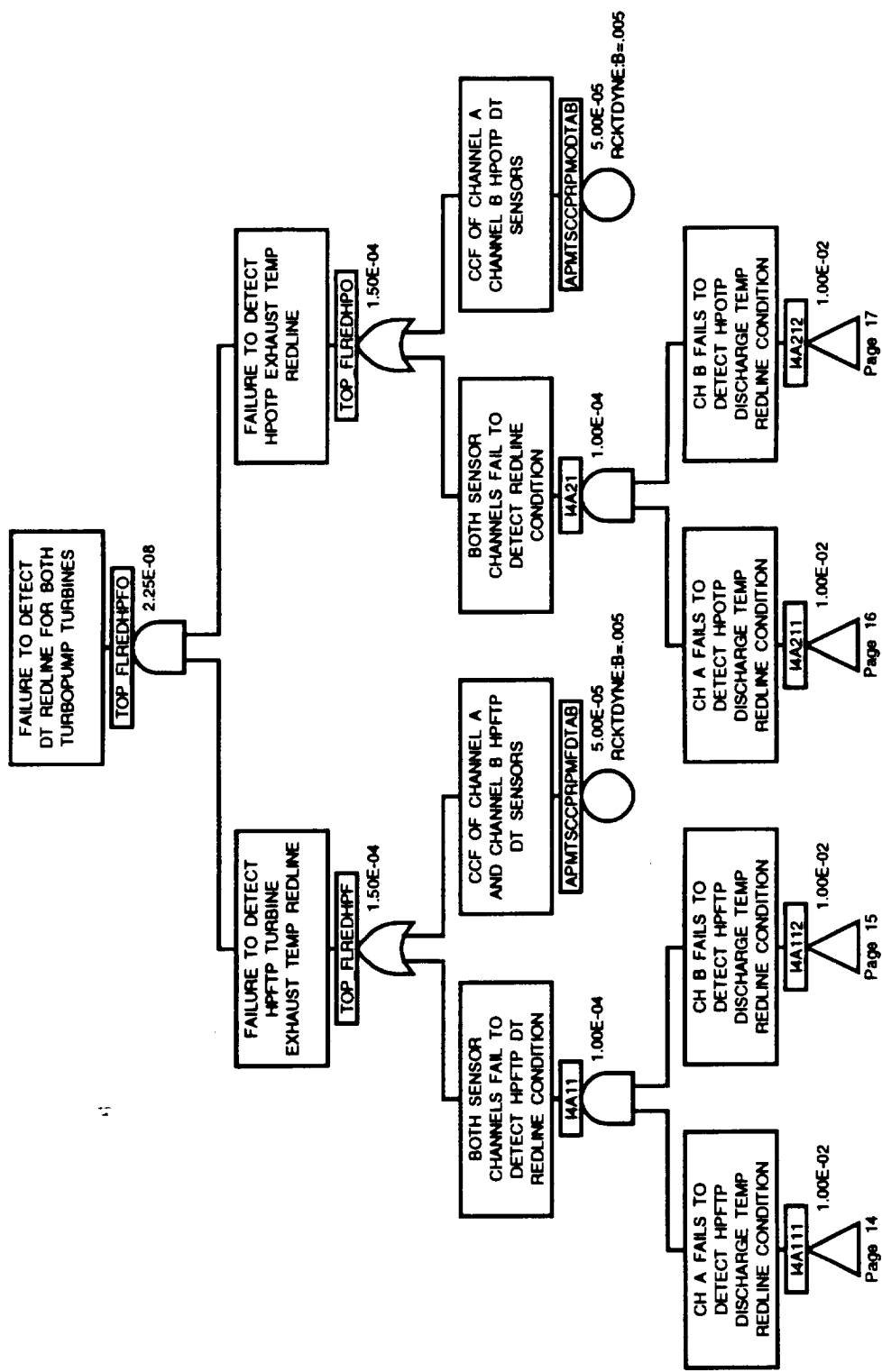
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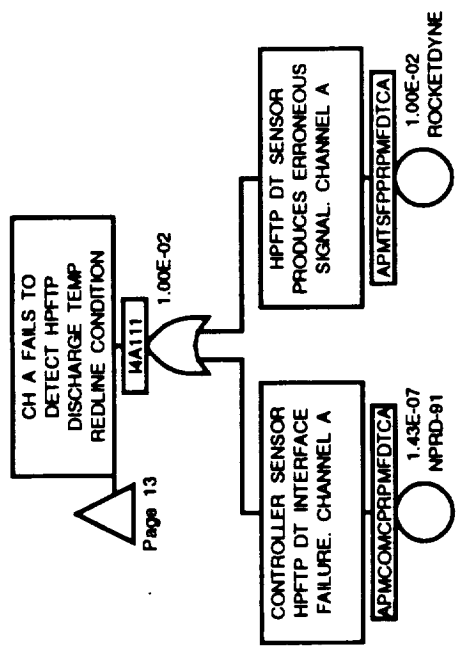




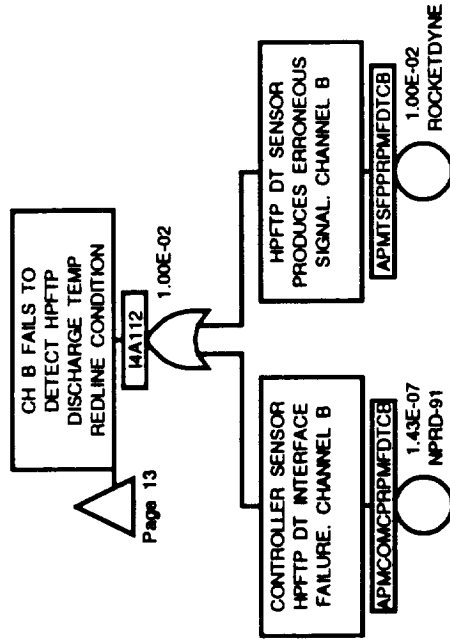


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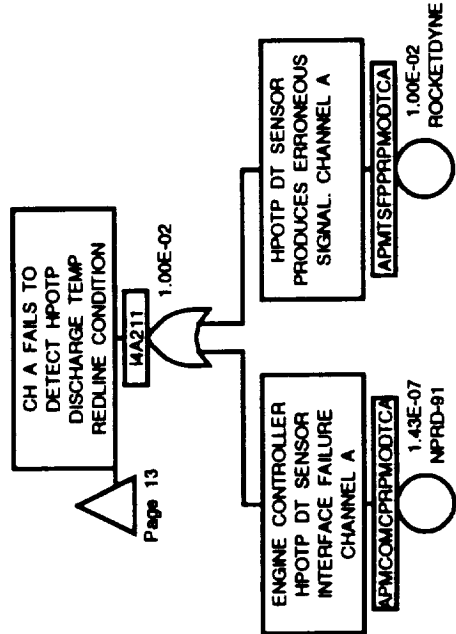




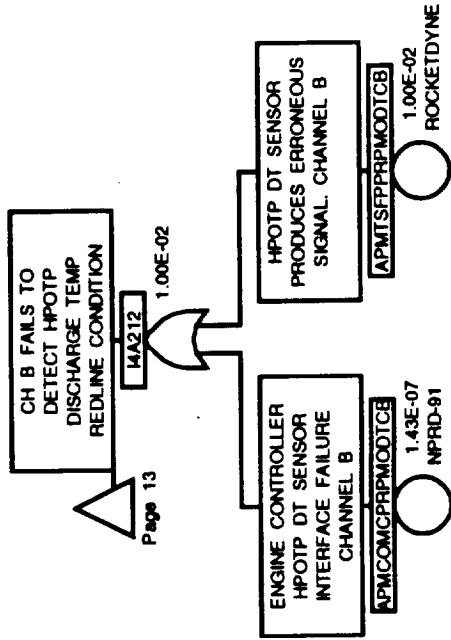
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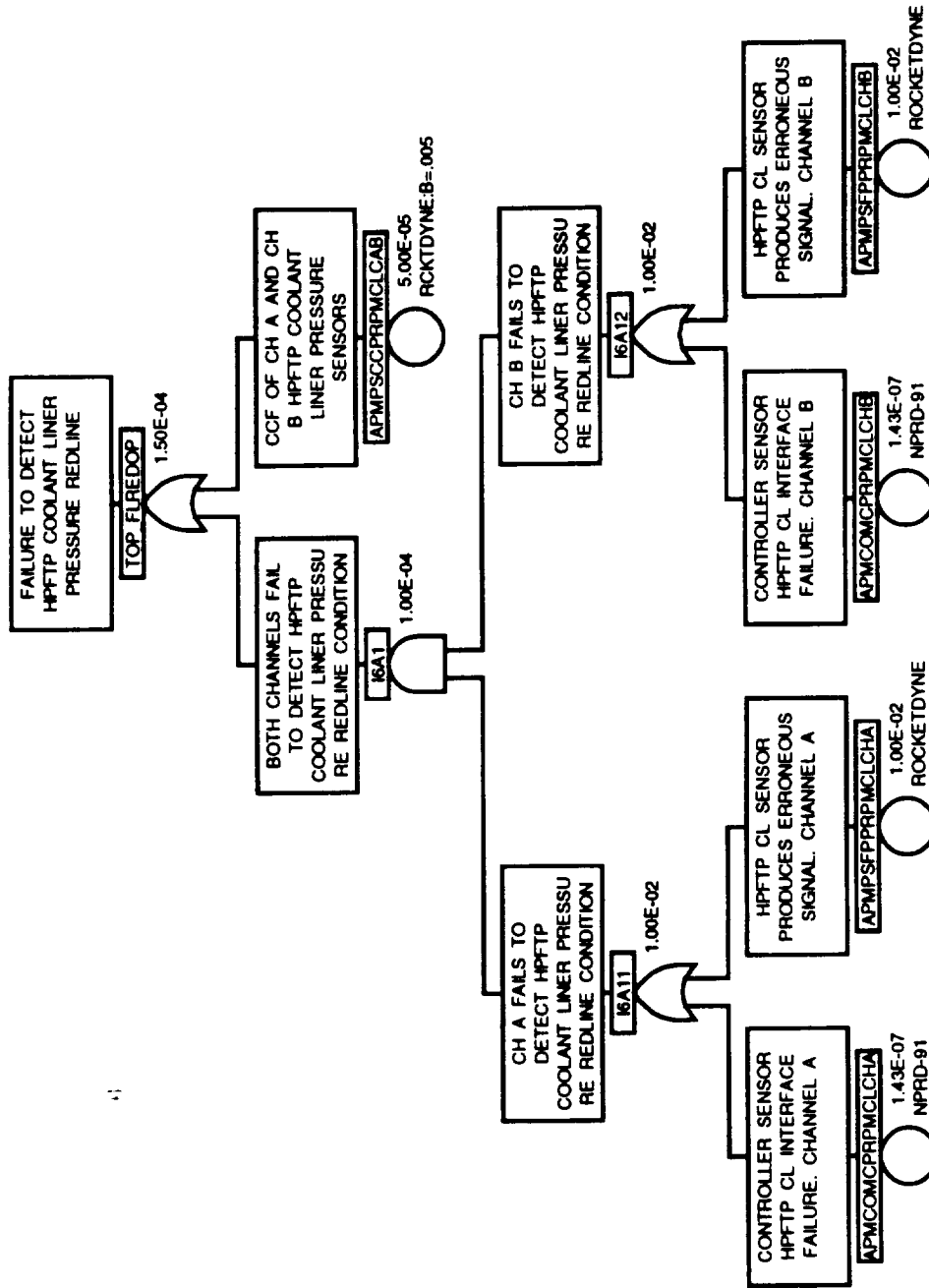
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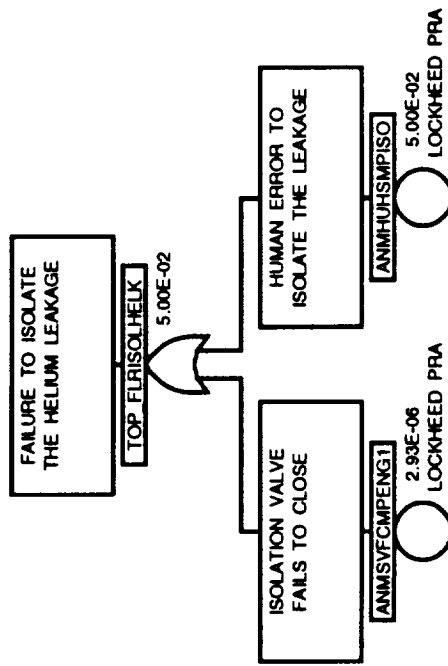
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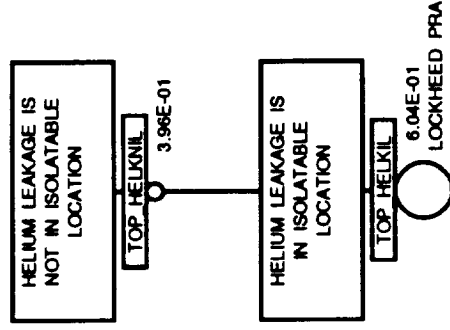


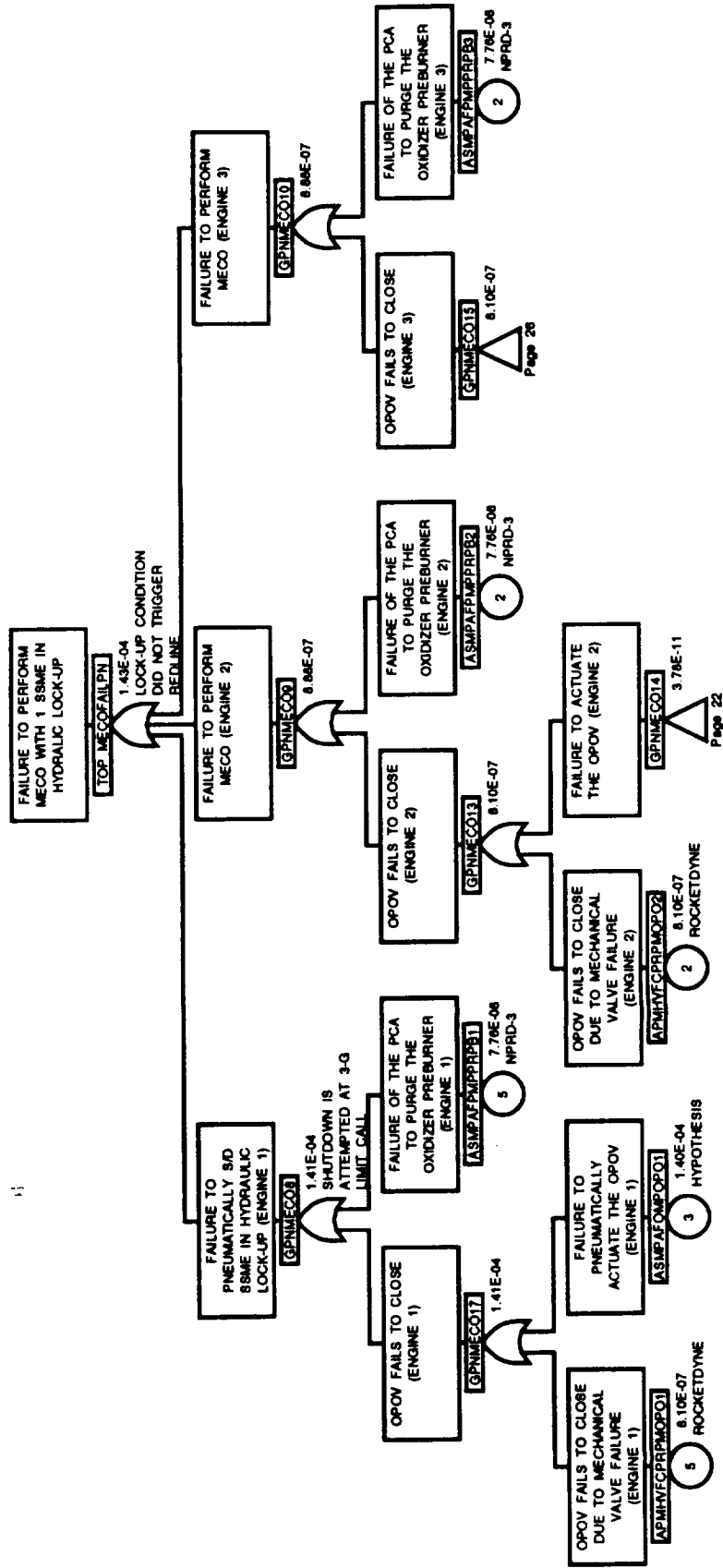
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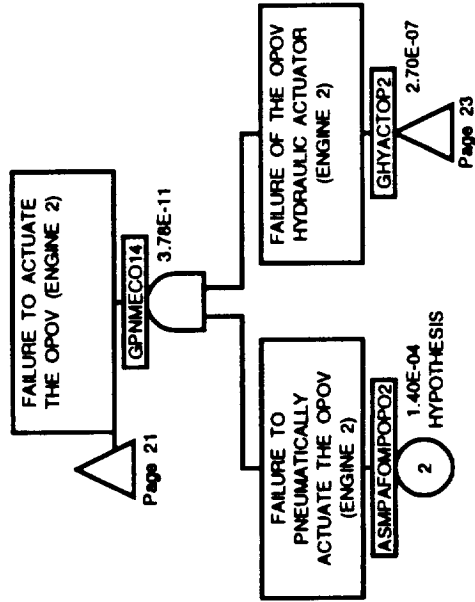


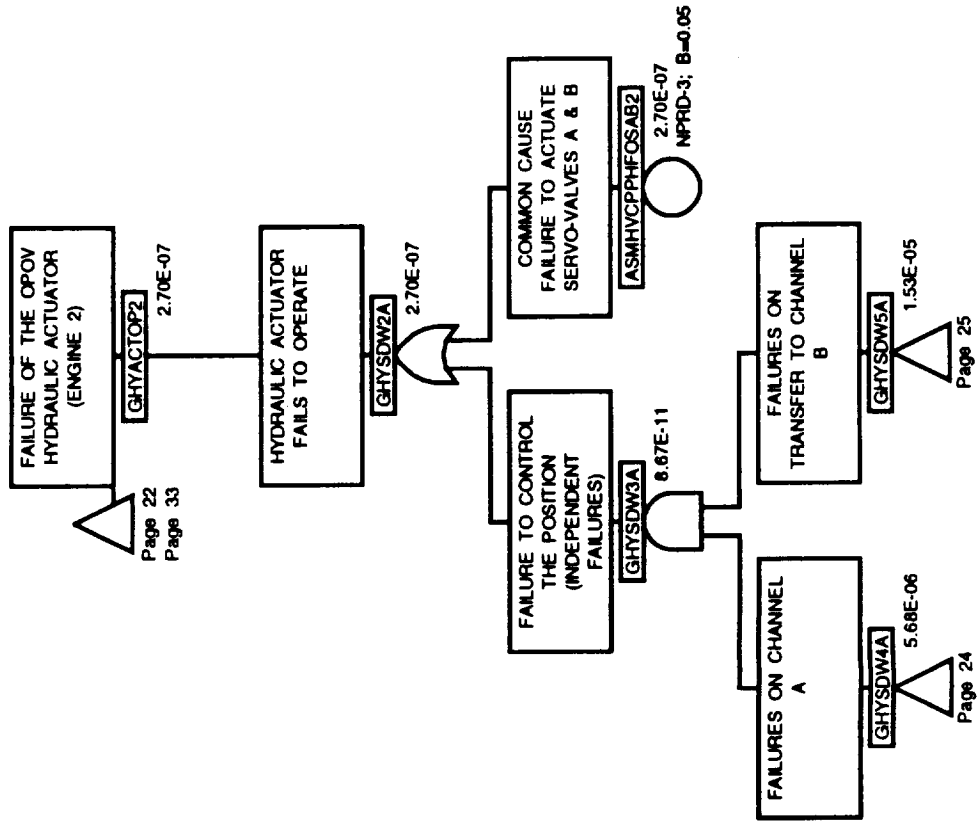


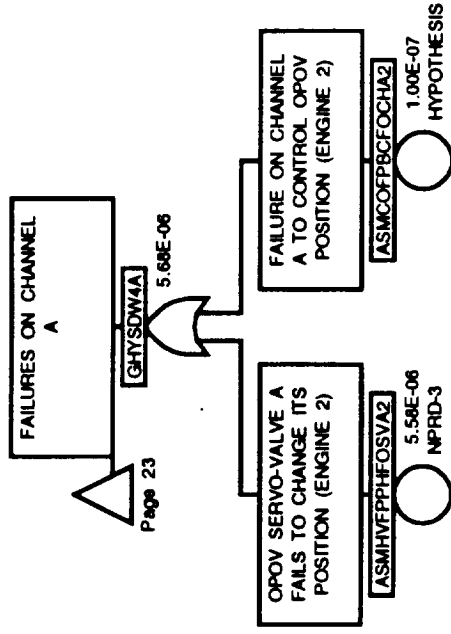




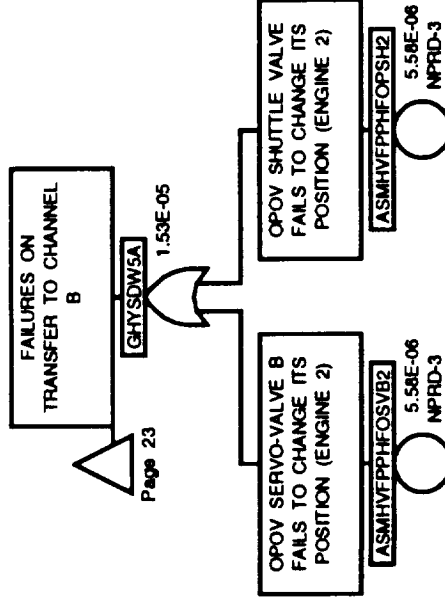




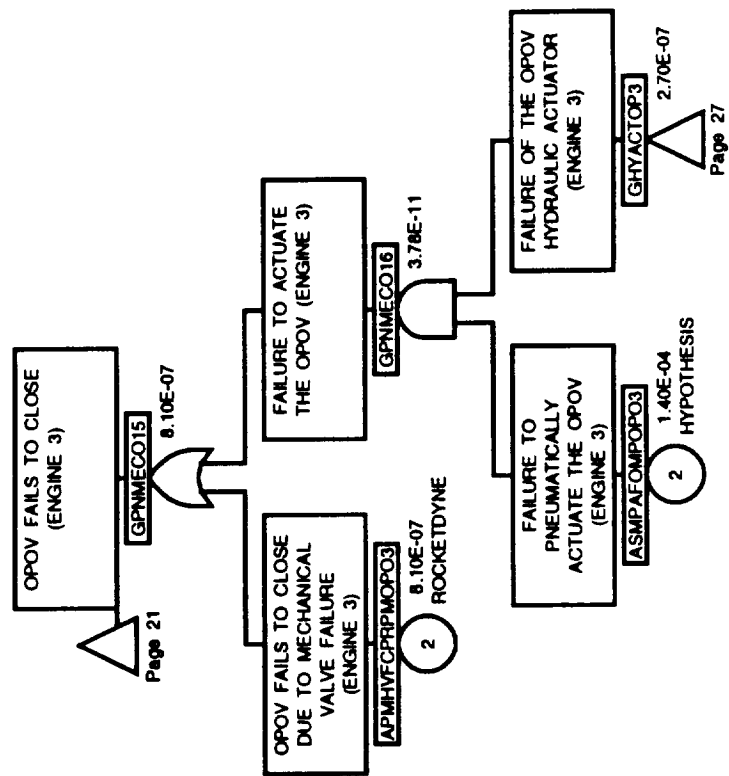




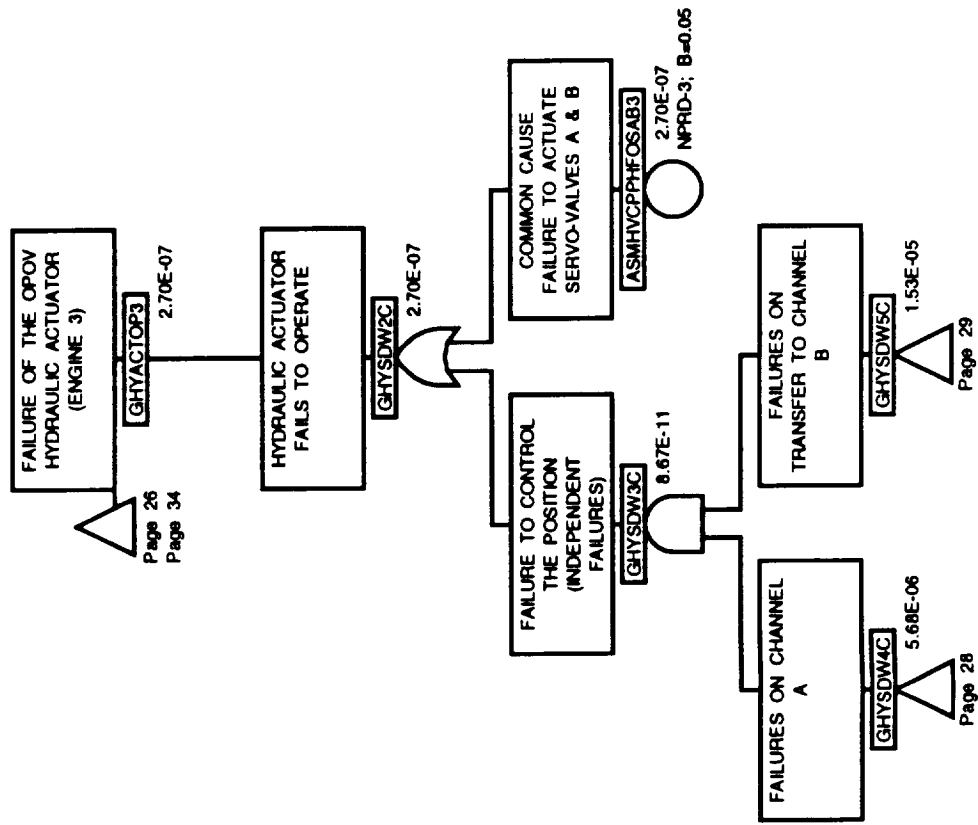
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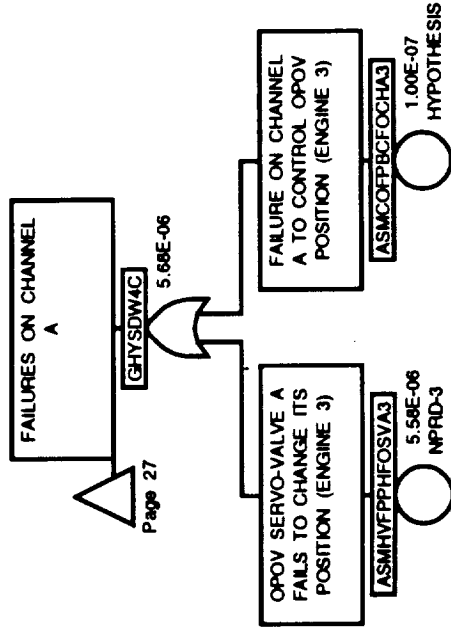


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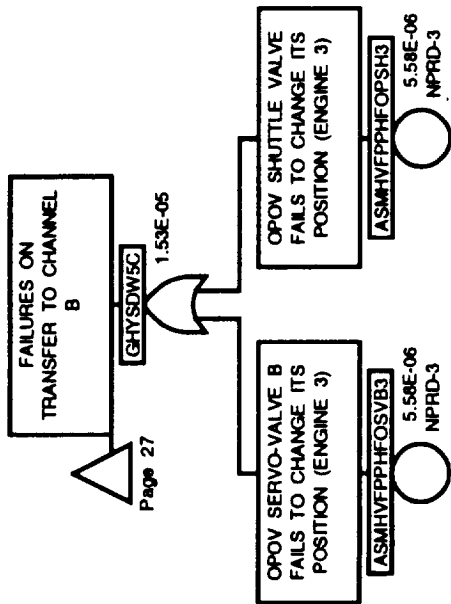


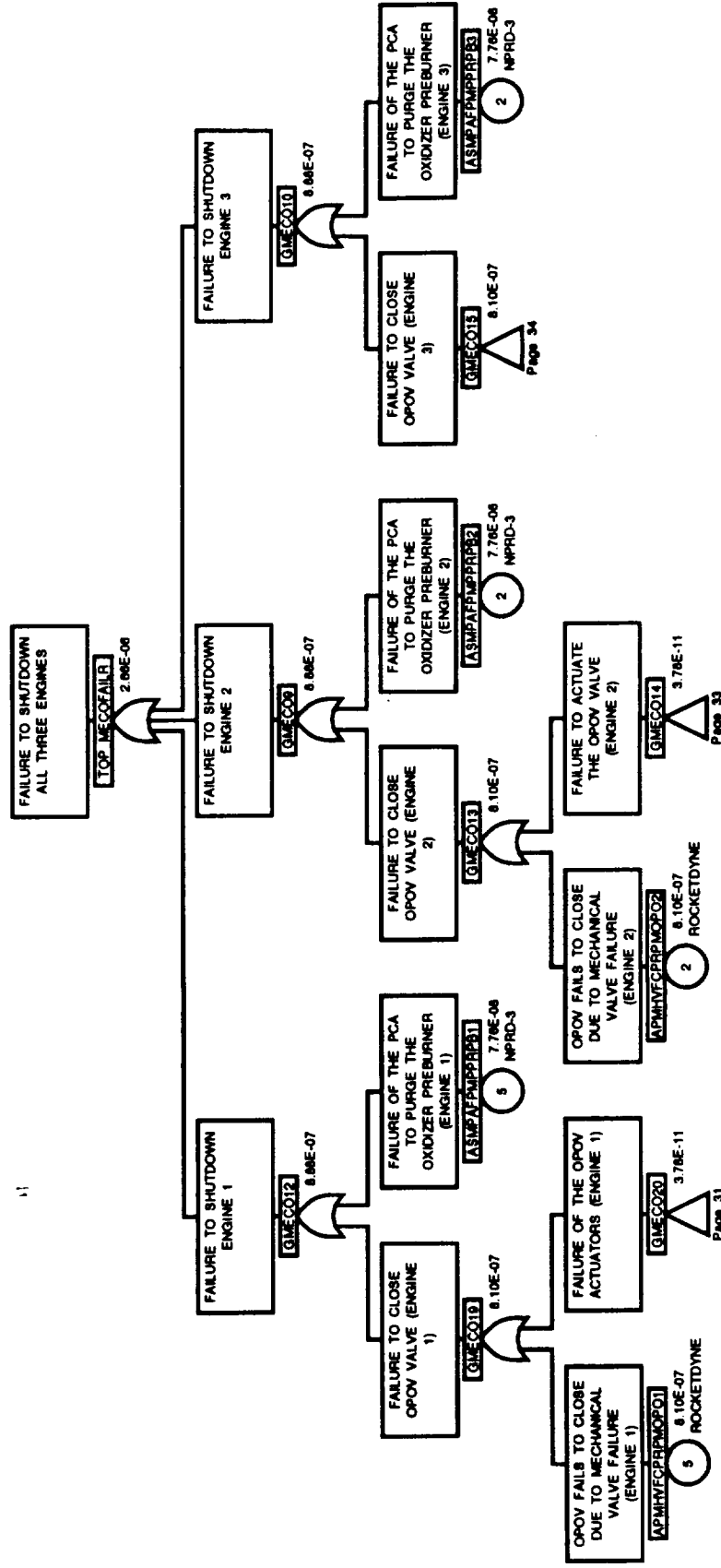


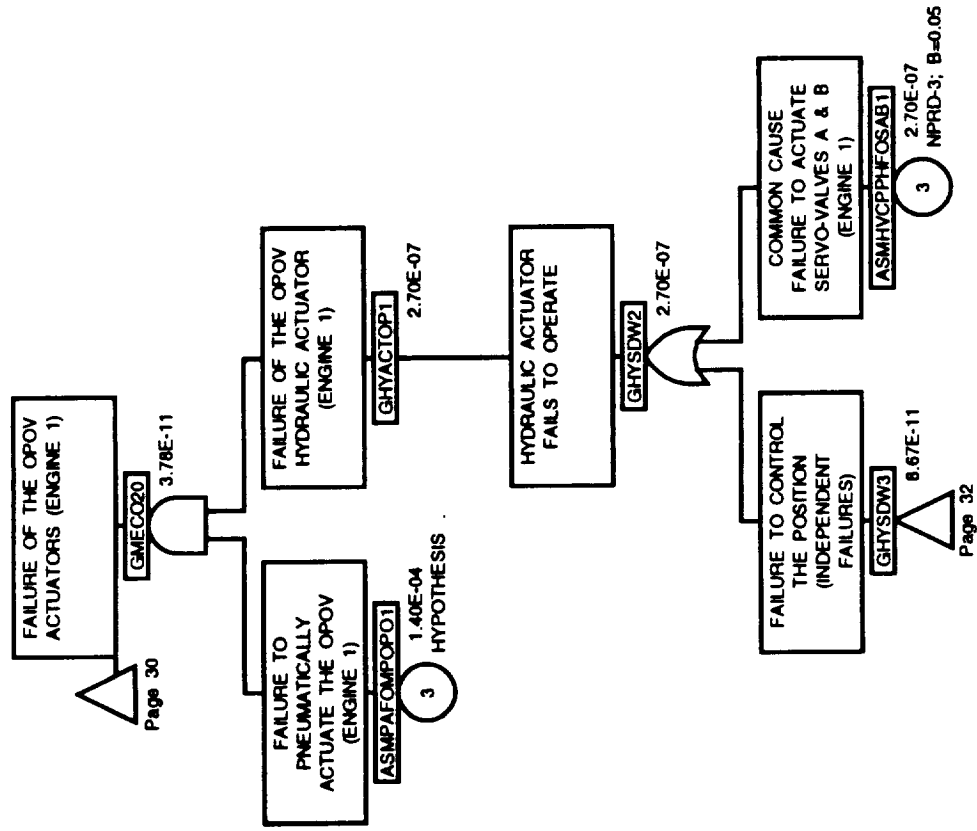




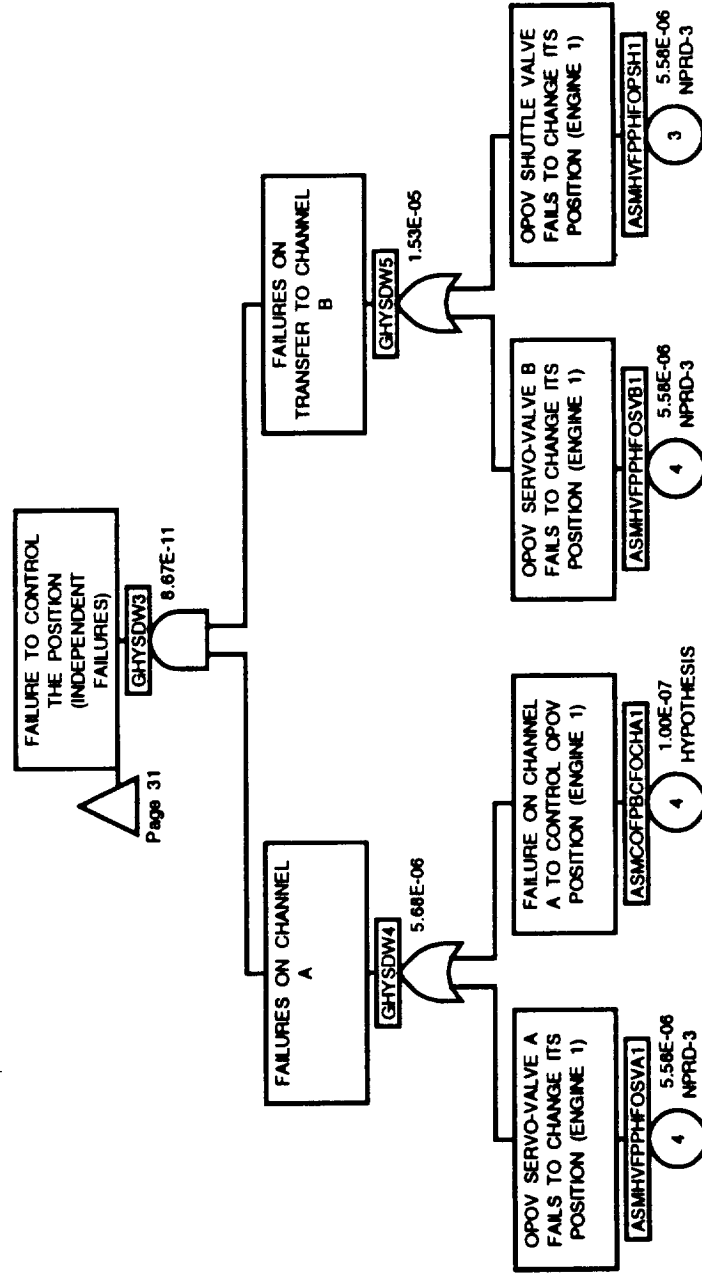
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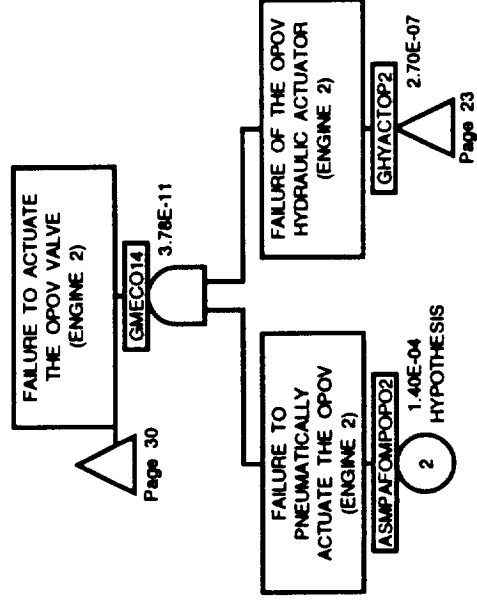




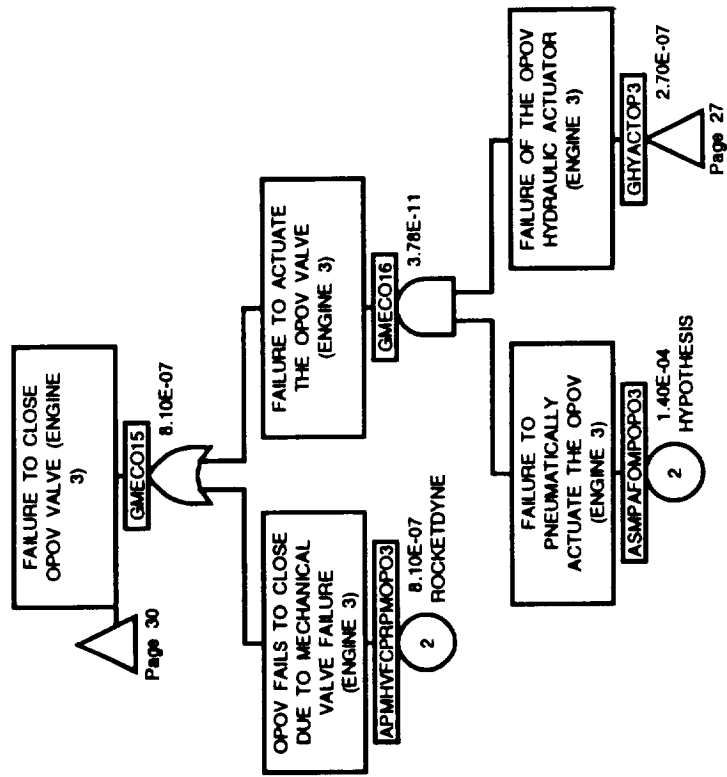


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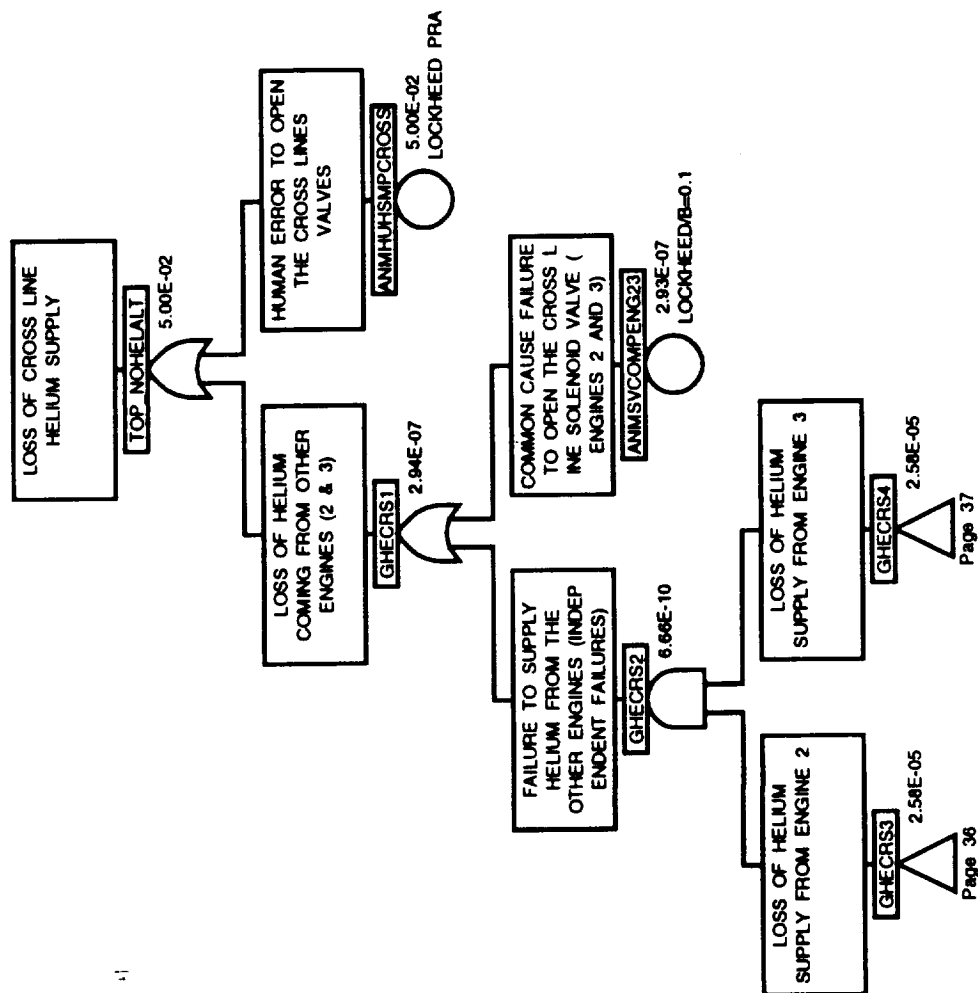


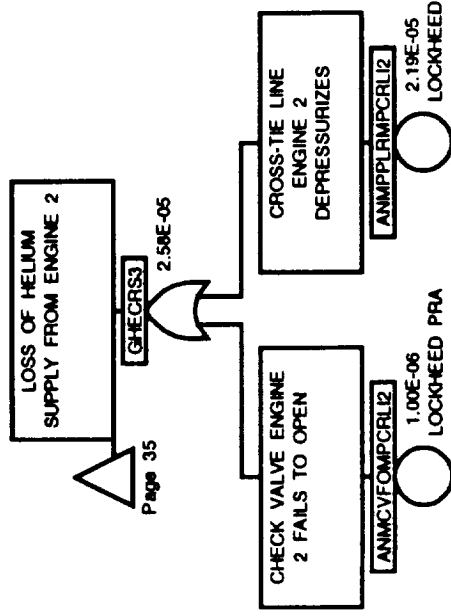


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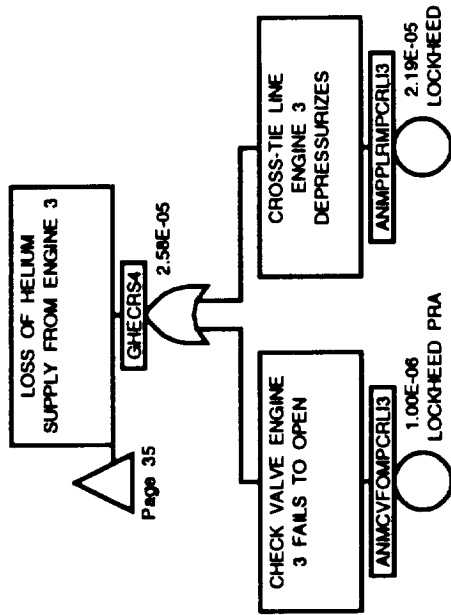


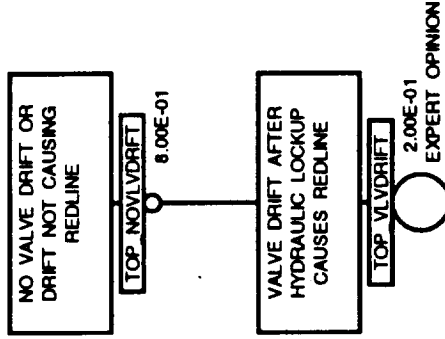


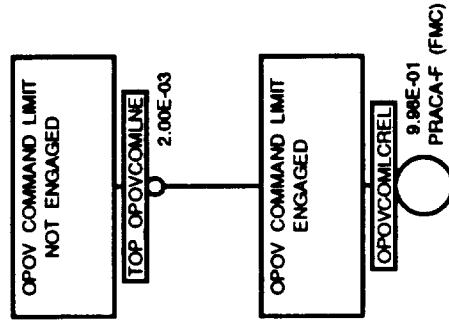


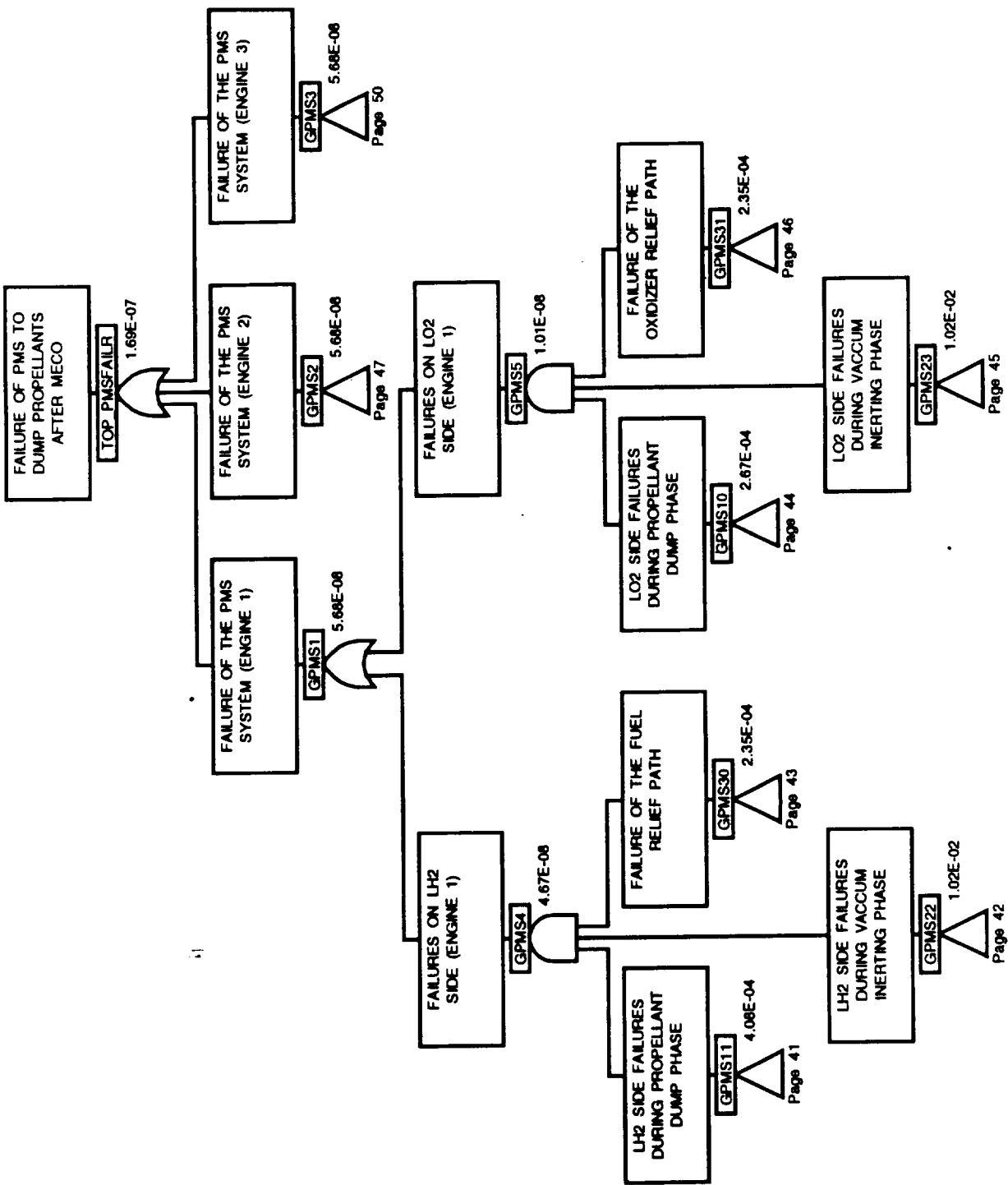


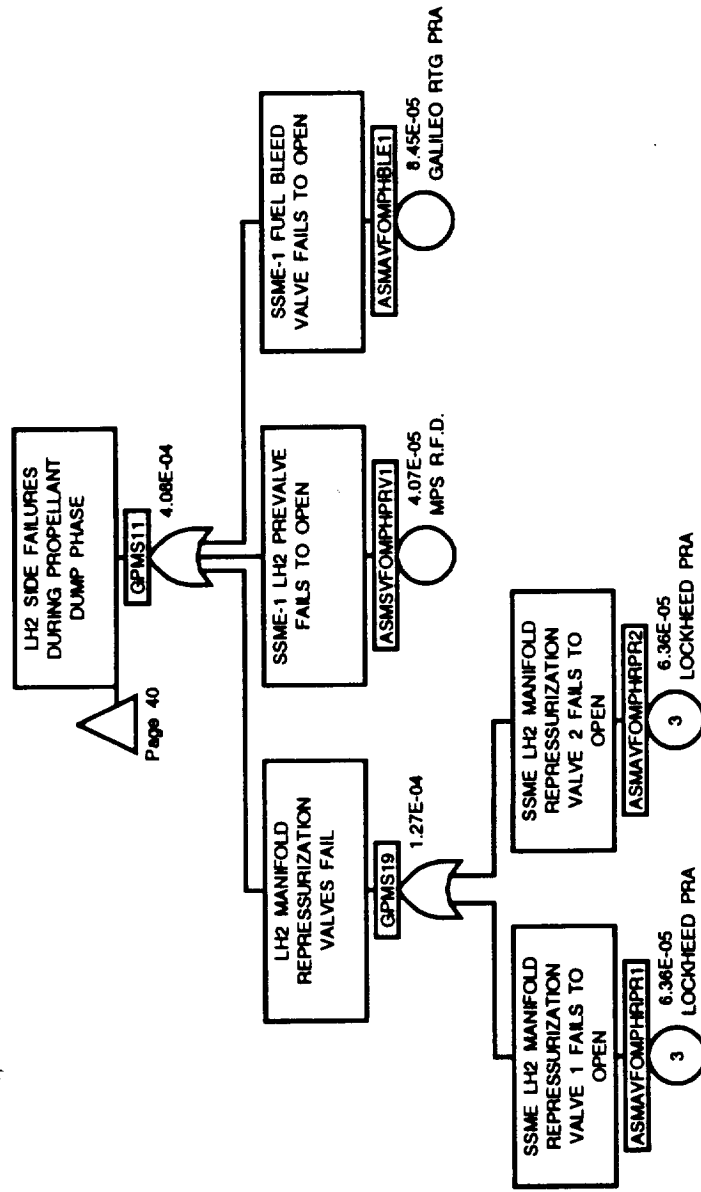
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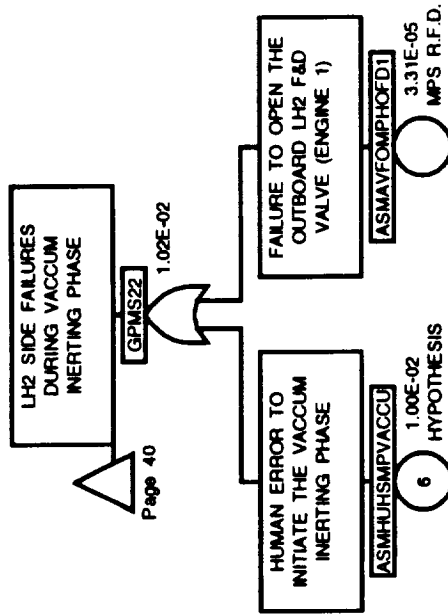






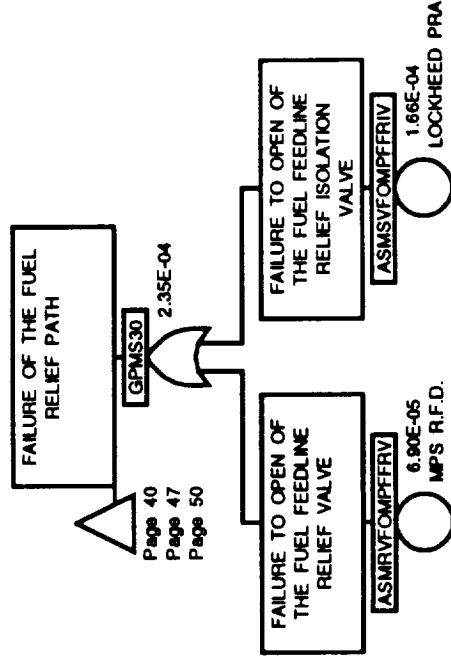


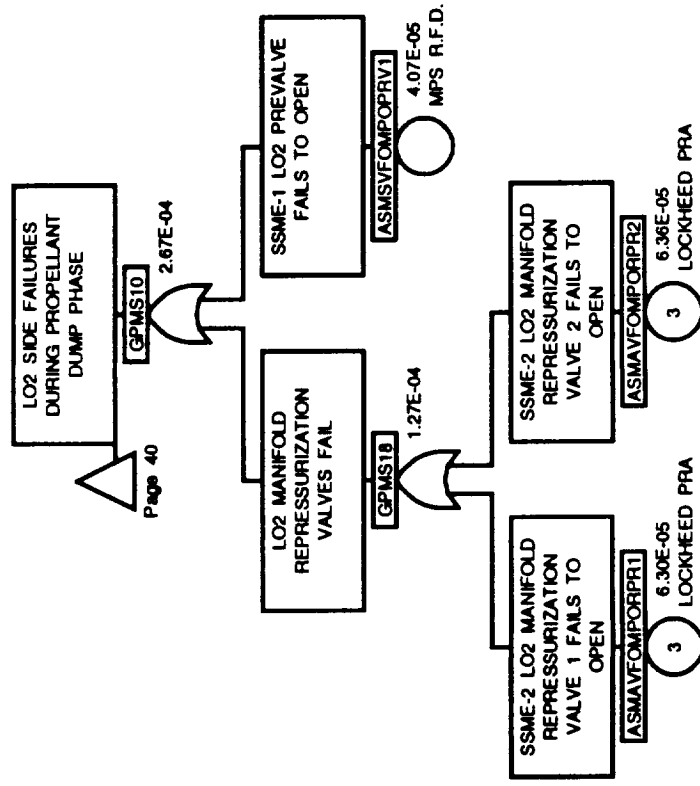
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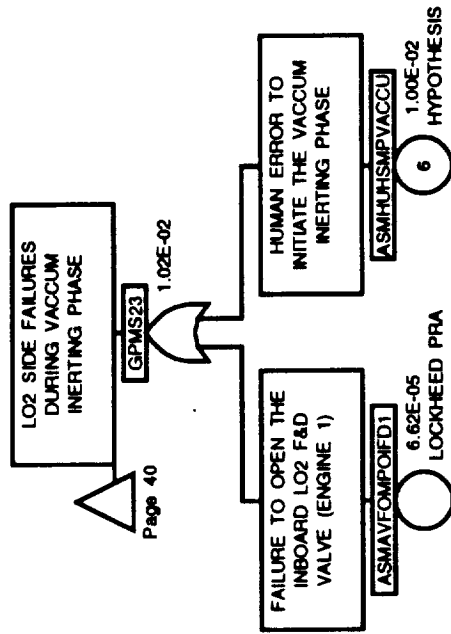
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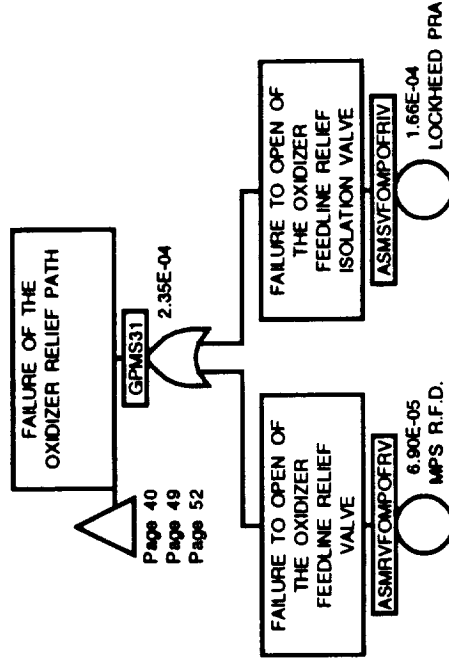




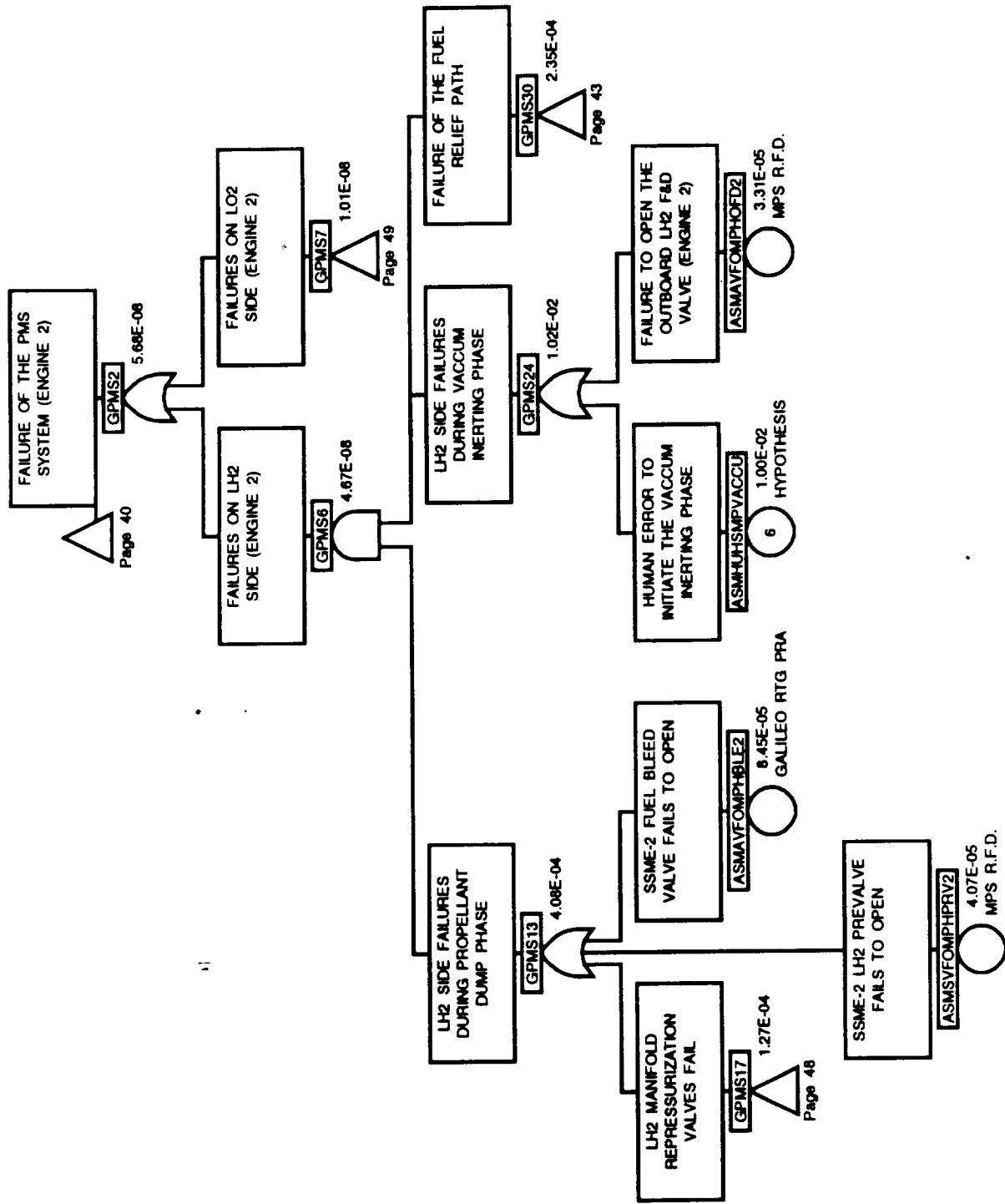
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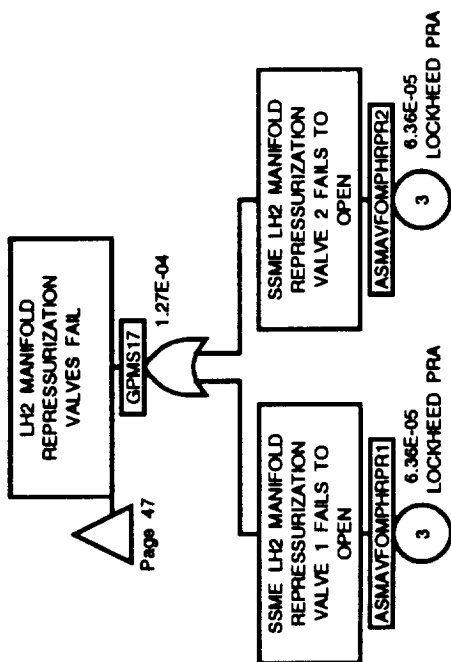


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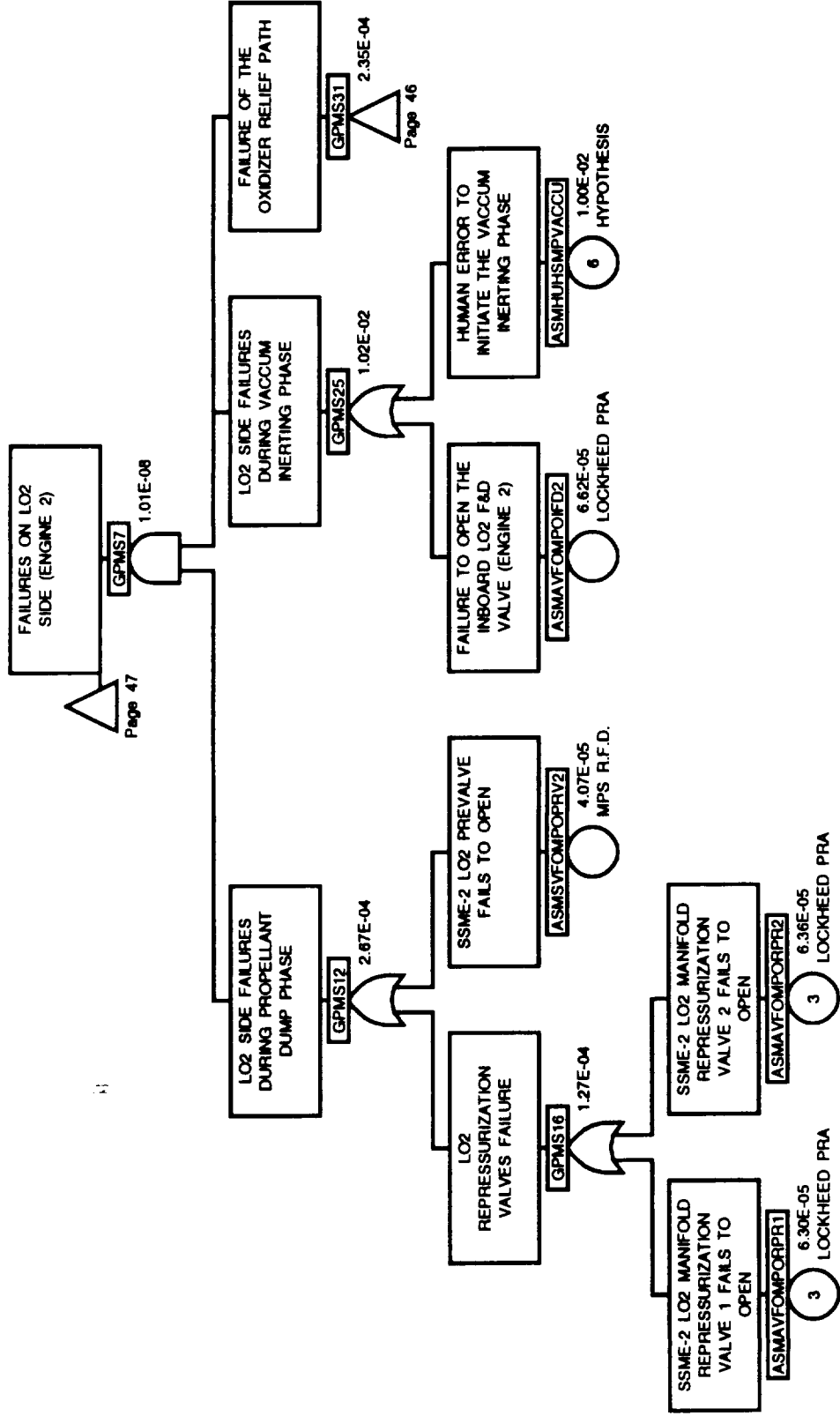


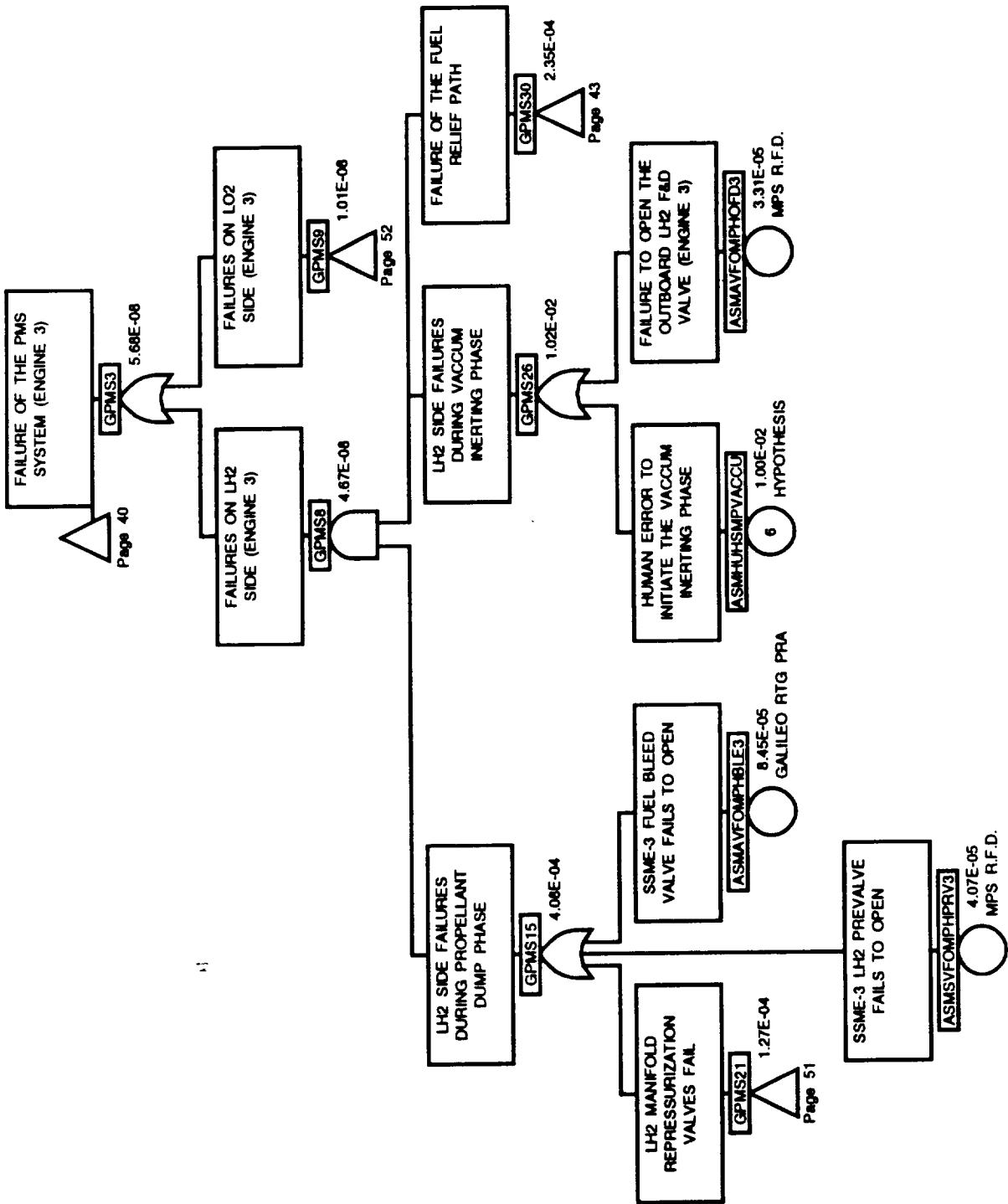
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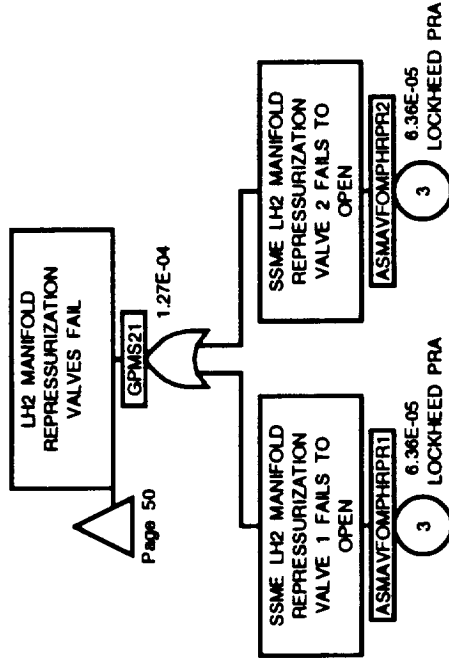


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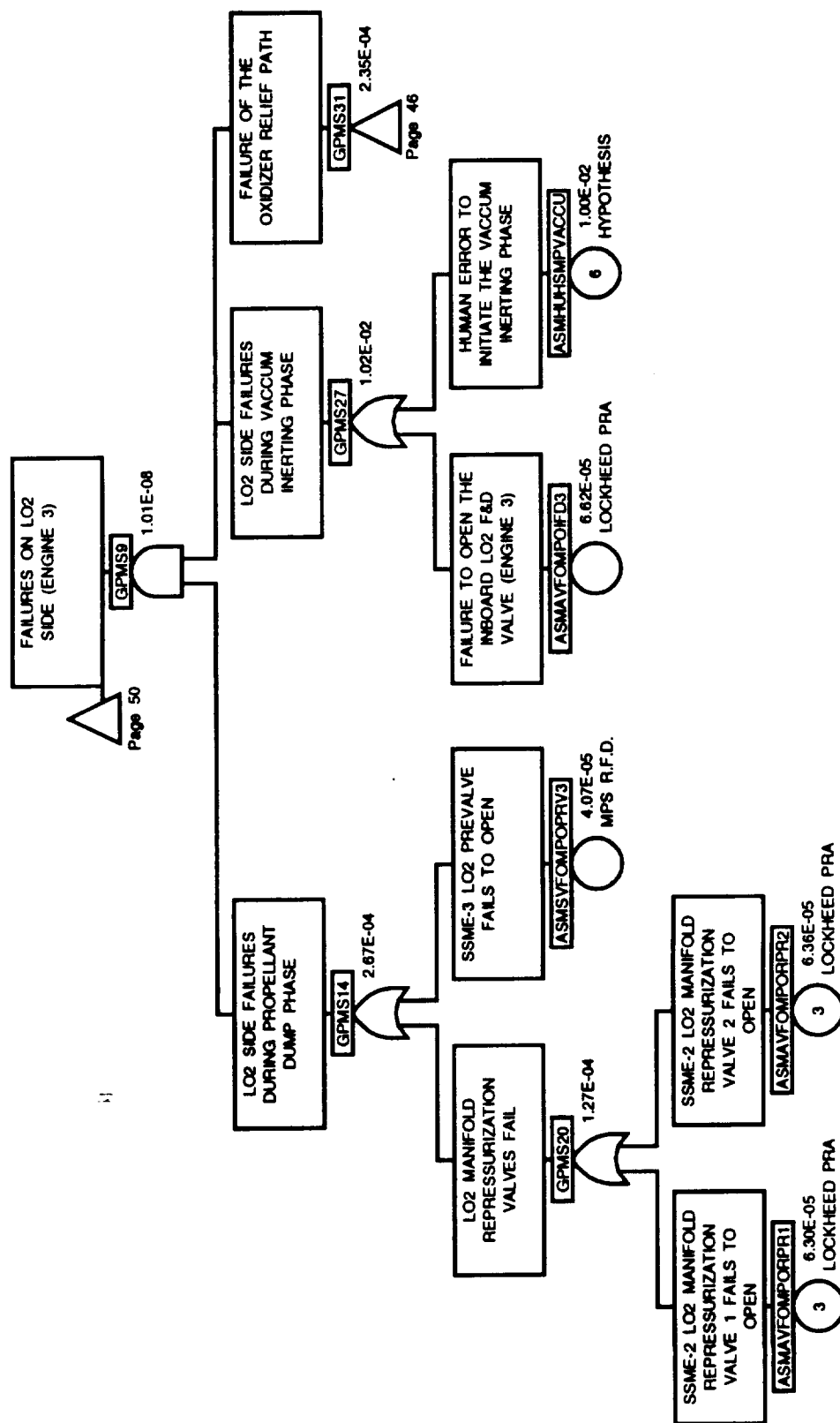


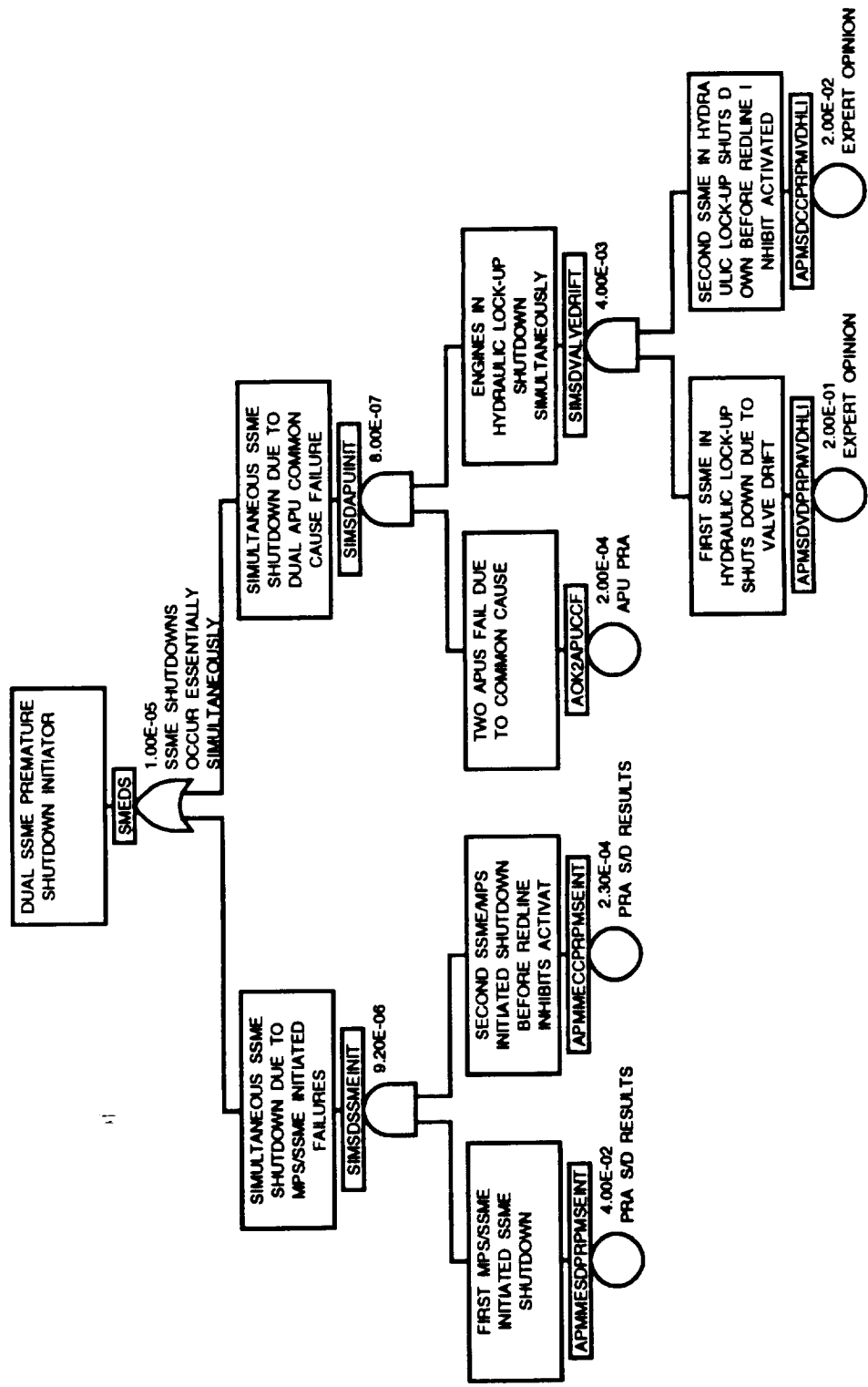


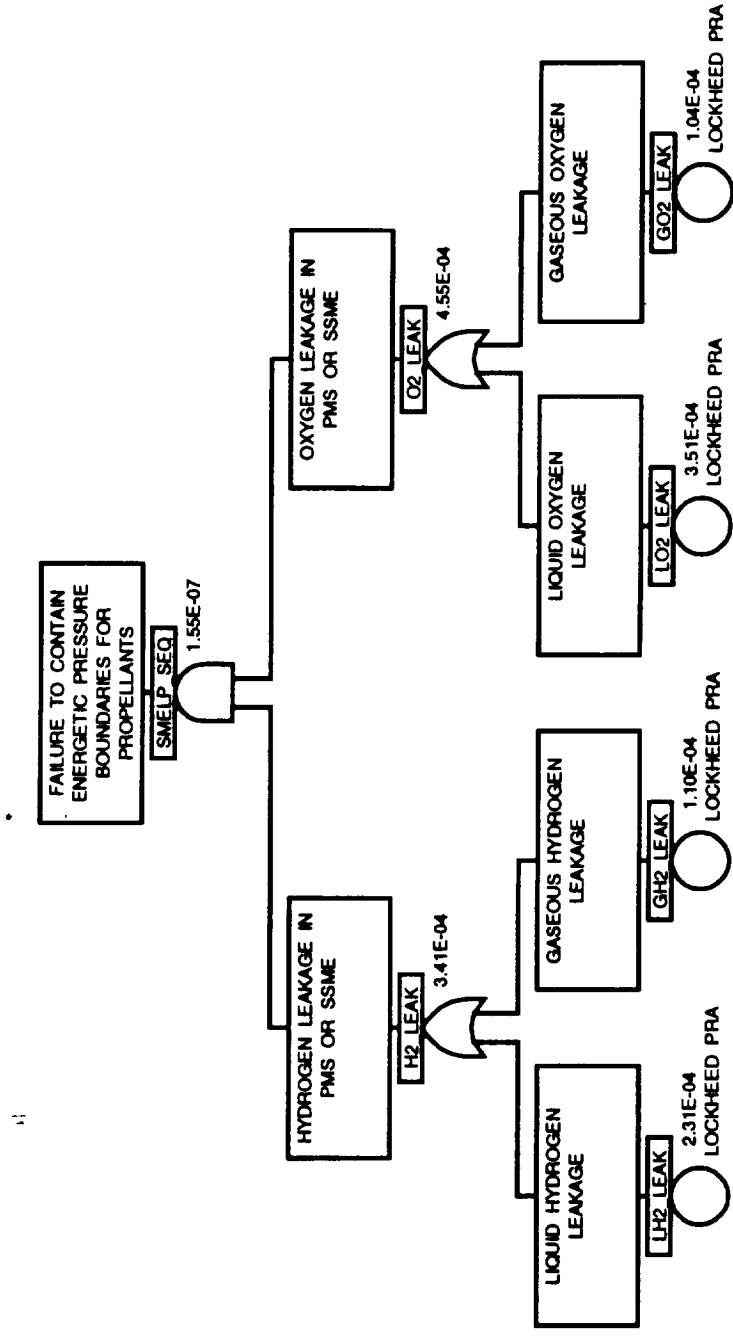


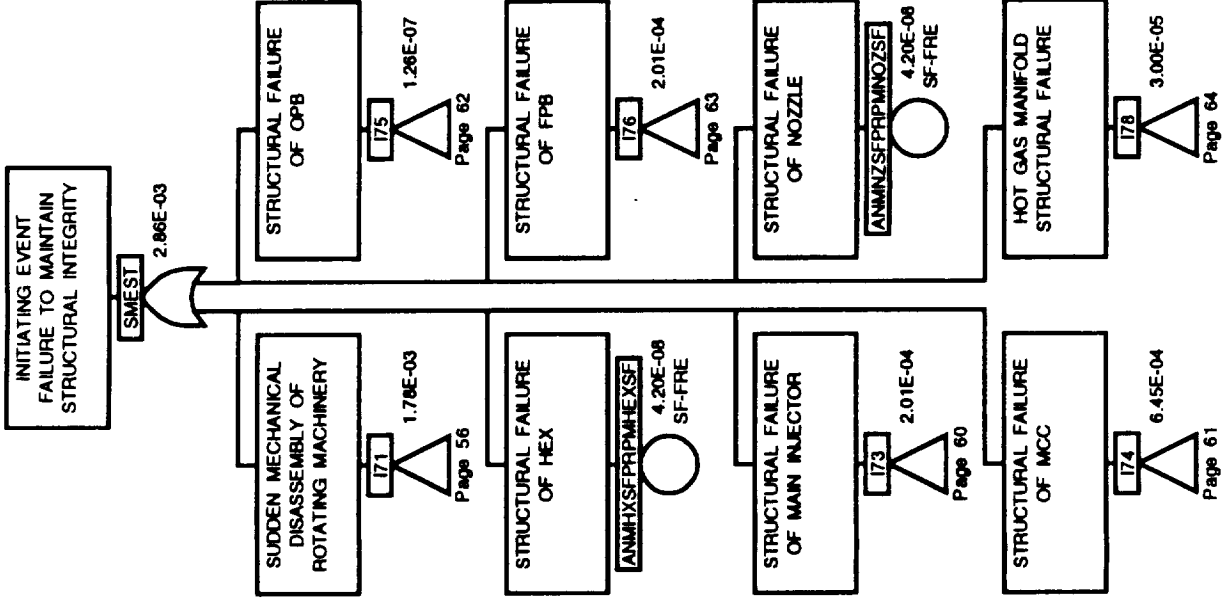


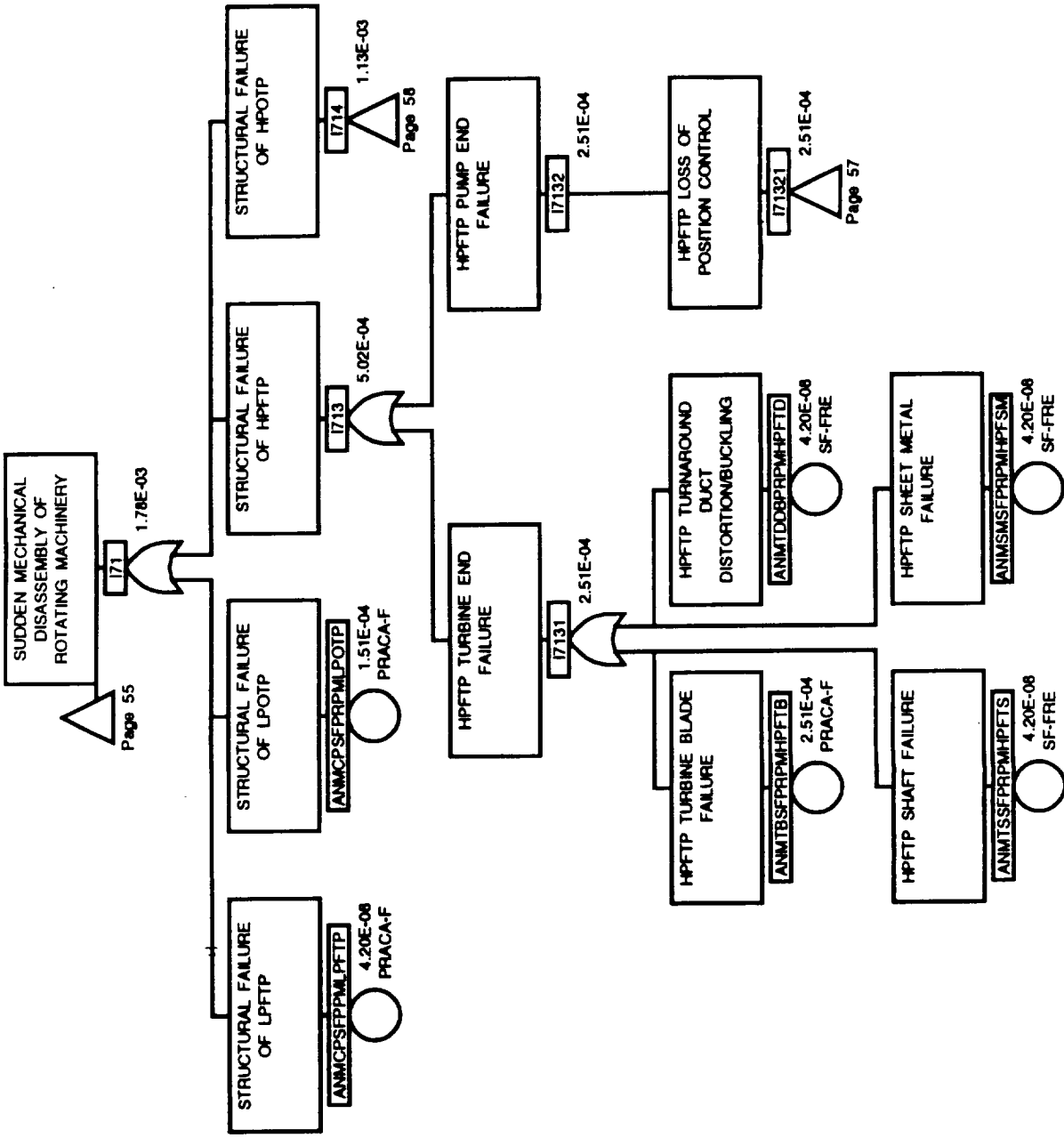
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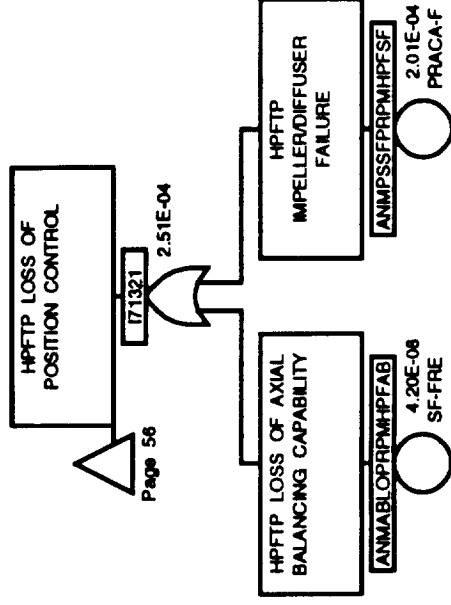


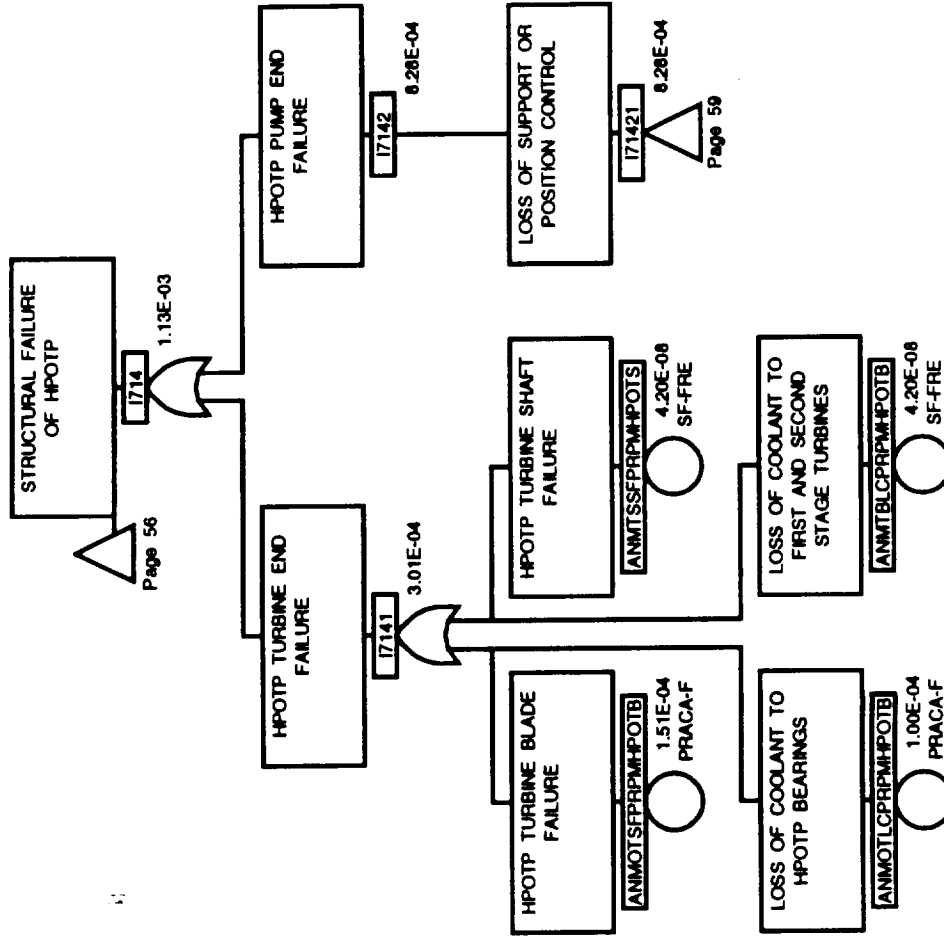




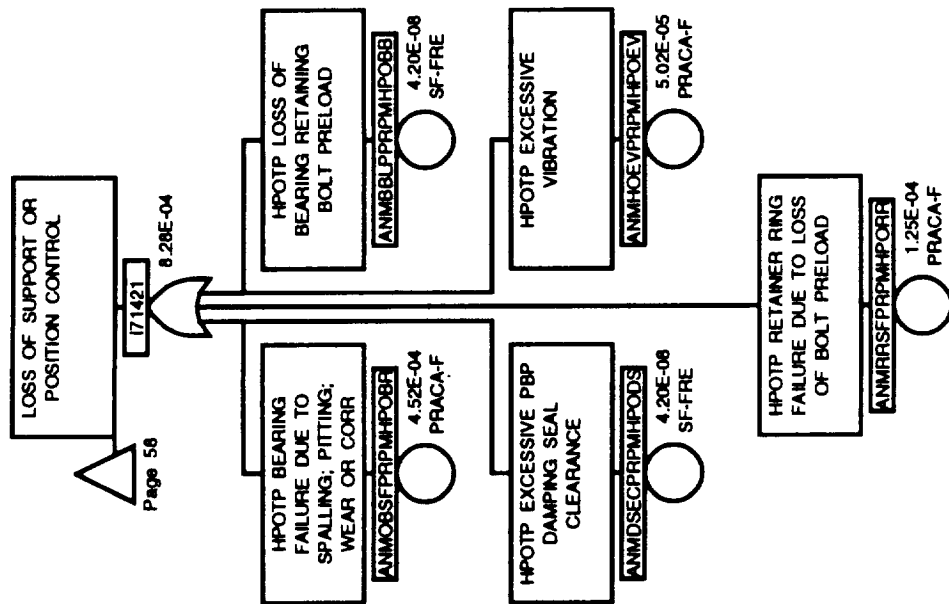


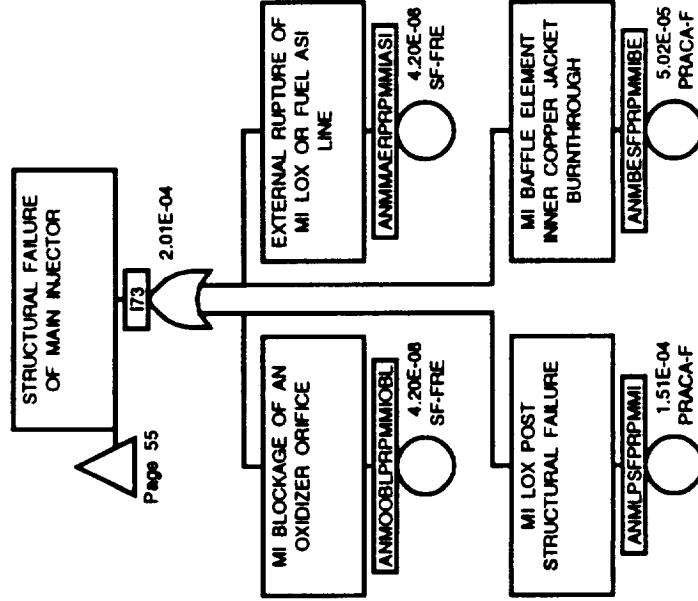


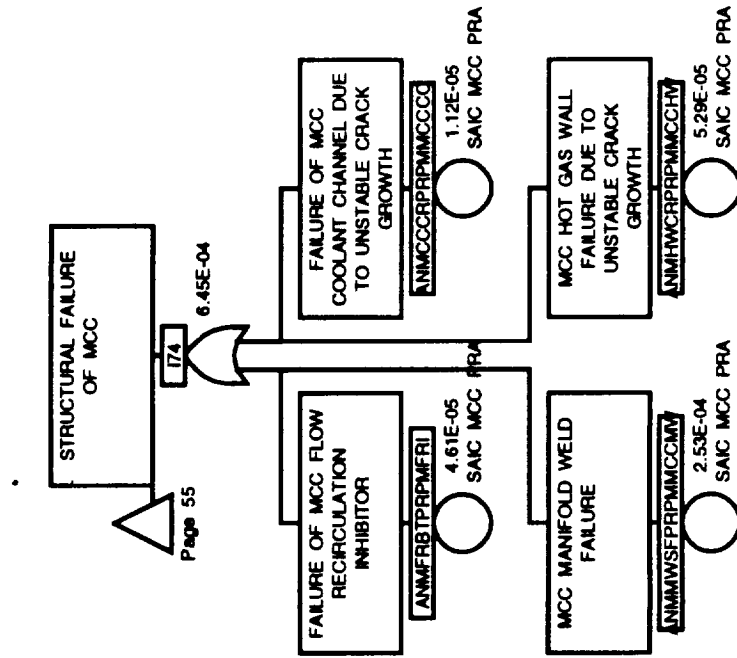


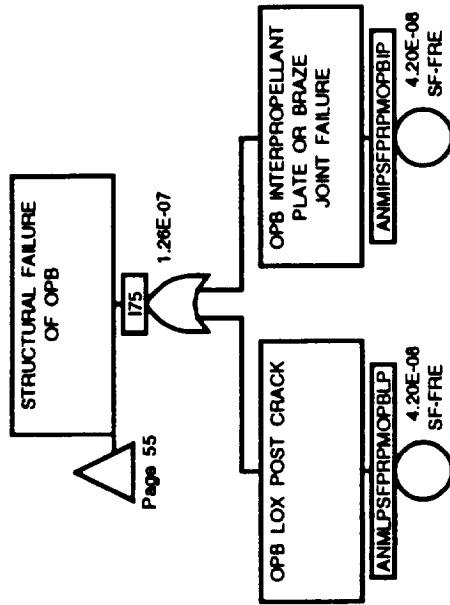


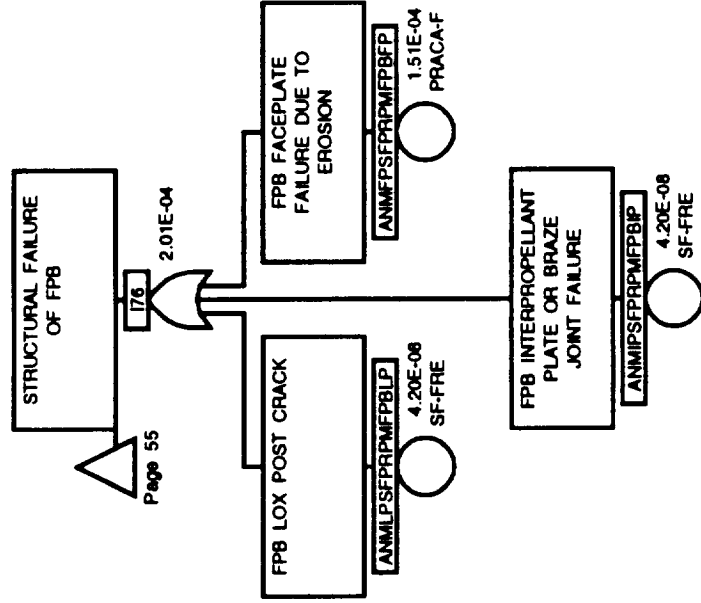






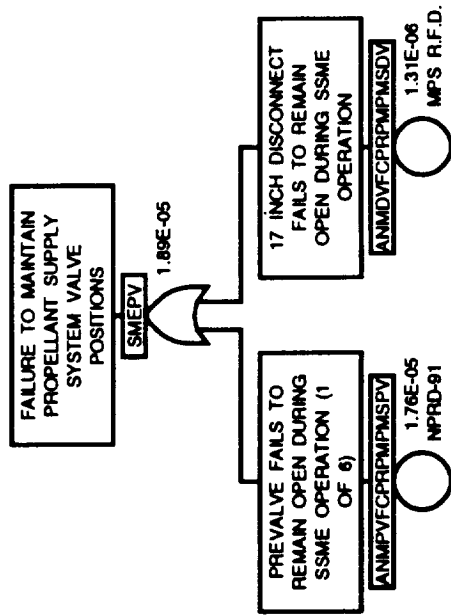


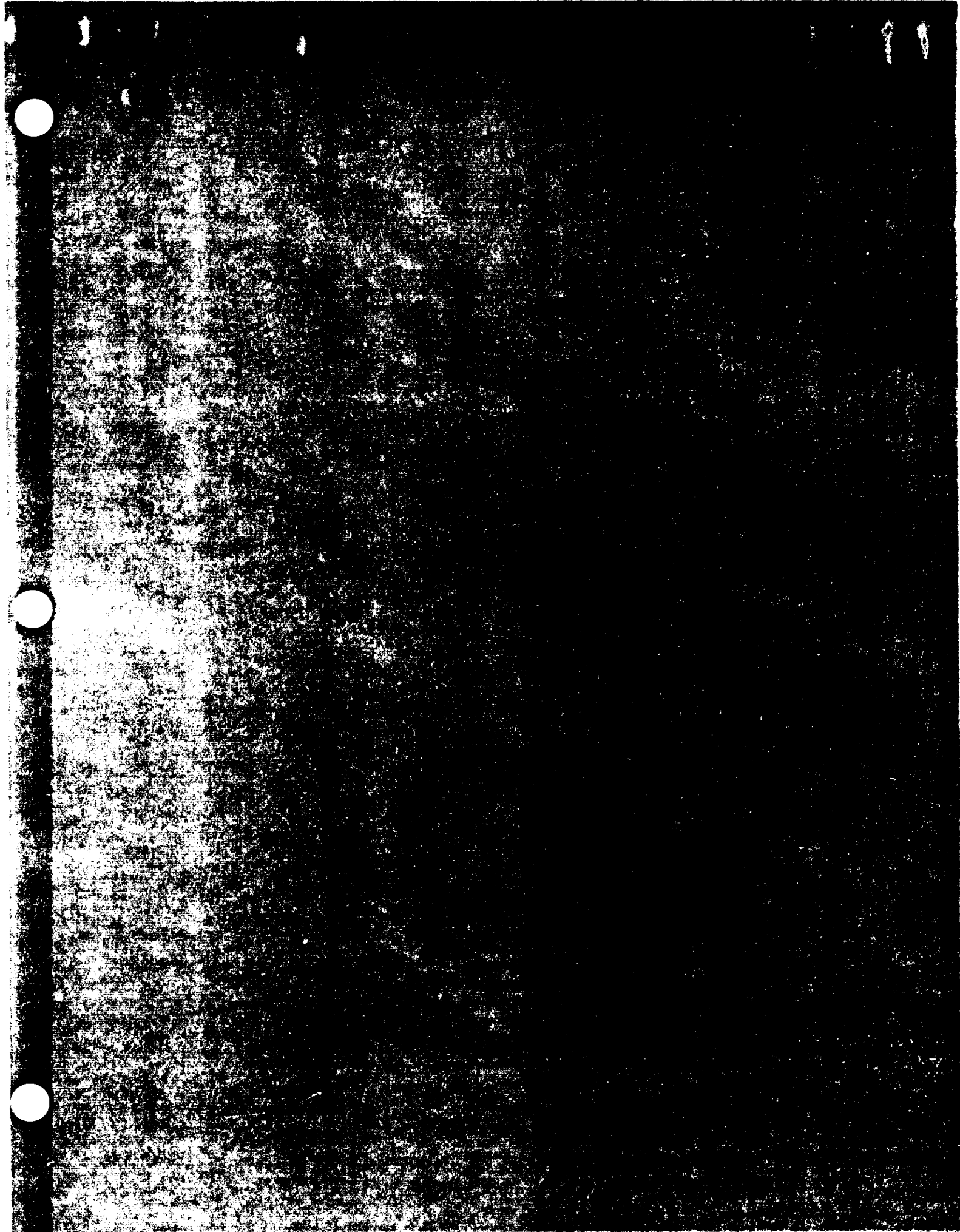




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FUEL TURBINE TEMPERATURE REDLINE  
SENSOR RELIABILITY ASSESSMENT

SENSOR FAILURE DATA - FUEL SIDE ONLY

PART NUMBER	7004-91	7013	TOTAL
TOTAL SECONDS	264,000	158,000	422,000
FAILURES	3	2	5

BOTH PART NUMBERS EXHIBIT THE SAME FAILURE RATE

MISSION RELIABILITY VALUES - SINGLE SENSOR (50%CONFIDENCE)

FAILURE (HIGH OR LOW)	0.993104
FAIL HIGH - DISQUALIFY	0.9943159
FAIL HIGH - VOTE FOR CUTOFF	0.9967419
FAIL LOW - DISQUALIFY	0.9979538

HISTORICAL SSME RELIABILITY DATA

SINGLE ENGINE - 104% MISSION	0.9924918
EXCEED FUEL TURBINE REDLINE	0.9984938

ERRONEOUS SHUTDOWN PROBABILITY

FIRST FAILURE HIGH OR LOW (1 OF 2)	0.0137444
SECOND FAILURE HIGH AND VOTE	0.0032581
COMBINED	4.478E-05
THREE ENGINE PROBABILITY	0.0001343
MTBF	7,440

LOSS OF PROTECTION PROBABILITY

FIRST FAILURE HIGH OR LOW (1 OF 2)	0.0137444
SECOND FAILURE - NO VOTE	0.0056841
COMBINED	7.812E-05
THREE ENGINE PROBABILITY	0.0002344
MTBF	4,270

REDLINE EXCEEDED PROBABILITY

SINGLE ENGINE	0.0015062
THREE ENGINE PROBABILITY	0.0045117
MTBF	220

REDLINE PROVIDES NEEDED PROTECTION

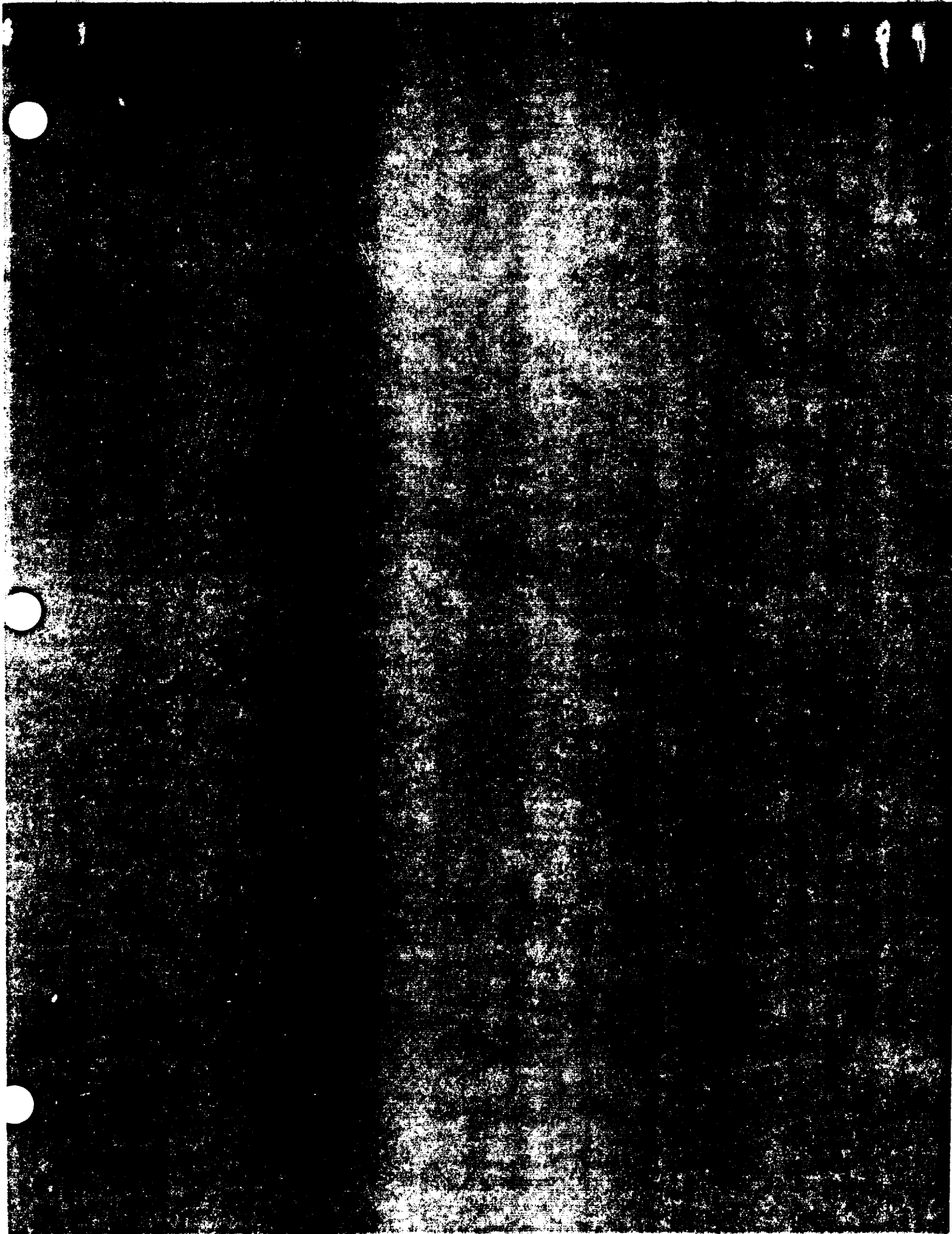
SAFE SHUT DOWN FOR 20 PERCENT OF HISTORICAL FAILURES	
EXPECTED NEED	1 IN 220 FLIGHTS
EXPECTED ERRONEOUS	1 IN 7,440 FLIGHTS
RATIO	34 TO 1

SENSOR CATASTROPHIC POTENTIAL

LOSS OF REDLINE	7.812E-05
ENGINE EXCEEDS REDLINE	0.0015062
COMBINED	1.177E-07
THREE ENGINE PROBABILITY	3.53E-07
MTBF	2,832,780

ERRONEOUS SHUTDOWN (3 ENGINES)	0.0001343
SECOND ENGINE SHUTDOWN	0.0075082
COMBINED	1.009E-06
MTBF	991,450

UNABLE TO ASSESS ORBITER ABORT RISK



## CUTOFF CODES

CODE	ID	DESCRIPTION
CADS	1	COMMAND AND DATA SIMULATOR COMMAND (SIMULATES ORBITER COMPUTER)
CADS ELU	2	CADS - ELECTRONIC LOCKUP
CADS FTD	3	CADS - HPFTP TURBINE DISCHARGE TEMPERATURE REDLINE LOST
CONT	4	ENGINE CONTROLLER INITIATED
CONT FD	5	CONTROLLER - FUEL DENSITY (OBSOLETE)
CONT IEA	6	CONTROLLER - INPUT ELECTRONICS CHANNEL A
ENG RDY	7	LOSS OF ENGINE READY
F SPD IC	8	HPFTP SPEED IGNITION CONFIRM
F TD T	9	HPFTP TURBINE DISCHARGE TEMPERATURE
F TD T E	10	HPFTP TURBINE DISCHARGE TEMPERATURE - ERRONEOUS
F TI T	11	HPFTP TURBINE INLET TEMPERATURE (OBSOLETE)
FAC	12	FACILITY INITIATED CUTOFF (NOT AN ENGINE PROBLEM)
FAC E	13	FACILITY INITIATED CUTOFF - ERRONEOUS
H2O PR	14	FACILITY WATER PRESSURE
HEX DP	15	HEAT EXCHANGER DELTA PRESSURE (OBSOLETE)
HEX PR	16	HEAT EXCHANGER PRESSURE (OBSOLETE)
HEX PR E	17	HEAT EXCHANGER PRESSURE - ERRONEOUS
HF ACC	18	HPFTP ACCELEROMETERS
HF ACC A	19	HPFTP ACCELEROMETERS - AXIAL (OBSOLETE)
HF ACC E	20	HPFTP ACCELEROMETERS - ERRONEOUS
HF ACC N	21	HPFTP ACCELEROMETERS - NON STANDARD MONITOR (OBSOLETE)
HF SPD	22	HPFTP SPEED (OBSOLETE)
HGM	23	HOT GAS MANIFOLD DELTA PRESSURE
HO ACC	24	HPOTP ACCELEROMETERS
HO ACC A	25	HPOTP ACCELEROMETERS - AXIAL (OBSOLETE)
HO ACC C	26	HPOTP ACCELEROMETERS - CROSSFEED FROM HPFTP
HO ACC E	27	HPOTP ACCELEROMETERS - ERRONEOUS
HO ACC N	28	HPOTP ACCELEROMETERS - NON STANDARD MONITOR (OBSOLETE)
HO BRG T	29	HPOTP BEARING COOLANT TEMPERATURE
HO SPD	30	HPOTP SPEED (OBSOLETE)
HO SPD E	31	HPOTP - ERRONEOUS
INJ ACC	32	MAIN INJECTOR ACCELEROMETERS
LF ACC	33	LPFTP ACCELEROMETERS
LF ACC E	34	LPFTP ACCELEROMETERS - ERRONEOUS
LO ACC E	35	LPOTP ACCELEROMETERS - ERRONEOUS
LOX T E	36	HPOTP LOX DISCHARGE TEMP RISE - ERRONEOUS (OBSOLETE)
LPF TURB	37	LPFTP TURBINE INLET PRESSURE (OBSOLETE)
MCC	38	MCC LINER CAVITY PRESSURE
MCC ACC E	39	MAIN COMBUSTION CHAMBER ACCELEROMETERS - ERRONEOUS
MCC PC	40	MAIN CHAMBER PRESSURE
MCF ACT	41	MAJOR COMPONENT FAIL REPORT - ACTUATOR
MCF CL	42	MCF - COMMAND LIMIT
MCF DCU	43	MCF - DIGITAL COMPUTER UNIT
MCF FD	44	MCF - FUEL DENSITY
MCF FTD	45	MCF - HPFTP TURBINE DISCHARGE TEMPERATURE
MCF FM	46	MCF - FUEL FLOWMETER
MCF OTD	47	MCF - HPOTP TURBINE DISCHARGE TEMPERATURE
MCF PC	48	MCF - MAIN CHAMBER PRESSURE
MOV ACC	49	MAIN OXIDIZER VALVE ACCELEROMETER (OBSOLETE)
O DR DP	50	HPOTP PRIMARY OXIDIZER SEAL DRAIN DELTA PRESSURE (OBSOLETE)
O DR P	51	HPOTP PRIMARY OXIDIZER SEAL DRAIN PRESSURE (OBSOLETE)
O DR P E	52	HPOTP PRIMARY OXIDIZER SEAL DRAIN PRESSURE - ERRONEOUS
O DR T	53	HPOTP PRIMARY OXIDIZER SEAL DRAIN TEMPERATURE (OBSOLETE)
O IS PRG	54	HPOTP INTERMEDIATE SEAL PURGE PRESSURE
O ISCP	55	HPOTP INTERMEDIATE SEAL CAVITY DELTA PRESSURE (OBSOLETE)
O ISCP	56	HPOTP INTERMEDIATE SEAL CAVITY PRESSURE (OBSOLETE)
O ISCP E	57	HPOTP INTERMEDIATE SEAL CAVITY PRESSURE ERRONEOUS
O TD T	58	HPOTP TURBINE DISCHARGE TEMPERATURE
O TD T E	59	HPOTP TURBINE DISCHARGE TEMPERATURE - ERRONEOUS
O TI T	60	HPOTP TURBINE INLET TEMPERATURE (OBSOLETE)
O TI T E	61	HPOTP TURBINE INLET TEMPERATURE - ERRONEOUS (OBSOLETE)
OBS	62	MANUAL CUTOFF BY OBSERVER
OBS E	63	ERRONEOUS OBSERVER CUTOFF
OBS FIRE	64	OBSERVER CUTOFF - FIRE
PB PG IC	65	PREBURNER PURGE IGNITION CONFIRM
PB PRG	66	PREBURNER PURGE FAILED ON
PBP PR	67	PREBURNER PUMP DISCHARGE PRESSURE (OBSOLETE)
PC IC H	68	CHAMBER PRESSURE IGNITION CONFIRM - HIGH
PC IC L	69	CHAMBER PRESSURE IGNITION CONFIRM - LOW
PC MS	70	CHAMBER PRESSURE MAINSTAGE
PH/T	71	POWERHEAD AREA ENVIRONMENT TEMPERATURE
PIF	72	LOW FUEL INLET PRESSURE (FACILITY)
PIO	73	LOW OXIDIZER INLET PRESSURE (FACILITY)
SATS	74	SHUTTLE AVIONICS TEST SET (CLUSTER GROUND TEST ORBITER COMPUTER SIMULATC
TH BNG	75	HPFTP THRUST BEARING SPEED (OBSOLETE)
TH BNG E	76	HPFTP THRUST BEARING SPEED - SENSOR MALFUNCTION (OBSOLETE)
VEH	77	VEHICLE (ORBITER) COMMAND



TEST NUMBER	ENGINE	ENGINE	COMP	MAJOR	DATE	COMMENT	DURATION	POWER LEVEL	FAILURE MODE FROM PCB	SCN	CONFIGURATION	COPY ID	DESCRIPTION
901.15	0002	O ISCP	HPOT	YES	15-Dec-77	HPOT I/S CAV PR R/L >80 PSIG	9.83	90	HPOT INTER SEAL CAVITY PRESSURE REDLINE	A008612	PRE MP1A	56	PRE MP1A
901.147	0103	HO ACC C	HPOT		01-Dec-77	HPOTURB BL FAILURE	31.36	81	SEVERE EROSION OF TURBINE AREA	A0050981	PRE MP1A	26	PRE MP1A
902.085	0002	HO ACC C	HPOT		17-Nov-77	HPOT TURBINE BLADE FAILURE-CROSSFEED	51.09	70	HPOT RADIAL CUTOFF-HPOT UN10101R17	A0086231	PRE MP1A	26	PRE MP1A
901.139	0103	HO ACC	HPOT		07-Nov-77	HPOT R/L G - REDUCE P/L & S FLOW	54.83	94	HPOT RADIAL ACCEL R/C/D - ROTOR BALANCE	A0086111	PRE MP1A	24	PRE MP1A
902.083	0002	CONT	SYSTEM		01-Nov-77	ICE IN PC PORT - RUNAWAY THROTTLE UP	48.63	70	CONTROLLER C/O-HPOTVA 8% SWITCH AND S/D	A0086201	PRE MP1A	4	PRE MP1A
902.080	0002	O DR P	HPOT		11-Oct-77	HPOT PR SL DR PR-8 PSIG	34.94	95	HPOT PR LOX SEAL DR PR EXCEEDED REDLINE	A0086051	PRE MP1A	51	PRE MP1A
902.079	0002	O DR P	HPOT		28-Sep-77	HPOT PR SL DR PR-13 PSIG	9.05	65	HPOT PR LOX SEAL DR PR EXCEEDED REDLINE	A0086021	PRE MP1A	51	PRE MP1A
902.075	0002	O DR T	HPOT		26-Sep-77	HPOT PR SL DR PR-3 PSIG	3.05	20	HPOT PR LOX SEAL DR PR EXCEEDED REDLINE	A0086001	PRE MP1A	53	PRE MP1A
902.074	0002	O DR T	HPOT		20-Aug-77	HPOT SL DRT-280 DEGREES R/L	21.71	70	HPOT PR LOX SEAL DR PR EXCEEDED R/L	A0086001	PRE MP1A	53	PRE MP1A
902.073	0002	O TO Y	NOZZLE		18-Aug-77	TUBE SPLITS (31)	7.05	70	NOZZLE TUBE RUPTURES HPOT R/L	A0050681	PRE MP1A	58	PRE MP1A
902.072	0002	O TO Y	NOZZLE		15-Aug-77	TUBE SPLITS (32)	155.50	64	NOZZLE TUBE RUPTURES HPOT R/L	A0050751	PRE MP1A	58	PRE MP1A
901.129	0004	PR PRG	PCA		04-Aug-77	PR PURGE 200 PSI MAX LEAKY SOL VALVE	257.10	75	ERONEOUS PCA HE PURGE PR R/L CUTOFF	A0050801	PRE MP1A	56	PRE MP1A
901.124	0004	O ISCP	HPOT		25-Jul-77	HPOT I/S CAV PR-55 PSIG	6.64	70	HPOT INTER SEAL CAVITY PRESSURE REDLINE	A0050481	PRE MP1A	56	PRE MP1A
902.070	0002	O DR P	HPOT		21-Jul-77	HPOT PR SL PR - CRACKED BELLOW	29.31	90	HPOT PR SL DR LINE	A0053891	PRE MP1A	51	PRE MP1A
902.068	0002	O TO Y	SYSTEM		18-Jul-77	HPOT TURB TEMP-DELATED OPBIGN	5.06	90	HPOT TURBINE DISCHARGE TEMP R/L CUTOFF	A0050471	PRE MP1A	58	PRE MP1A
901.123	0004	O DR P	HPOT		07-Jul-77	FAILED HPOT BELLOW	126.48	70	HPOT PR SL DR PRESS R/C/O	A0053821	PRE MP1A	51	PRE MP1A
901.122	0004	O DR DP	HPOT		05-Jul-77	DELTE DR DP R/L	6.06	70	HPOT PR SL DR PRESS R/C/O	A0050471	PRE MP1A	51	PRE MP1A
901.121	0004	O DR DP	HPOT		05-Jul-77	HPOT PR SEAL DRAIN LINE DELTA PR R/L	4.35	70	HPOT PR SEAL DRAIN LINE DELTA PR R/L	A0050431	PRE MP1A	50	PRE MP1A
901.120	0004	F DT	SENSOR		02-Jul-77	PR SENSOR FAILED CAUSING HIGH PR PC	238.70	70	HPOT TURBINE DISCHARGE TEMP R/L CUTOFF	A0050411	PRE MP1A	9	PRE MP1A
901.116	0004	O DR P	HPOT		21-Jun-77	HPOT BELLOW FAILED	73.23	90	HPOT PR SL DR PRESS R/C/O	A0050221	PRE MP1A	51	PRE MP1A
901.114	0004	O DR P	HPOT		23-May-77	HPOT PR SL DR PR 2 PSI	7.70	70	HPOT PRIMARY SEAL DRAIN LINE PRESS R/C/O	A0050781	PRE MP1A	53	PRE MP1A
901.113	0004	O DR T	HPOT		20-May-77	CHANGE R/L	17.34	50	HPOT INTERMEDIATE SEAL CAV PR R/L C/O	A0050181	PRE MP1A	56	PRE MP1A
902.062	0002	O ISCP	HPOT		05-May-77	HPOT I/S CAV PR (2 PSIG MIN)	29.93	70	HPOT INTERMEDIATE SEAL CAV PR R/L C/O	A0050031	PRE MP1A	56	PRE MP1A
902.059	0002	O ISCP	HPOT		27-Apr-77	HPOT I/S CAV PR	4.13	51	HPOT TURBINE DISCHARGE TEMP R/L CUTOFF	A0050031	PRE MP1A	56	PRE MP1A
901.107	0003	O TO Y	SYSTEM		09-Mar-77	CHANGE MOV START SCHEDULE	8.50	65	HPOT TURBINE DISCHARGE TEMP R/L CUTOFF	A0034501	PRE MP1A	58	PRE MP1A
901.105	0003	HF ACC	HPOT		03-Mar-77	ADD SHIM AT G5	35.33	100	HPOT RADIAL ACC REDLINE C/O (CAV)	A0034501	PRE MP1A	18	PRE MP1A
901.104	0003	OBS	SYSTEM		26-Feb-77	OVERSEER OP/VP POS	10.61	65	OP/VALVE POSITION REDLINE	A0034441	PRE MP1A	62	PRE MP1A
901.103	0003	HO ACC	HPOT		13-Feb-77	HPOT SEVERE EROSION IN SHUTDOWN	23.01	100	HPOT SIB SYNC-TORQUE EXCESSIVE-MSI RUB	A006651	PRE MP1A	24	PRE MP1A
902.049	0002	O TO Y	SYSTEM		13-Feb-77	HPOT DEVALVED OPBIGN	4.31	51	HPOT TURBINE DISCHARGE TEMP REDLINE C/O	A0034221	PRE MP1A	58	PRE MP1A
901.099	0003	CONT PD	SENSOR		31-Jan-77	HPOT DSH PR-SENSORS FAILED	39.60	100	OPB R/L EDM WATER IN FUEL MANIFOLD	A0034091	PRE MP1A	5	PRE MP1A
901.096	0003	F DT	SYSTEM		28-Jan-77	HPOT OVERTEMP	4.25	51	CONTROLLER INITIATED S/D-SENSORS FAILED	A0034051	PRE MP1A	70	PRE MP1A
901.090	0003	HF ACC	HPOT		11-Jan-77	MCC PC TOO LOW - CHANGED R/L	28.63	100	HPOT TURBINE DISCHARGE TEMP R/L CUTOFF	A0034021	PRE MP1A	9	PRE MP1A
902.037	0002	HF ACC	HPOT		28-Dec-76	CHANGE R/L	17.69	85	HPOT RADIAL ACCEL R/C/O	A0024971	PRE MP1A	18	PRE MP1A
902.033	0002	HF ACC	HPOT		27-Oct-76	REPLACE HPOT LPT SW & R/L CHANGES	28.09	75	HPOT RADIAL ACCEL R/C/O	A0026291	PRE MP1A	18	PRE MP1A
901.074	0003	HF SPD	SENSOR		01-Oct-76	HPOT RADIAL VIBRATION SAFETY C/O	33.88	90	TEST CUT BY HPOT RAD ACCEL VOIING LOGIC	A0026191	PRE MP1A	18	PRE MP1A
901.073	0003	F DT	SYSTEM		26-Sep-76	HPOT SPD DROP OUT (NSIR)	26.52	75	SENSOR OUTPUT FAILED	A0024881	PRE MP1A	22	PRE MP1A
901.072	0003	F DT	SYSTEM		16-Sep-76	DELETE TURB IN R/L	29.53	75	HPOT TURBINE INLET TEMP REDLINE EXCEEDED	A0024761	PRE MP1A	11	PRE MP1A
902.071	0003	O DR P	HPOT		13-Sep-76	CHANGED F T IN R/L	17.15	90	HPOT TURBINE INLET TEMP REDLINE EXCEEDED	A0024681	PRE MP1A	11	PRE MP1A
902.067	0002	F DT	SYSTEM		01-Sep-76	HPOT PR SL DR PR	18.30	93	HPOT PR SEAL CAVITY PR REDLINE EXCEEDED	A0024681	PRE MP1A	11	PRE MP1A
902.026	0002	O TO Y	SYSTEM		24-Aug-76	HPOT INTEMP R/C/D	2.96	20	HPOT TURBINE INLET TEMP REDLINE EXCEEDED	A0024471	PRE MP1A	60	PRE MP1A
902.024	0002	O TO Y	SYSTEM		21-Aug-76	OPB OVERTEMP	3.77	60	OPB OVERTEMP	A0024451	PRE MP1A	60	PRE MP1A
902.023	0002	O TO Y	SYSTEM		18-Aug-76	OPB OVERTEMP	3.63	50	OPB OVERTEMP	A0024381	PRE MP1A	60	PRE MP1A
902.021	0002	O TO Y	SYSTEM		17-Aug-76	HPOT TURBINE INLET TEMP REDLINE	3.43	50	HPOT TURBINE INLET TEMP REDLINE EXCEEDED	A0024351	PRE MP1A	11	PRE MP1A
901.067	0001	HF ACC	HPOT		11-Aug-76	OPB OVERTEMP	3.73	75	HPOT OVERTEMP - C/CV SCHEDULE CHANGED	A0024271	PRE MP1A	60	PRE MP1A
902.018	0002	HF ACC	HPOT		26-Jul-76	LAST TEST ON 0001D	41.45	63	HPOT RADIAL VIBRATION SAFETY C/O	A0024191	PRE MP1A	18	PRE MP1A
901.066	0001	HF ACC	HPOT		14-Jul-76	HPOT RADIAL VIBRATION SAFETY C/O	22.07	85	HPOT RADIAL VIBRATION SAFETY C/O	A0024151	PRE MP1A	18	PRE MP1A
901.065	0001	HF ACC	HPOT		09-Jul-76	SUB SYNC VIB	4.24	76	HPOT RADIAL VIBRATION SAFETY C/O	A0024121	PRE MP1A	18	PRE MP1A
902.016	0002	HF ACC	HPOT		07-Jul-76	NO COMPONENT CHANGE	16.91	76	HPOT RADIAL VIBRATION SAFETY C/O	A0024031	PRE MP1A	18	PRE MP1A
902.015	0002	HF ACC	HPOT		15-Jun-76	SW & R/L CHANGES	16.40	75	HPOT RADIAL VIBRATION SAFETY C/O	A0024031	PRE MP1A	18	PRE MP1A
902.014	0002	HF ACC	HPOT		15-Jun-76	HPOT RADIAL VIBRATION SAFETY C/O	16.70	65	HPOT RADIAL VIBRATION SAFETY C/O	A0024031	PRE MP1A	18	PRE MP1A
902.013	0002	HF ACC	HPOT		12-Jun-76	HPOT AXIAL VIBRATION SAFETY C/O	3.27	50	HPOT AXIAL VIBRATION SAFETY C/O	A0033901	PRE MP1A	19	PRE MP1A
902.012	0002	HF ACC	HPOT		07-Jun-76	HPOT AXIAL VIBRATION SAFETY C/O	3.16	50	HPOT AXIAL VIBRATION SAFETY C/O	A0033901	PRE MP1A	19	PRE MP1A
901.059	0001	HF ACC	HPOT		05-Jun-76	HPOT WHIRL	3.97	50	HPOT RADIAL VIBRATION SAFETY C/O	A0033871	PRE MP1A	18	PRE MP1A
901.058	0001	HF ACC	HPOT		03-Jun-76	CHANGED R/L	12.08	75	HPOT RADIAL VIBRATION SAFETY C/O	A0033861	PRE MP1A	18	PRE MP1A
902.013	0002	HF ACC	HPOT		01-Jun-76	HPOT RADIAL VIBRATION SAFETY C/O	11.10	65	HPOT RADIAL VIBRATION SAFETY C/O	A003371	PRE MP1A	18	PRE MP1A
901.057	0001	HF ACC	HPOT		26-May-76	SEQ CHANGE	11.86	74	HPOT RADIAL VIBRATION SAFETY C/O	A003371	PRE MP1A	18	PRE MP1A
901.056	0001	HF ACC	HPOT		21-May-76	CHANGED R/L	7.27	65	HPOT AXIAL VIBRATION SAFETY C/O	A003371	PRE MP1A	19	PRE MP1A
901.055	0001	HF ACC	HPOT		18-May-76	HPB EROSION & HPOT CHANGES	6.29	61	HPOT AXIAL VIBRATION SAFETY C/O	A003371	PRE MP1A	19	PRE MP1A
901.054	0001	HF ACC	HPOT		08-May-76	CHANGES TO HPOTURB	7.31	65	HPOT RADIAL VIBRATION SAFETY C/O	A003371	PRE MP1A	18	PRE MP1A
901.053	0001	HF ACC	HPOT		06-May-76	CHANGES TO HPOTURB	6.52	62	HPOT RADIAL VIBRATION SAFETY C/O	A003371	PRE MP1A	18	PRE MP1A
901.052	0001	HF ACC	HPOT		26-Apr-76	NO PUMP CHANGES	7.34	65	HPOT RADIAL VIBRATION SAFETY C/O	A0033651	PRE MP1A	18	PRE MP1A

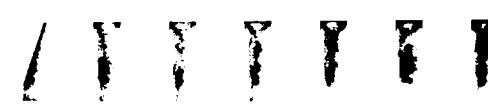
TEST NUMBER	ENGINE	ENGINE	MAJOR EVENT	DATE	COMMENT	DURATION SECS	POWER LEVEL	FAILURE MODE FROM DCE	UCS	CONTAMINATION	CUTPOINT ID	DESCRIPTION RATIONALE
901.051	0001	F111		22-Apr-76	HPF TURB IN T R/L	10.32	75	HPFT TURBINE INLET TEMP REDLINE	A003359	PRE MPFA	11	PRE MPFA
901.046	0001	HF ACC A		02-Apr-76	EXCESSIVE AXIAL VIBRATION	6.27	61	EXCESSIVE AXIAL VIBRATION	A001428	PRE MPFA	19	PRE MPFA
901.044	0001	TH BNG		12-Mar-76	HPFTP BNG SPD	45.18	55	THRUST BEARING WELDED TO HPFT SHAFT	A001422	PRE MPFA	75	PRE MPFA
901.041	0001	O111		05-Mar-76	OPB O/I	3.84	50	OPB OVERTEMP	A001413	PRE MPFA	60	PRE MPFA
901.040	0001	HGM		02-Mar-76	HGM LINER DELTA P R/L	3.39	50	HGM LINER DELTA P R/L	A001410	PRE MPFA	23	PRE MPFA
901.039	0001	O111		27-Feb-76	OPB OVERTEMP	2.88	20	OPB OVERTEMP	A001408	PRE MPFA	23	PRE MPFA
901.035	0001	HGM		24-Jan-76	HGM Gndg P	3.16	20	HGM LINER DELTA P R/L - LATE LOX POWER	A007597	PRE MPFA	23	PRE MPFA
901.033	0001	TH BNG		19-Jan-76	HPFTP BNG SPEED	2.86	20	HPFTP BNG SPEED	NO UCR	PRE MPFA	75	PRE MPFA
901.032	0001	TH BNG		16-Jan-76	HPFTP BNG SPEED	2.76	20	HPFTP BNG SPEED	NO UCR	PRE MPFA	75	PRE MPFA
901.031	0001	TH BNG		15-Jan-76	HPFTP BNG SPEED	2.73	20	HPFTP BNG SPEED	NO UCR	PRE MPFA	75	PRE MPFA
901.023	0001	HF ACC A		12-Nov-75	HPFTP AX & RAD ACCL	2.99	20	HPFT AXIAL ACCEL REDLINE EXCEEDED	A007553	PRE MPFA	19	PRE MPFA
901.022	0001	HF ACC A		07-Nov-75	EXCESSIVE AXIAL VIBRATION	2.76	20	HPFT AXIAL ACCEL REDLINE EXCEEDED	A007552	PRE MPFA	19	PRE MPFA

Catastrophic Failures in Entire SSME History

TEST NUMBER	ENGINE	COMP	DATE	COMMENT	DURATION	POWER LEVEL	FAILURE MODE FROM DCR	UCR	CONFIGURATION
904.044	0212	HPOTP	23-Jun-89	HPOTP #2 BEARING FAILURE	1270.72	96	BEARING WEAR WITH OPERATING TIME	A023129	5 FPL/PH2
902.471	2206	DUCT-LPF	02-Jun-89	LPF DUCT BELLOW TIE BROKE	147.68	104	FLEX JOINT TRIPOD FATIGUE - SMALL RADIUS	A008935	5 FPL/PH2
750.285	0210	NOZLE	21-May-87	FEED LINE CRACK AT STOP WELD	224.00	109	LEAK IN NO. 3 DOWNCOMMER	A015716	5 FPL/PH2
750.259	2308	MCC	27-Mar-85	DISCH MAN RUPTURE - EXT DAM	101.56	109	PREM C/O. HPFTP ACCELS	A015713	5 FPL/PH2
901.468	0207	FPB	04-Feb-85	CRACK AT F-13 FLANGE-eng retired	203.86	109	CRACK STARTED IN BOSS TO MAN. WELD	A014585	5 FPL/PH2
901.436	0108	HPFTP	14-Feb-84	CUNT LNR PR-MAJOR DAMAGE	611.06	109	EXTENSIVE TURB DAMAGE (RLCO)	A013338	5 FPL/PH2
750.175	2208	DUCT	27-Aug-82	HPO DUCT RUPTURE - ULTRASONIC F/M	116.08	111	PREM C/O P/B BOOST PUMP ACCLES	A011506	4 FPL
750.160	0110	FPB-HCE	12-Feb-82	H2O FROM EDM/EXT DAMAGE (CG1B)	3.16	20	TURB DIS TEMP. WATER IN ENG. EDM OPER	A016045	4 FPL
902.249	0204	HPFTP	21-Sep-81	TURB BL FAIL/VOLUTE RUPTURE/EXT DAM	450.57	109	PREM C/O HPFTP TURB BLADE FAILURE	A018288	4 FPL
SF1001-C	0006	FPB	12-Jul-80	HOLE BURNED IN FPB	106.52	102	OBSERVER PREMATURE CUT DUE TO FIRE	A015391	2 MPTA
SF0601-A	2002	MFV	02-Jul-79	MFV BODY FAILURE	18.49	100	VALVE CAP TO BODY BOLTS BROKEN	A009437	2 MPTA
901.225	2001	MOV	27-Dec-78	MOV FRETTING-FIRE-EXT DAM	255.63	100	MOV FIRE - HPFT R/L	A010816	2 MPTA
901.136	0004	HPOTP	08-Sep-77	HPOTP BNG FAILURE - EXT DAM	300.22	90	CUTOFF DUE TO HPOT FIRE OPOVA FID 34-0	A005350	1 PRE MPTA
901.133	0004	FPB	27-Aug-77	HOLE IN FPB BODY	48.21	90	HOLE BURNT THRU FPB BODY OF POWERHEAD	A005072	1 PRE MPTA
901.110	0003	HPOTP	24-Mar-77	HPOTP FIRE EXT DAM	74.07	75	SEVERE INTERNAL FIRE DAMAGE	A005353	1 PRE MPTA



B.2. Integrated Solid  
Rocket Booster



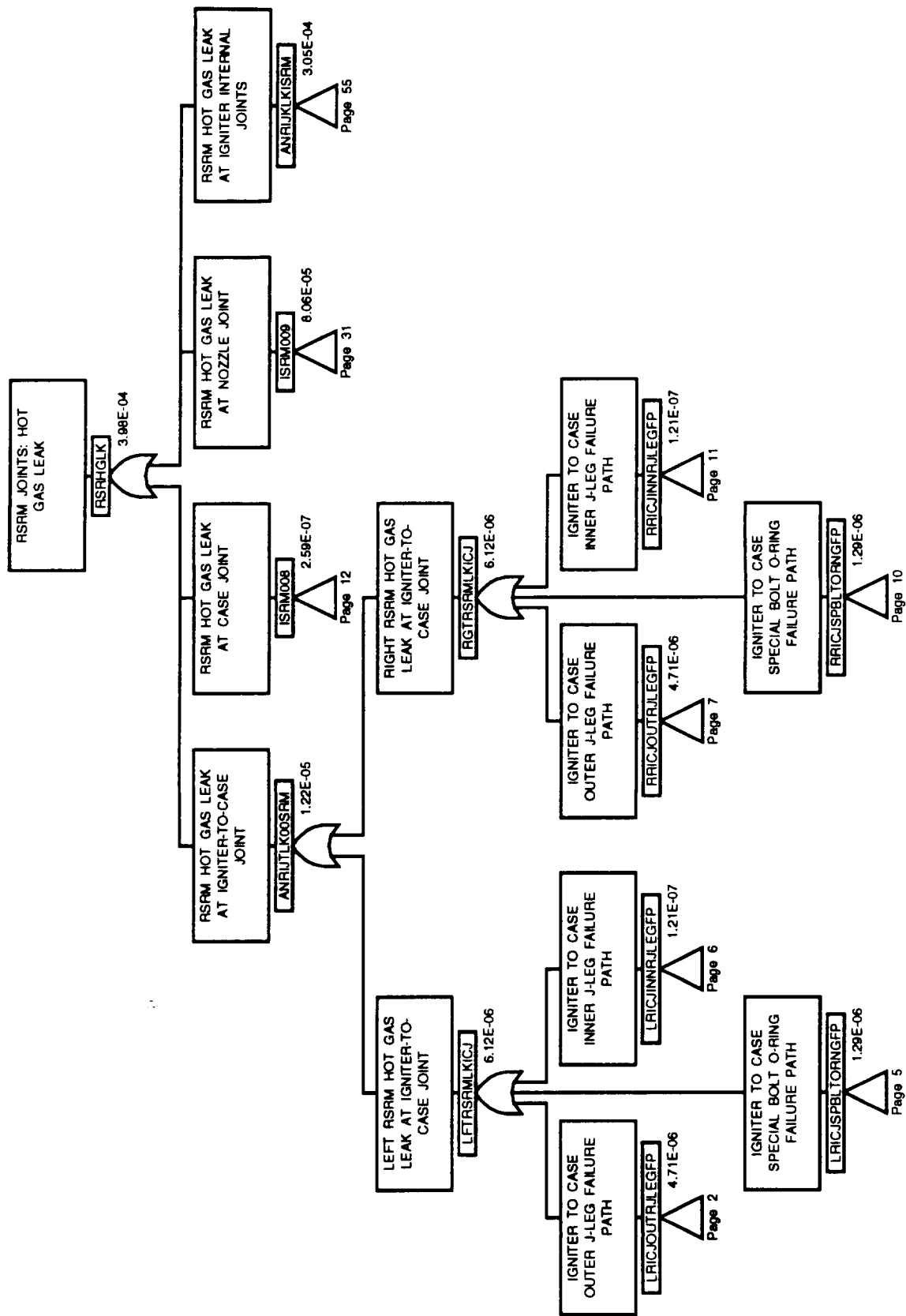


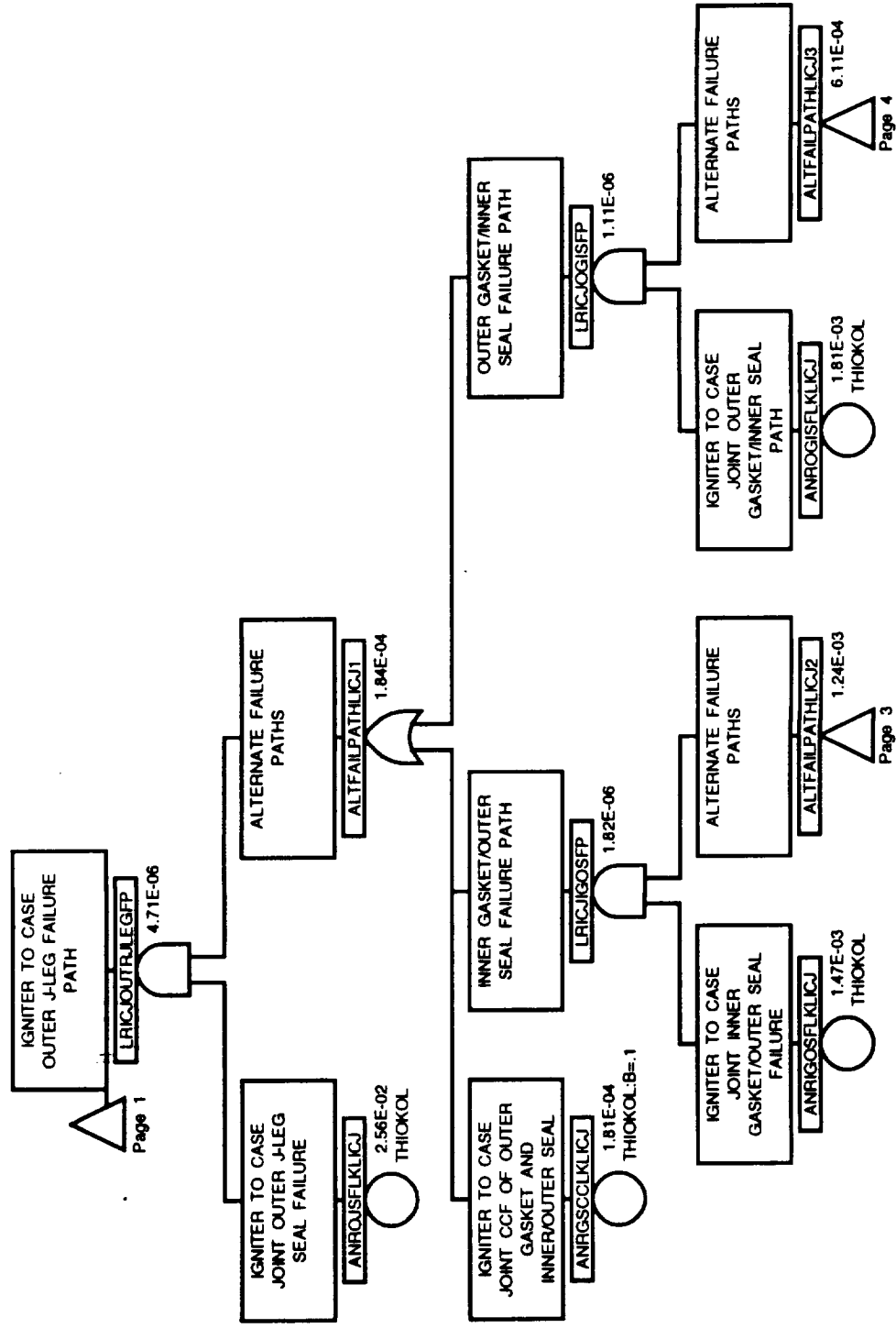
ISRB Initiator Frequency Summary						
Initiator ID	Initiator Description	One Motor Initiator Freq (per mission)	Pair Initiator Freq (per mission)	Mean # of Missions Between Occurrences	Percent of Non-nominal Initiators	Development
RSRHGLK	RSRM JOINTS: HOT GAS LEAK	1.99E-04	3.98E-04	2513	31.59%	Fault Trees-Page 1
RSRZRUP	RSRM NOZZLE RUPTURE	4.45E-05	8.90E-05	11236	7.06%	Fault Trees-Page 64
RSRPVRUP	RSRM PRESSURE VESSEL RUPTURE	3.61E-05	7.22E-05	13850	5.73%	Fault Trees-Page 65
RSRWRTHR	RSRM WRONG THRUST	5.00E-09	1.00E-08	100000000	0.00%	Fault Trees-Page 66
SRBNOHLDN	SRB NO. LATE, OR IMPROPER HOLDDOWN RELEASE	1.29E-04	2.58E-04	3876	20.48%	Fault Trees-Page 68
SRBNOIGN	NO OR LATE IGNITION OF 1 SRB/RSRM	1.11E-04	2.22E-04	4505	17.62%	Fault Trees-Page 82
SRBNOSEP	SRB FAILS TO SEPARATE	6.95E-05	1.39E-04	7194	11.03%	Fault Trees-Page 87
SRBPREMHD	SRB HOLDDOWN: PREMATURE RELEASE	8.00E-07	1.60E-06	625000	0.13%	Fault Trees-Page 190
SRBRECPREM	SRB RECOVERY DEVICE: PREMATURE RELEASE	3.00E-06	6.00E-06	166667	0.48%	Fault Trees-Page 191
SRBSTR	SRB STRUCTURAL FAILURES	5.00E-07	1.00E-06	1000000	0.08%	Fault Trees-Page 192
SRBTV	SRB THRUST VECTOR CONTROL SYSTEM FAILURE	3.57E-05	7.13E-05	14025	5.66%	Fault Trees-Page 193

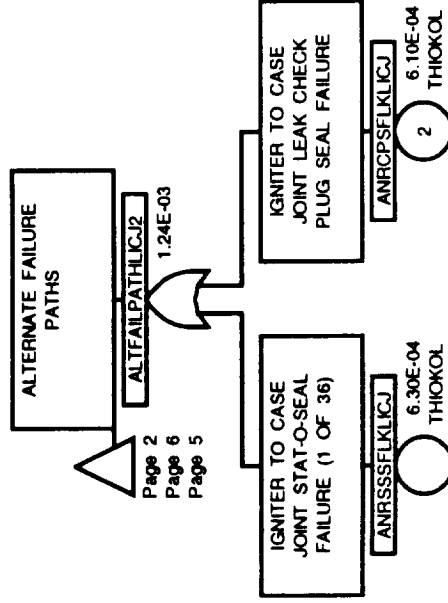
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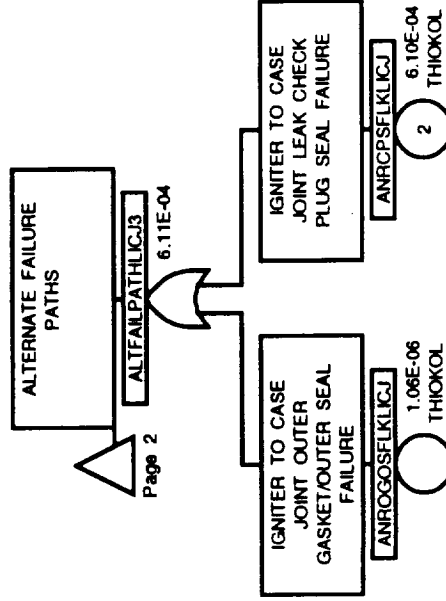
## ISRB Hypothesis Descriptions

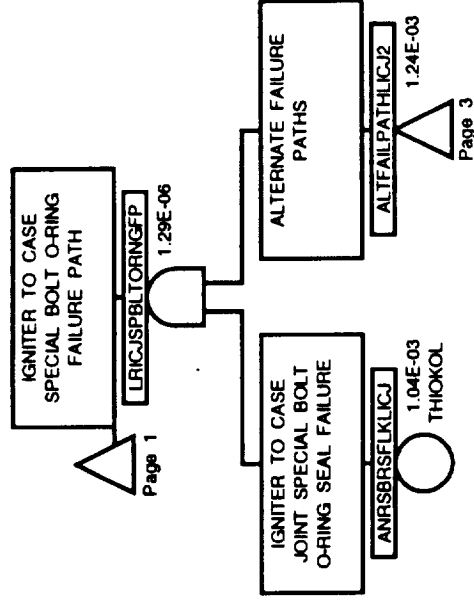
Hypothesis-1	The analyst made an educated estimate of the anticipated frequency of the event in question. This was deemed necessary when there was insufficient data to support a statistical analysis. The estimation was made after conferring with experts on reliability of the sub-component based on their respective experience.
Hypothesis-2	Insufficient data to support a statistical analysis was available for the NASA Standard Initiators (NSIs) and NASA Standard Detonators (NSDs) however the components were found to be similar in both design and function as the Confined Detonating Fuses (CDFs). However due to additional elements in the NSI and NSD assemblies they were assumed to be 2-3 times more prone to fail than the CDF.
Hypothesis-3	The data available for the Pyrotechnic Initiator Controllers (PICs) indicates that they are extremely reliable components however the fact that no actual failures have occurred makes the estimation of their failure rate difficult. As a conservative assumption, their failure rate was assumed to be on the same order of magnitude as the CDFs.
Hypothesis-4	The ISRB use pyrogenic igniters for which a limited amount of failure data exists. For this reason the analyst made a conservative assumption based on the data available and conversations with USBI personnel.
Hypothesis-5	This estimate concerned the possibility of an explosive device detonating without any external influences; an extremely rare event. A conservative estimate was made which considered such an event to be 10 times less likely than an explosive device (CDF) failing to detonate on command.
Hypothesis-6	The Booster Separation Motors (BSMs) have a limited amount of failure related data however it was agreed (USBI & MSFC) that the failure modes were approximately an order of magnitude (10 times) more likely than an explosive device (CDF) failing to detonate.

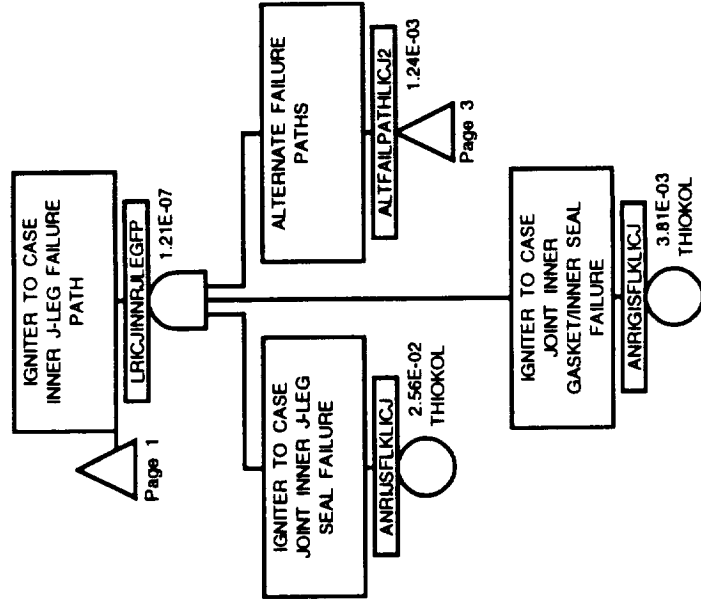




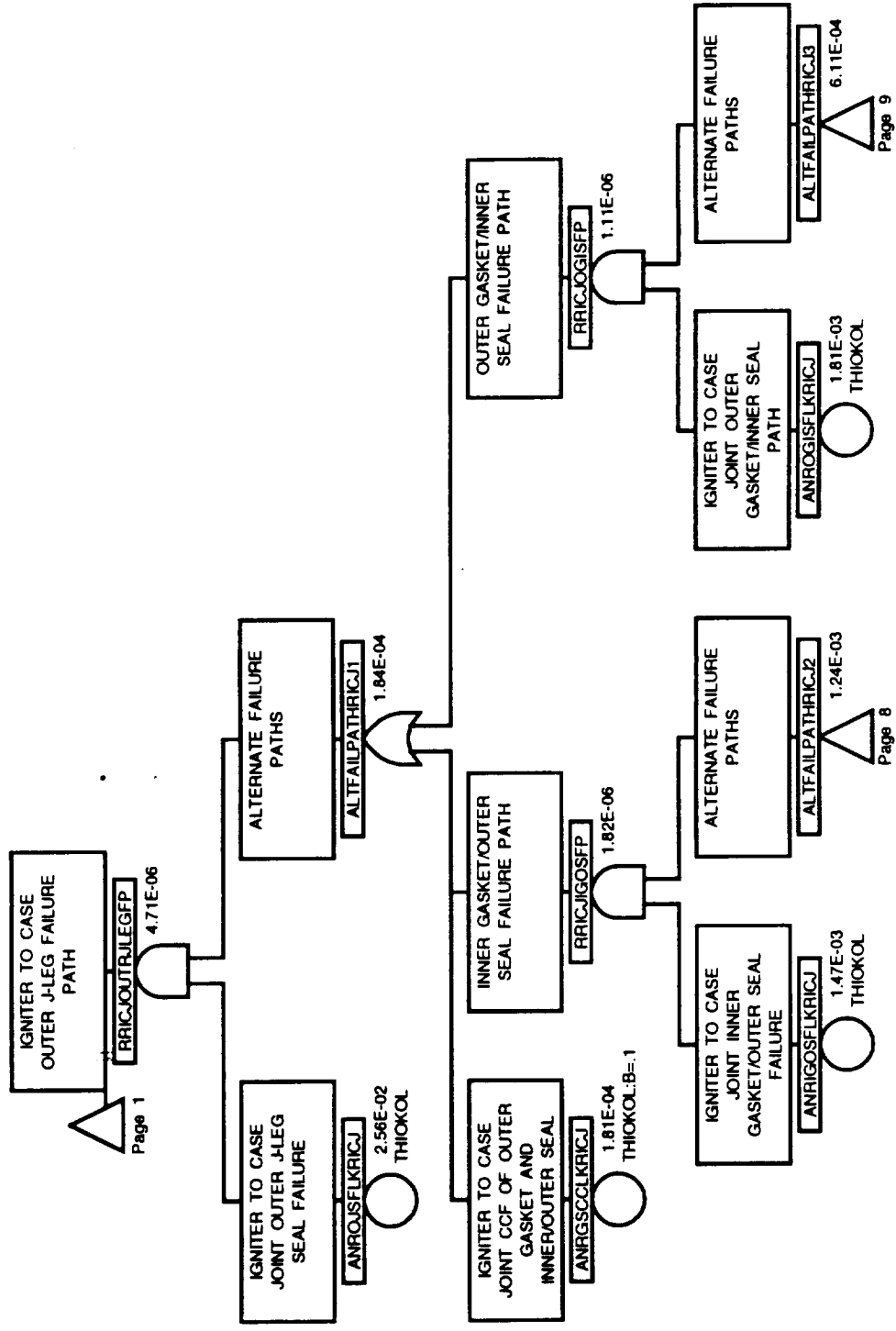


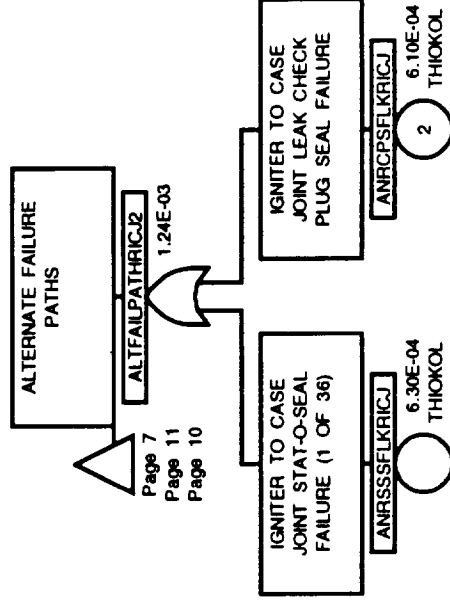


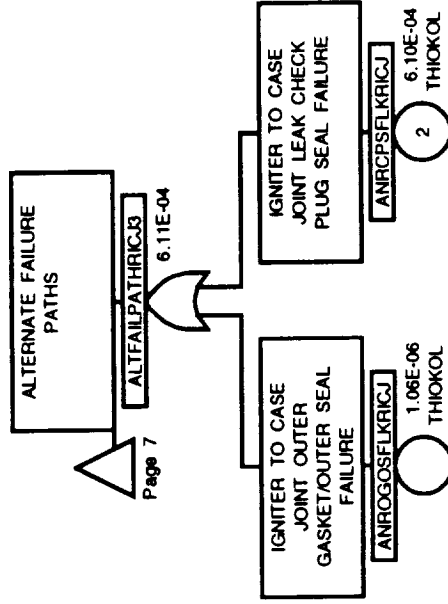




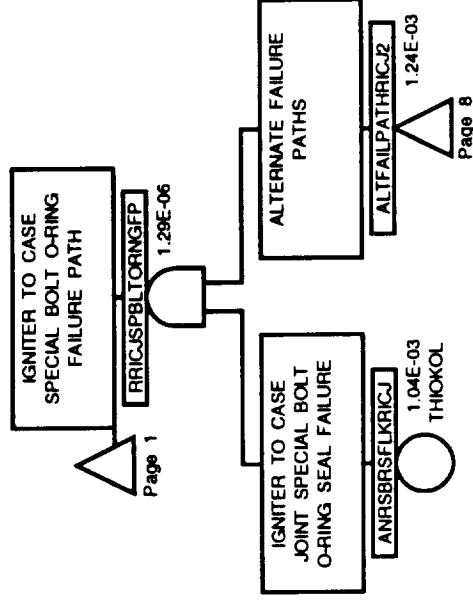


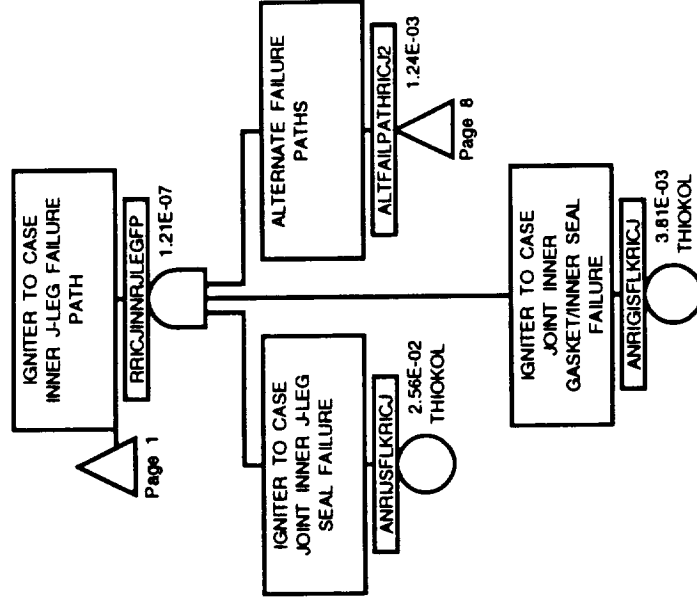


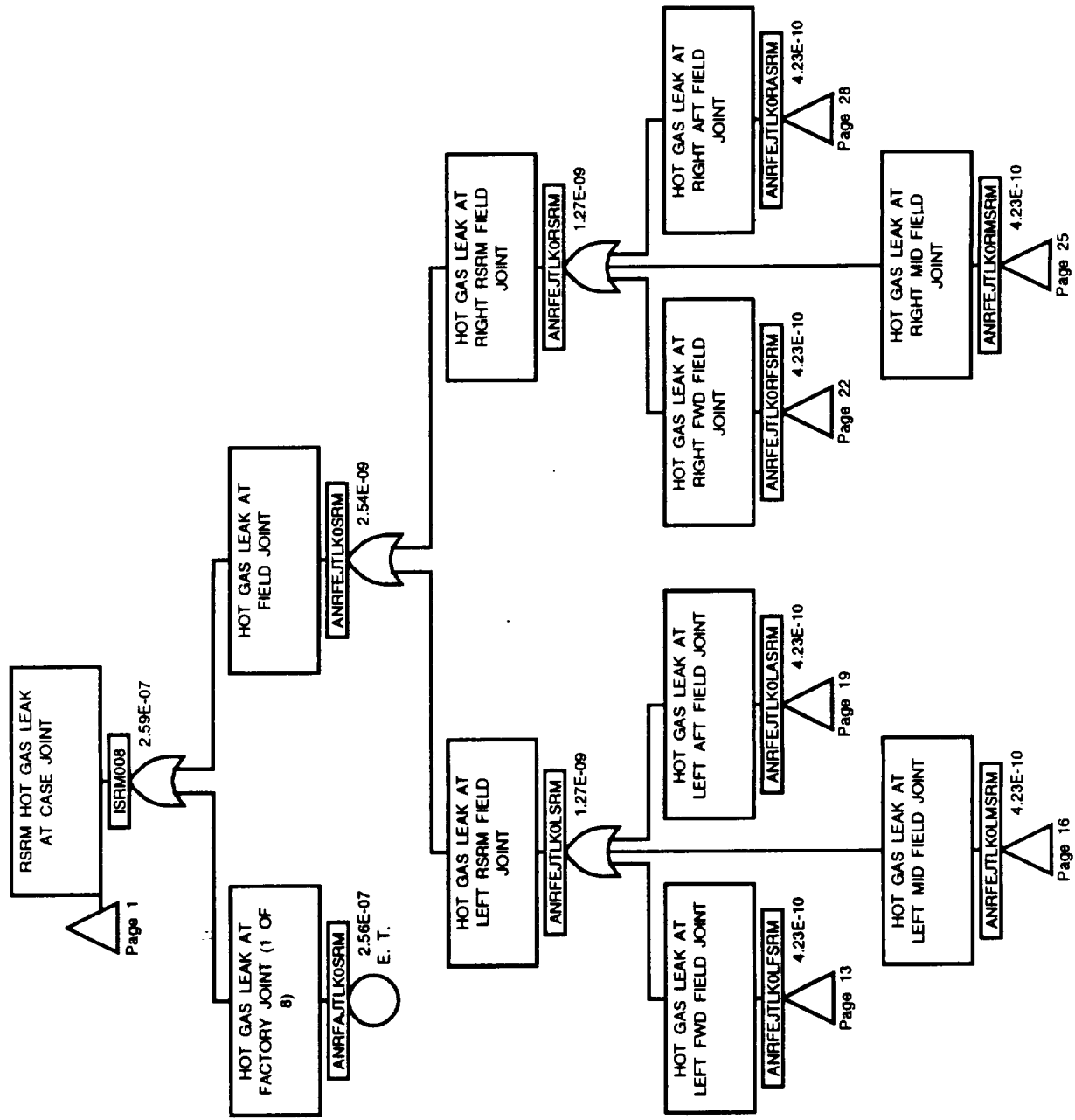


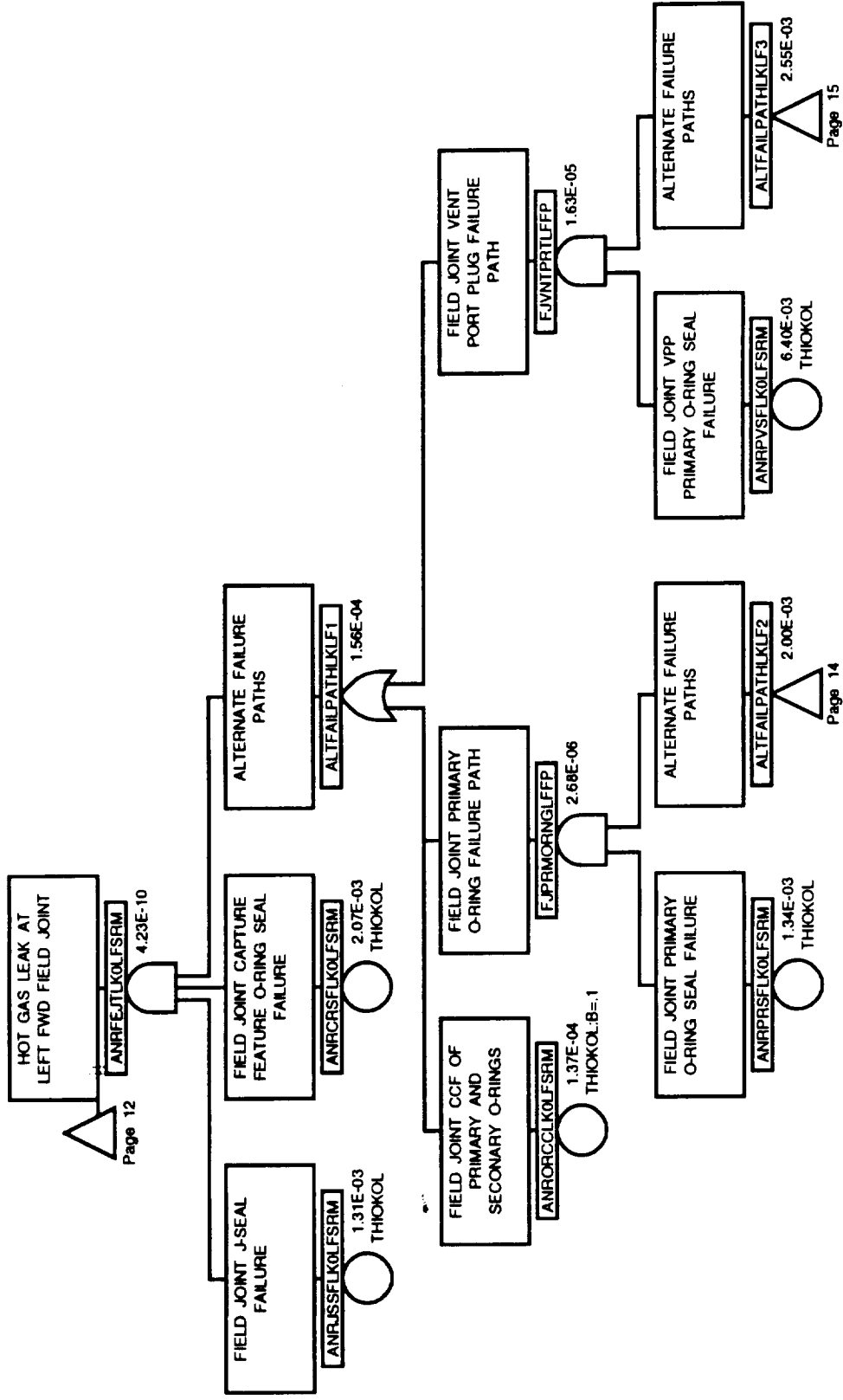


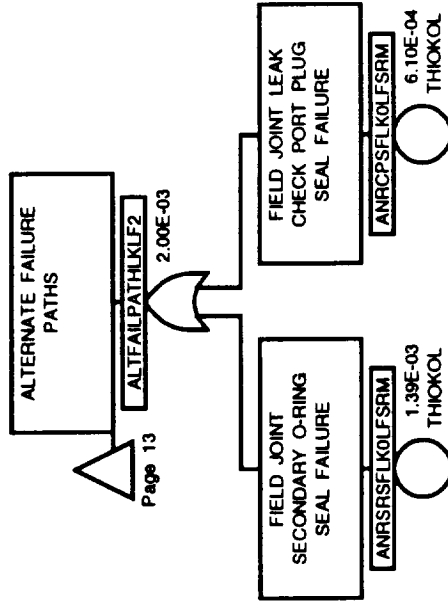
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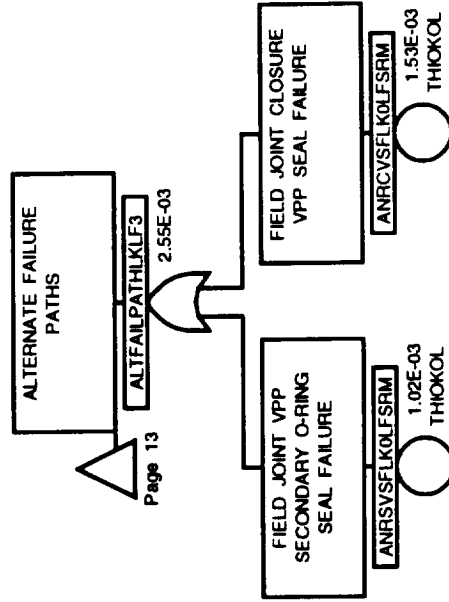


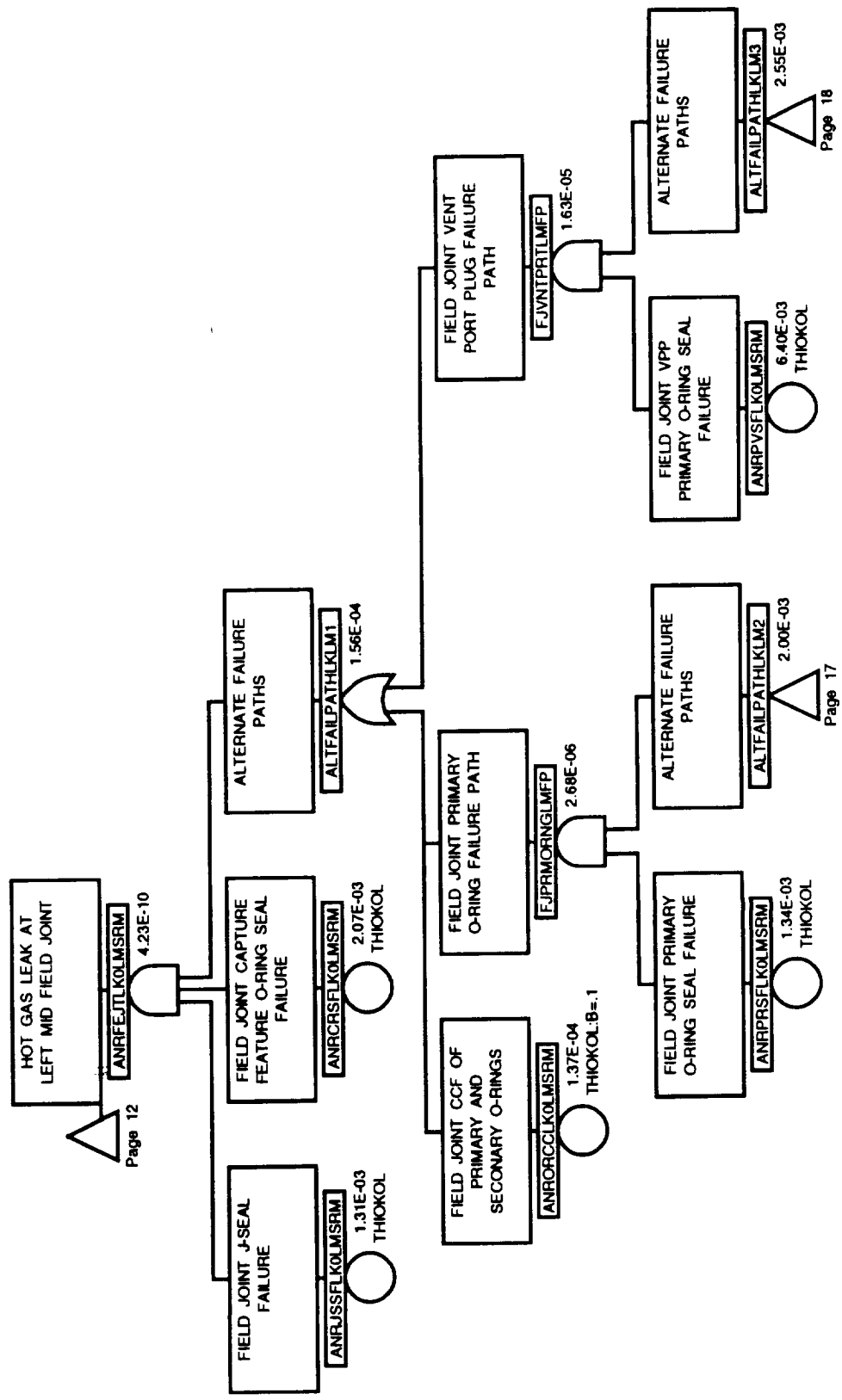




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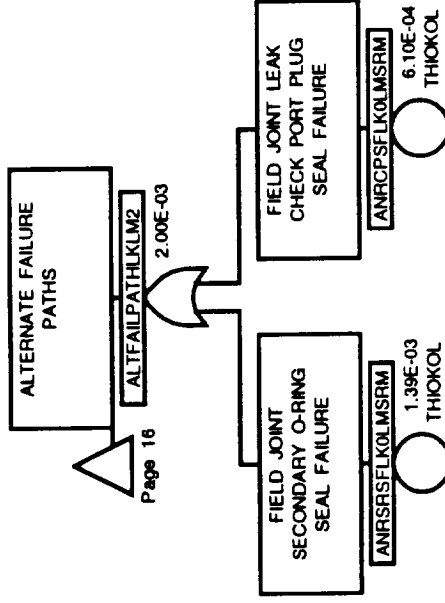




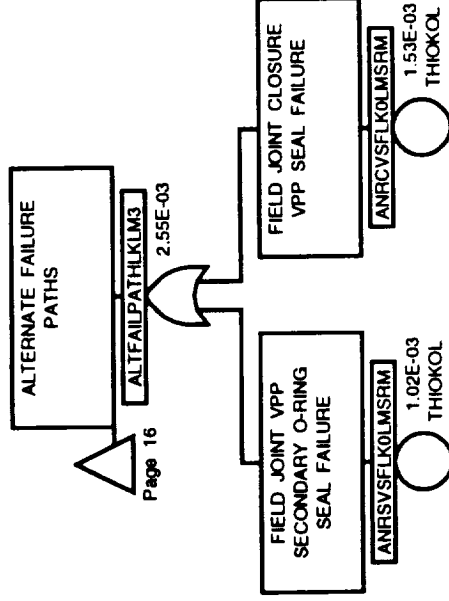
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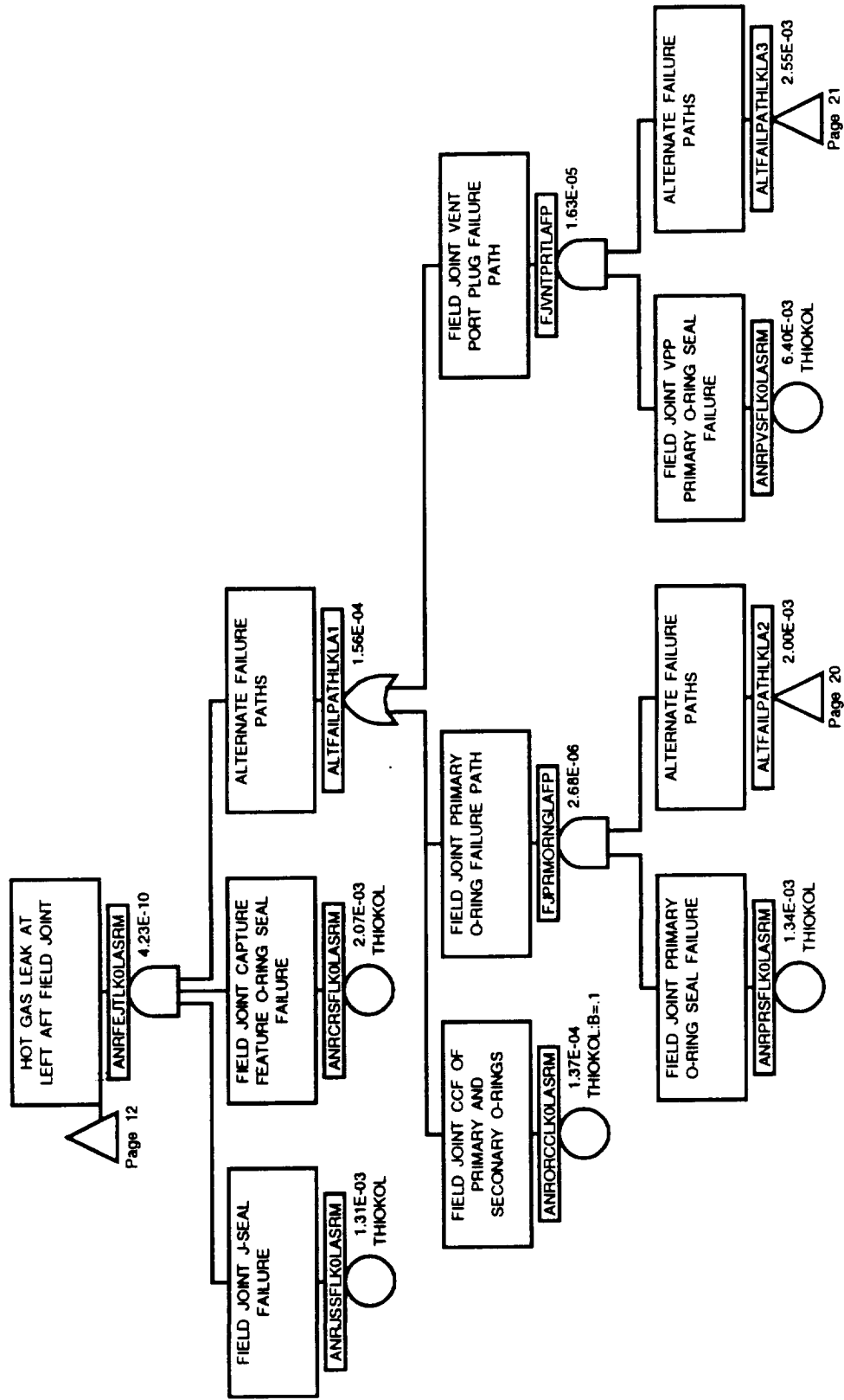
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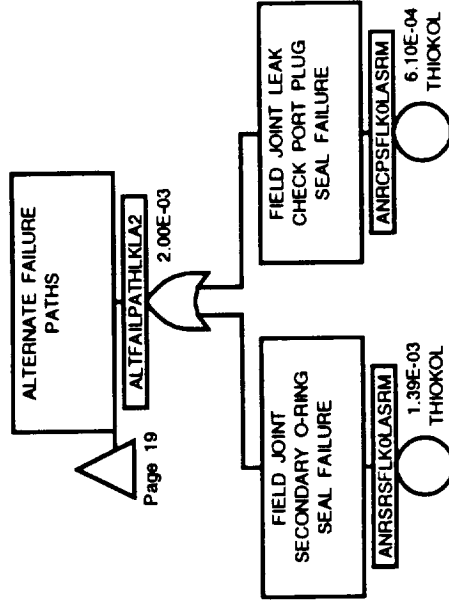
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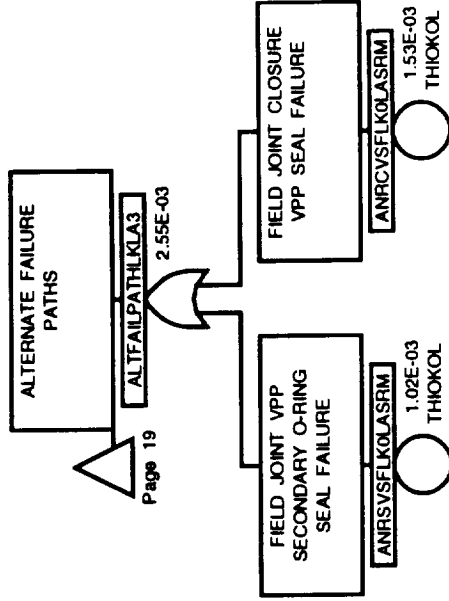
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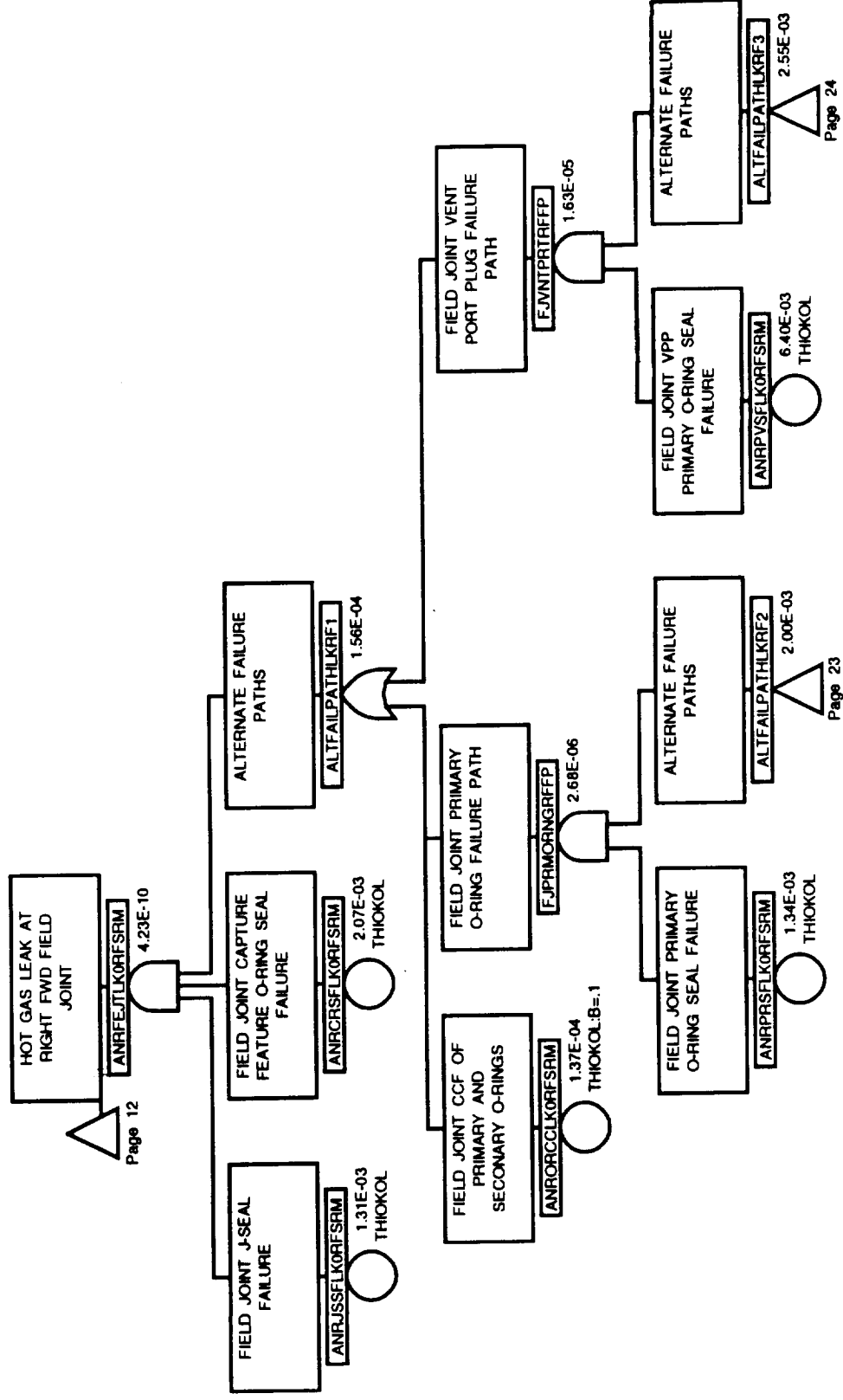
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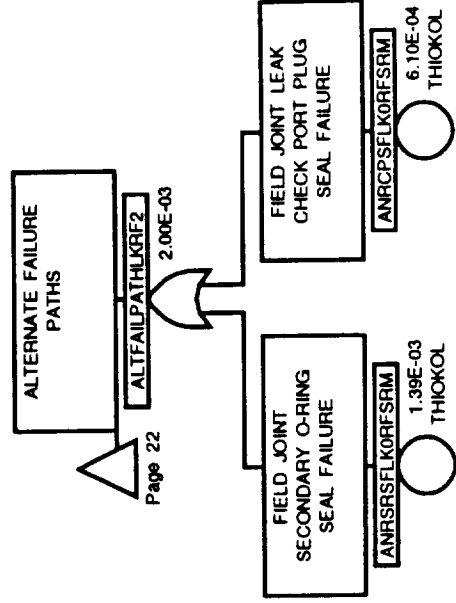


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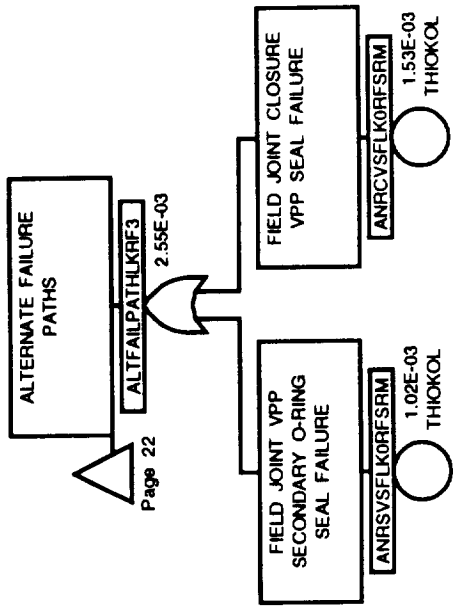




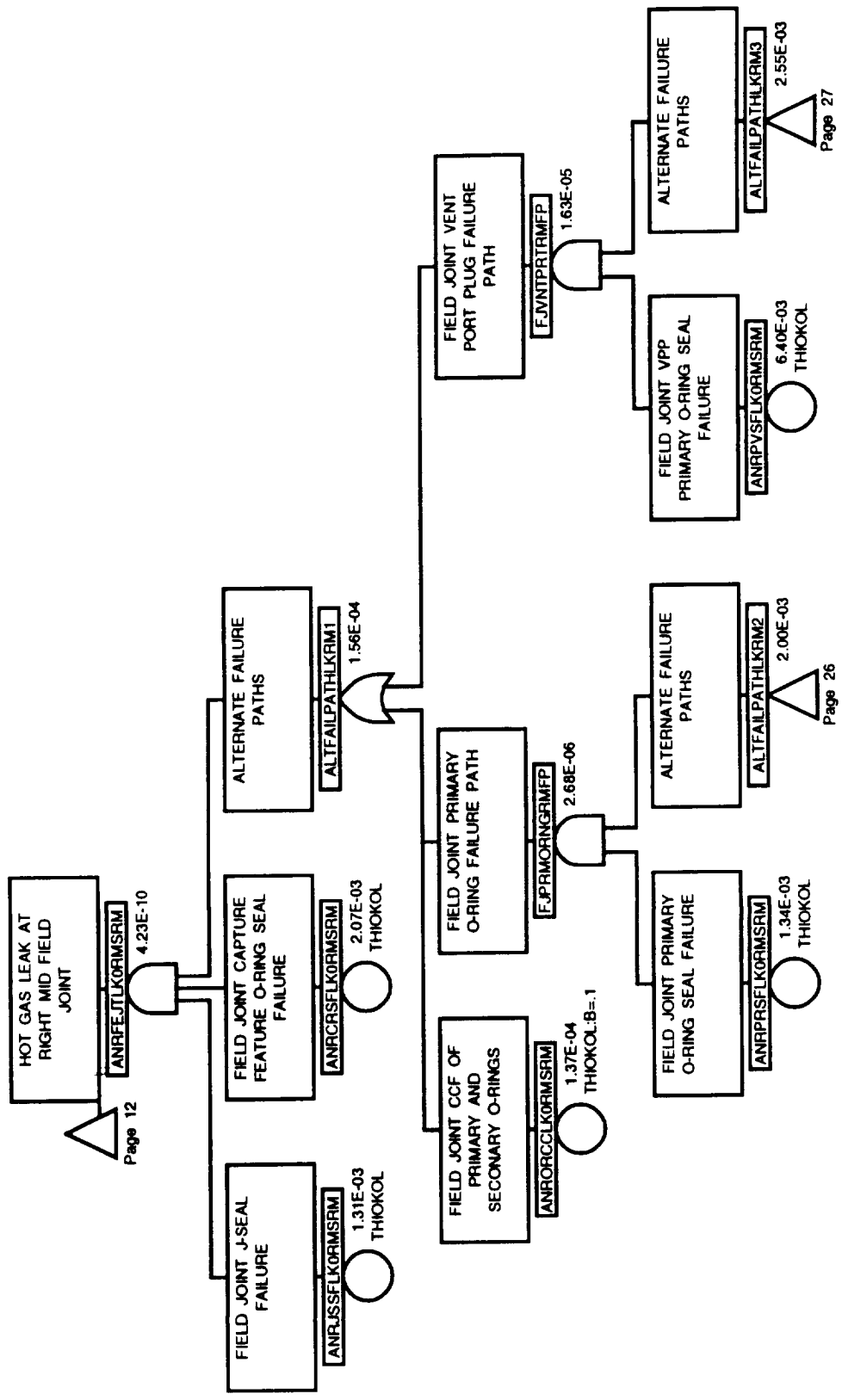




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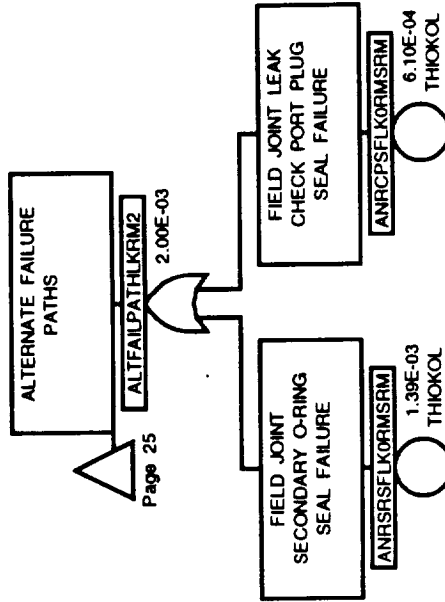
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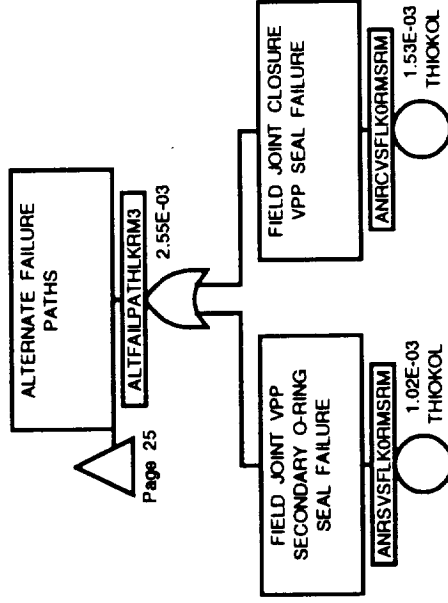
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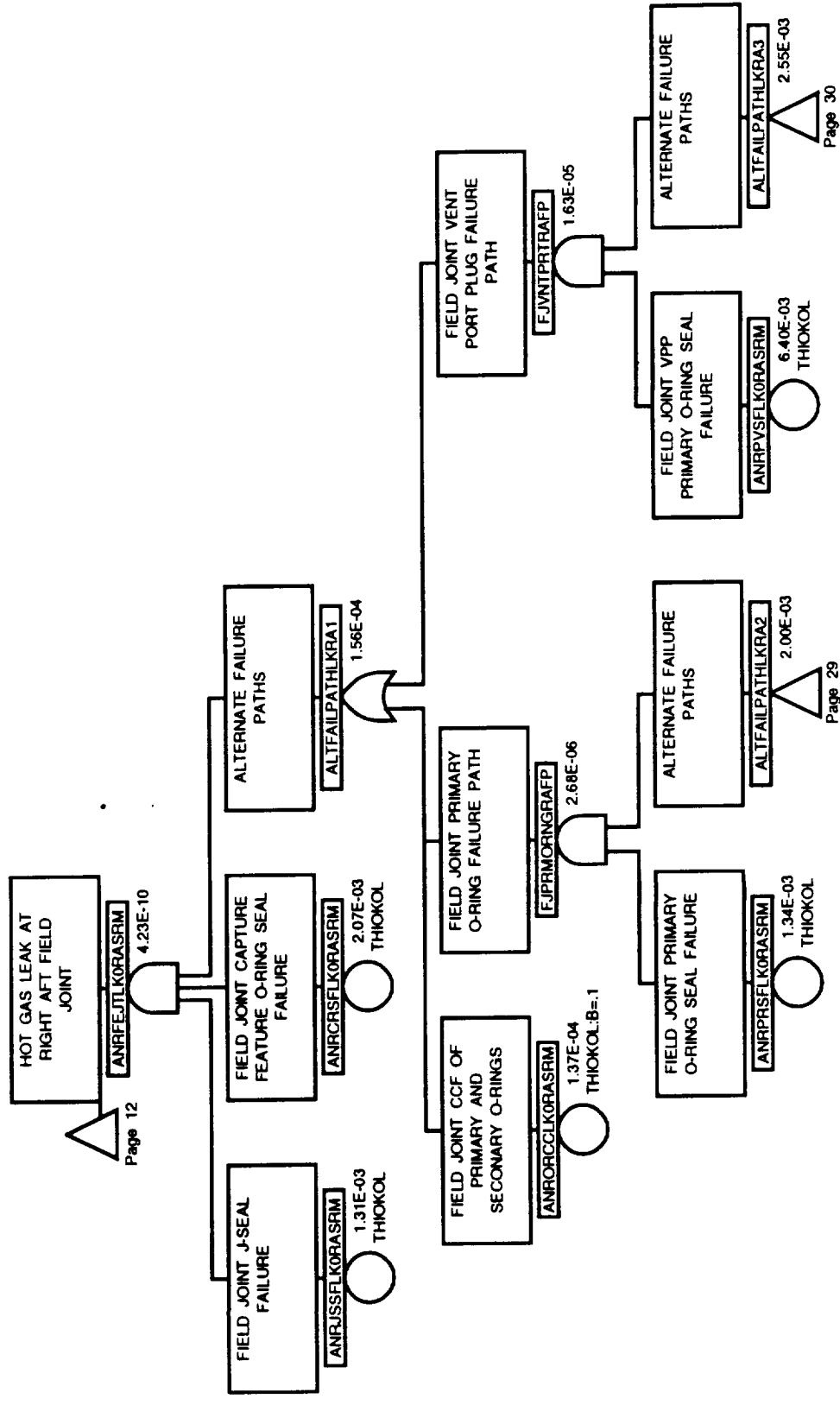
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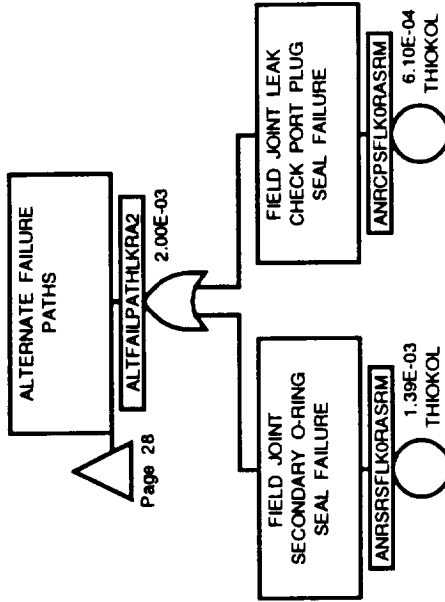
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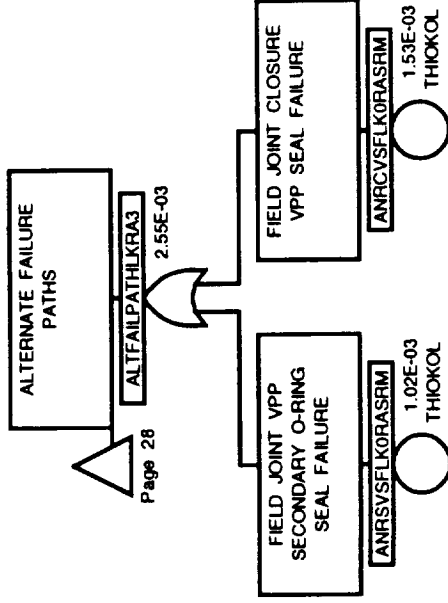
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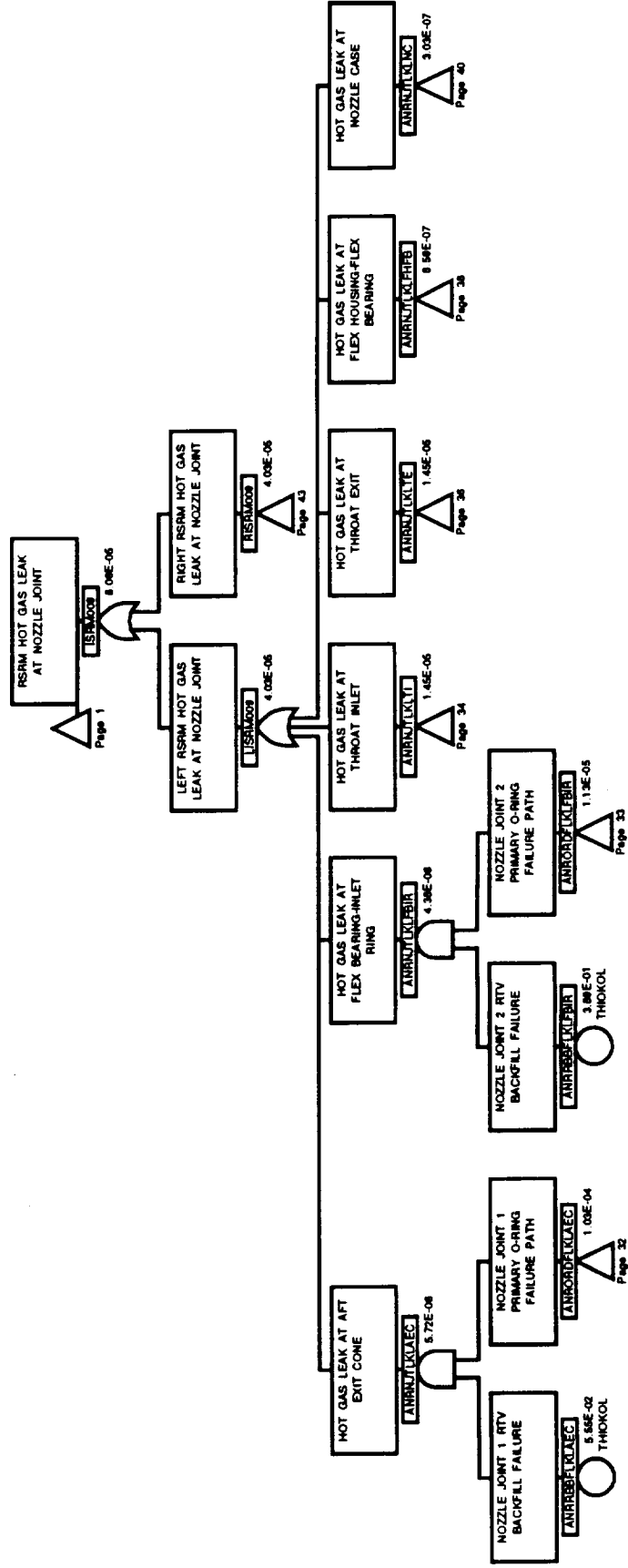


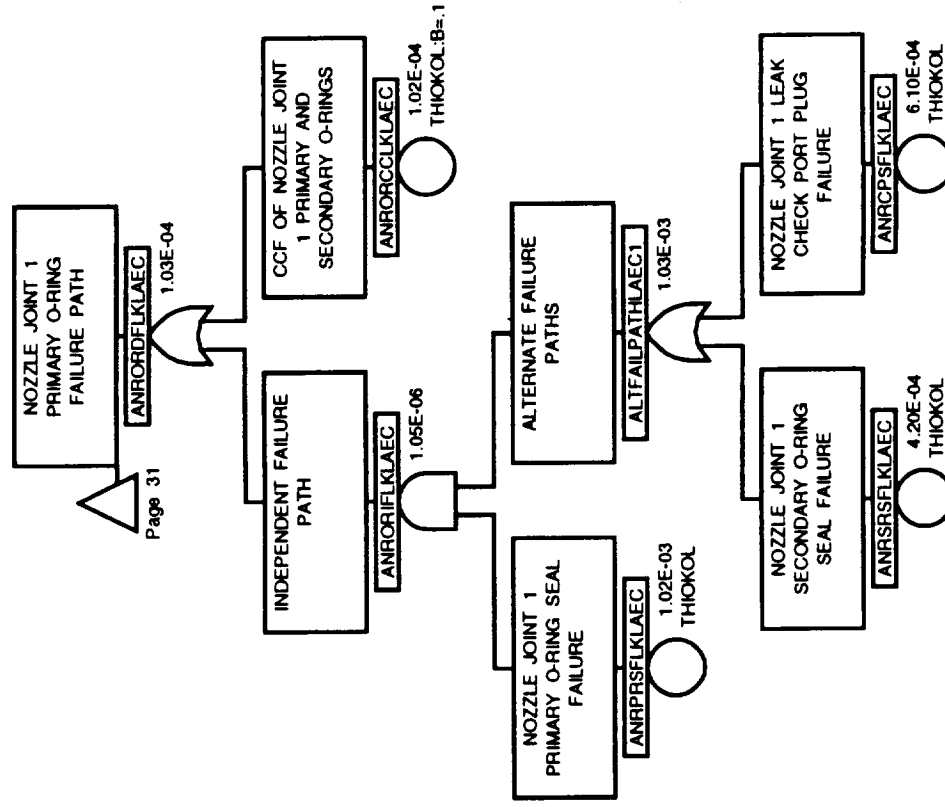
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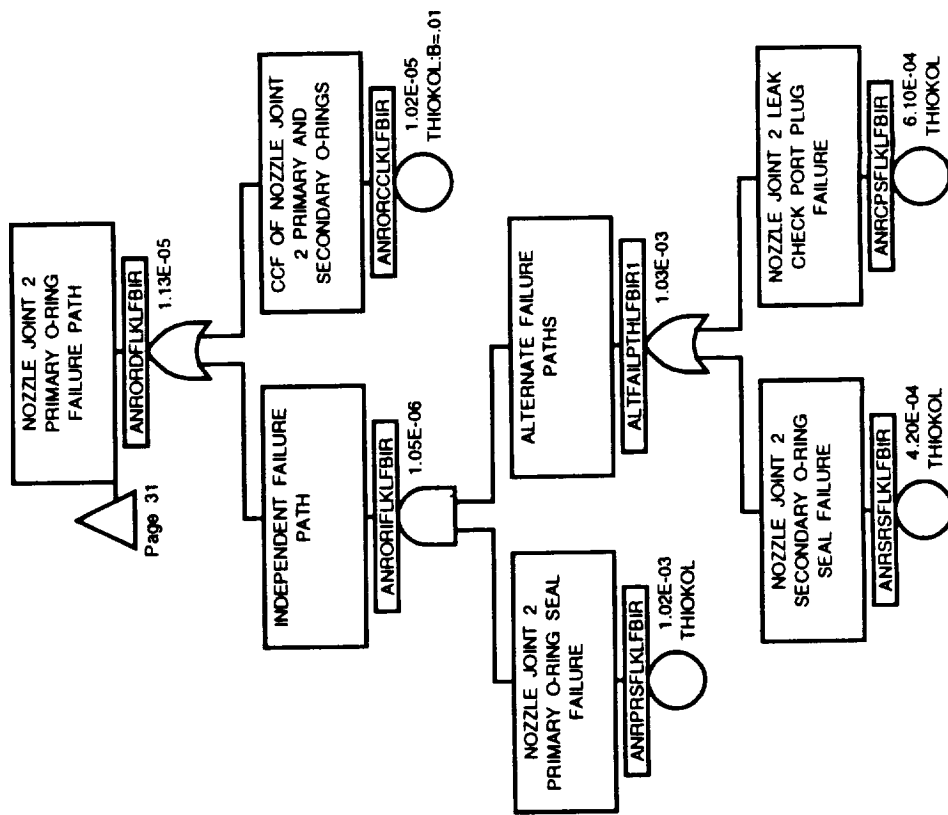


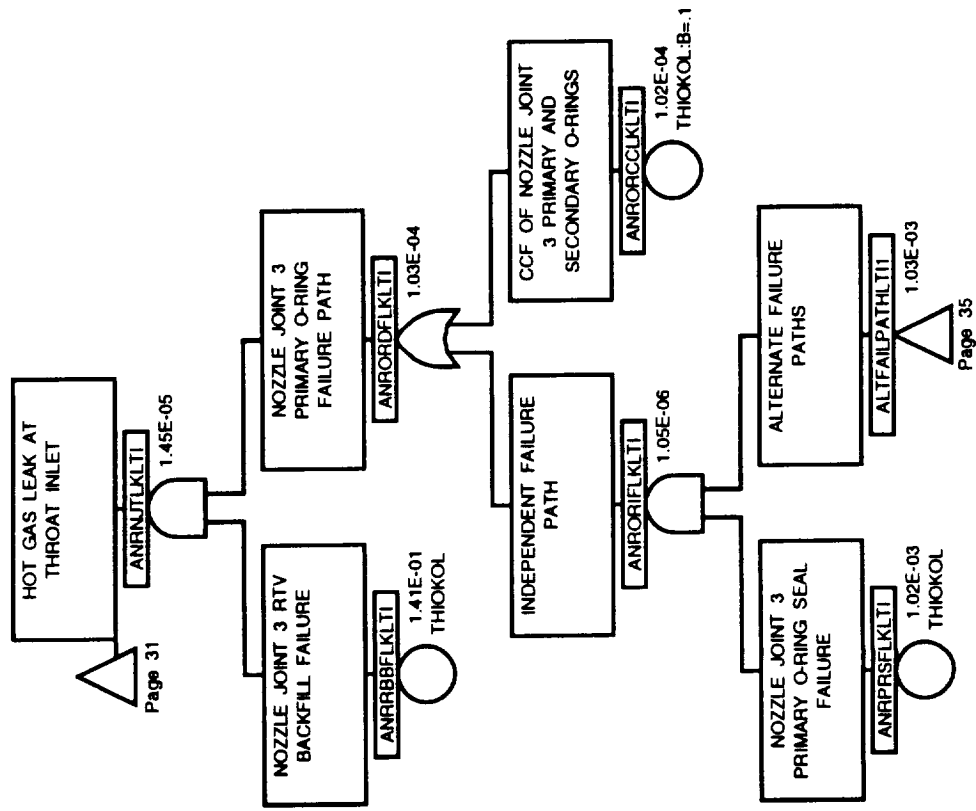
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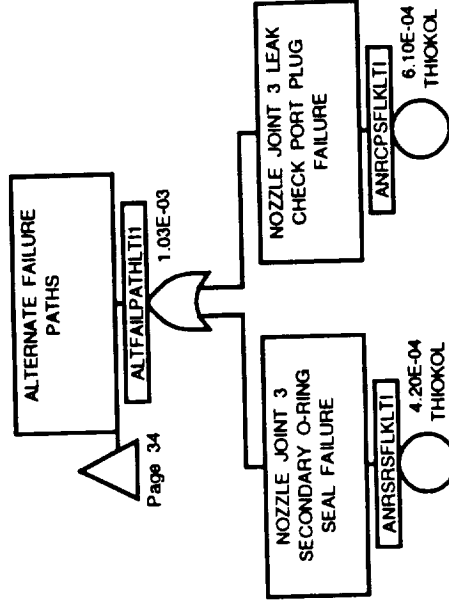




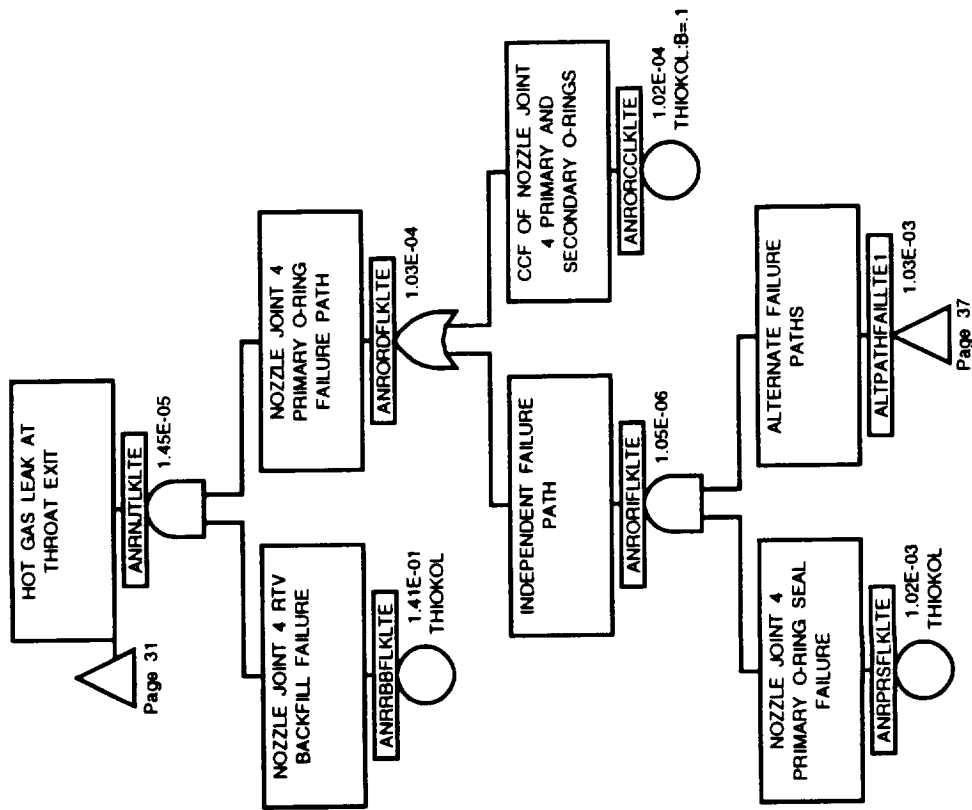


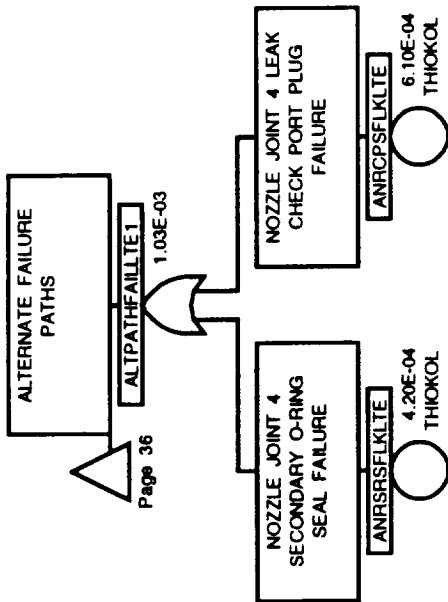


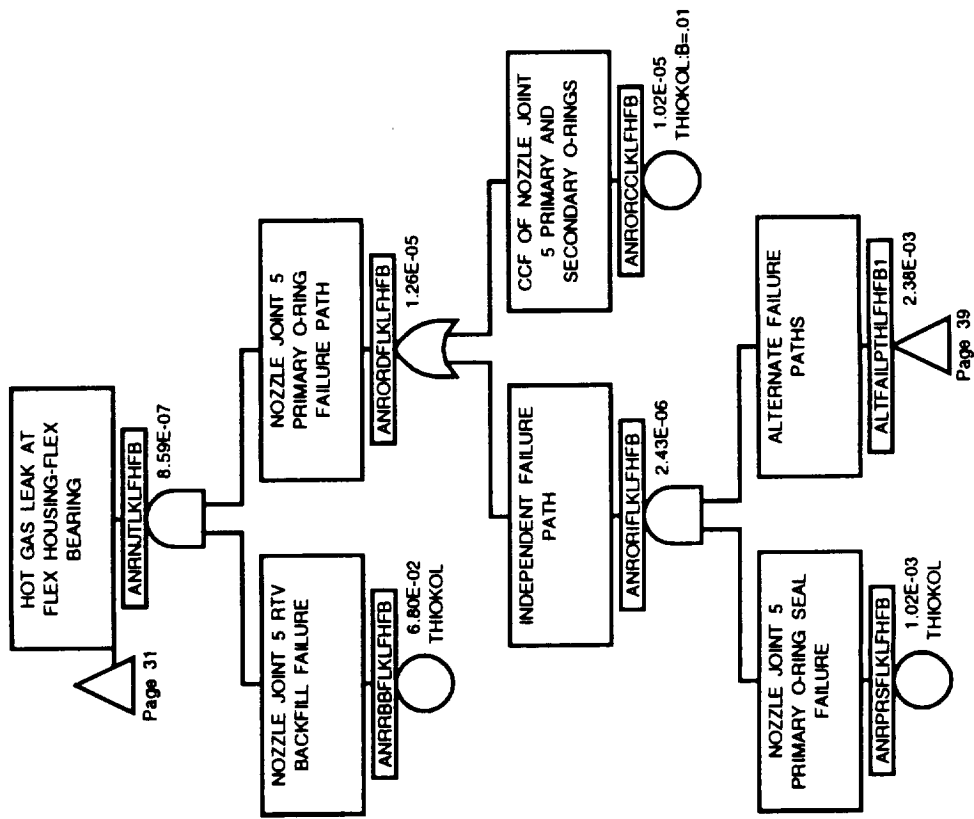




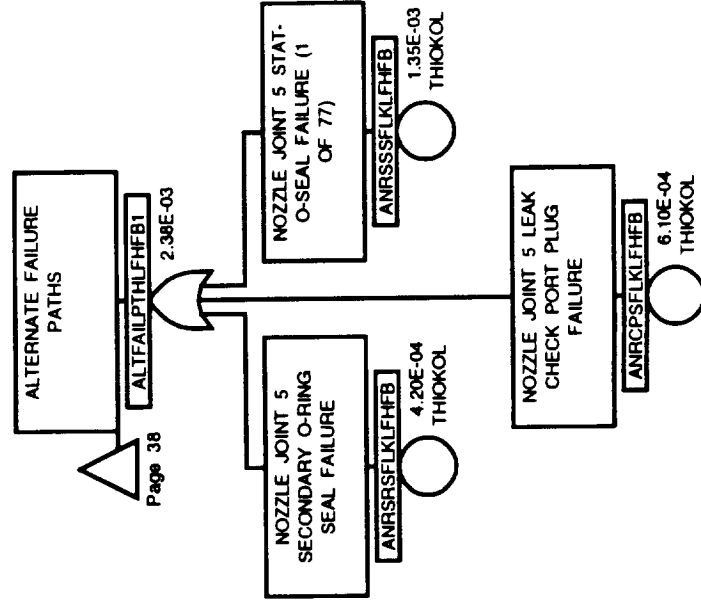
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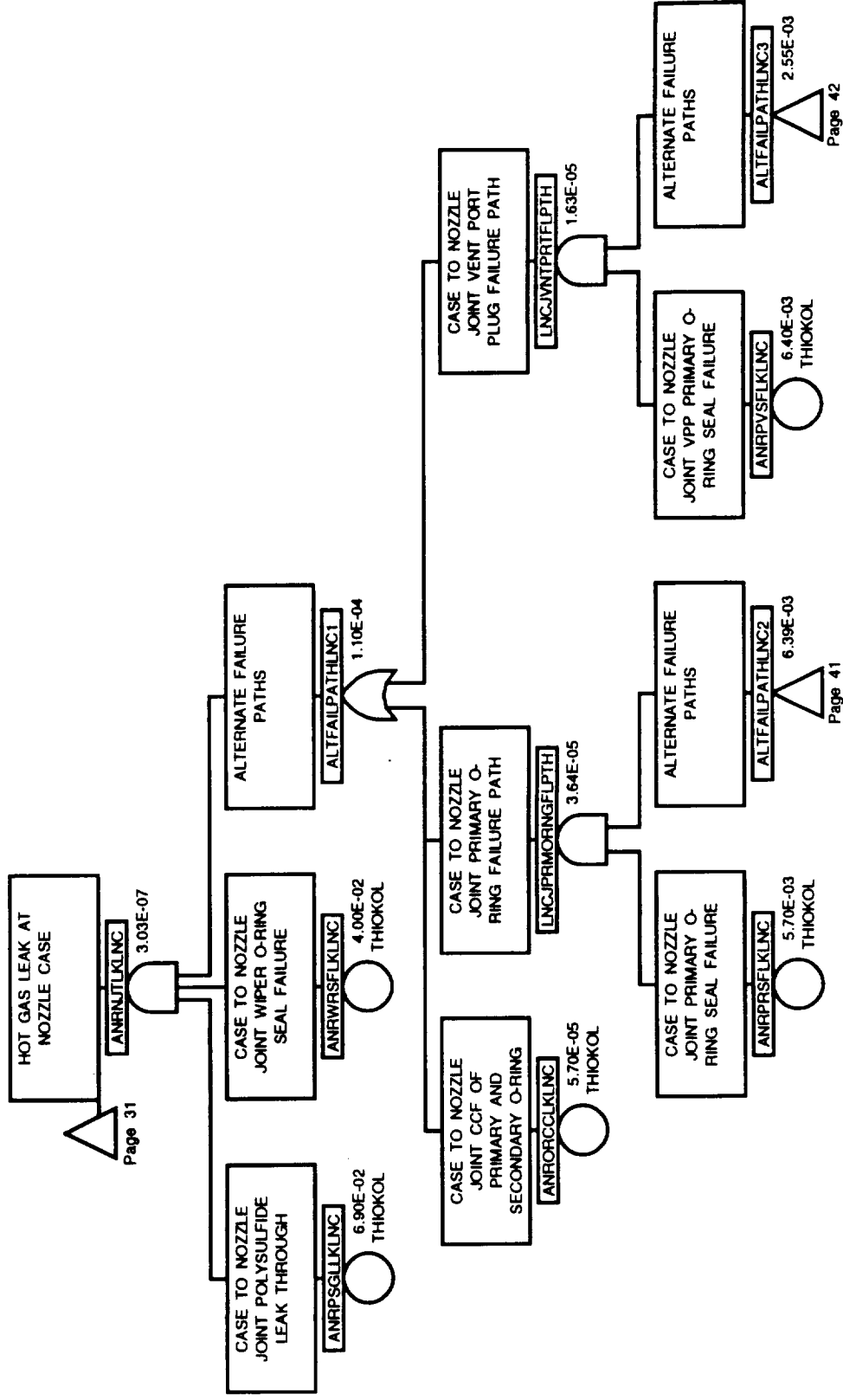


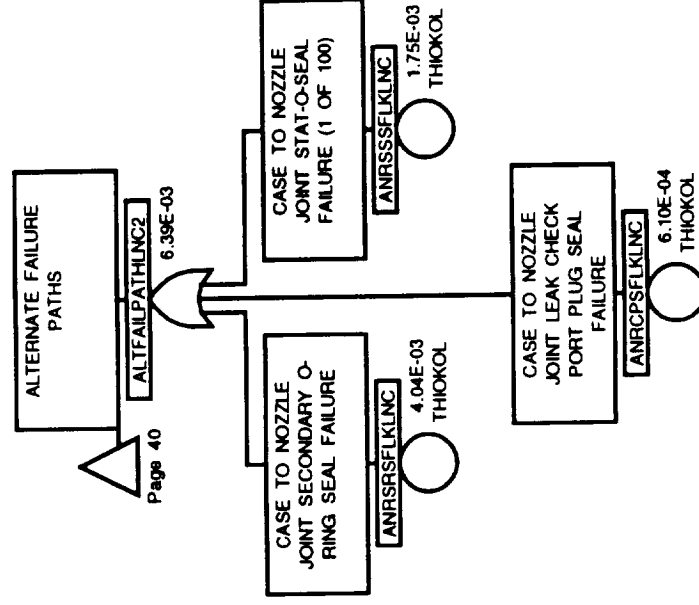




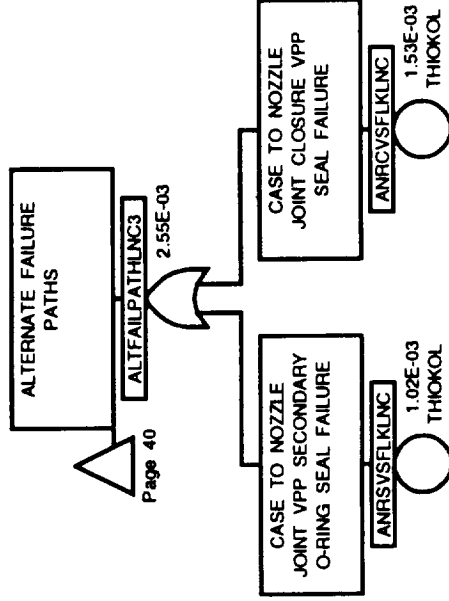




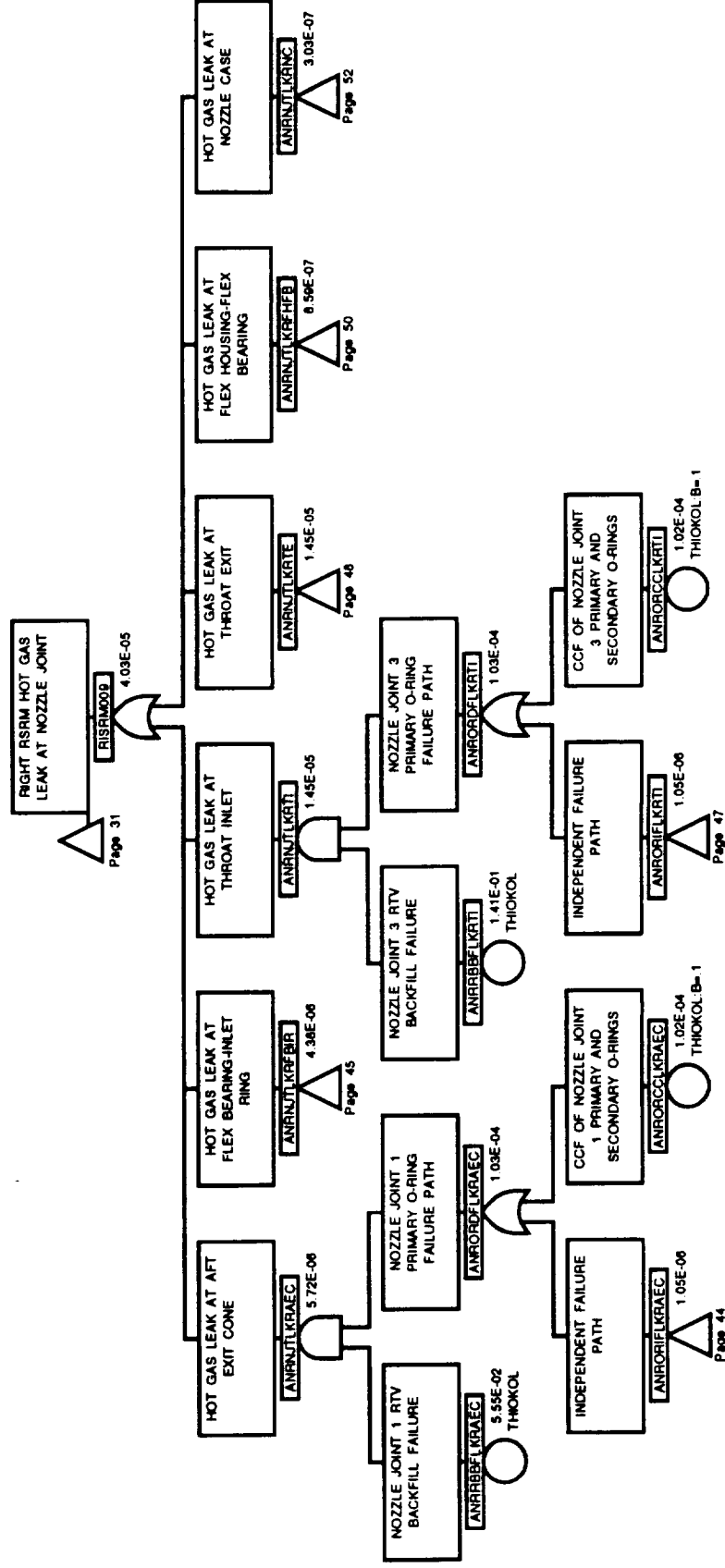


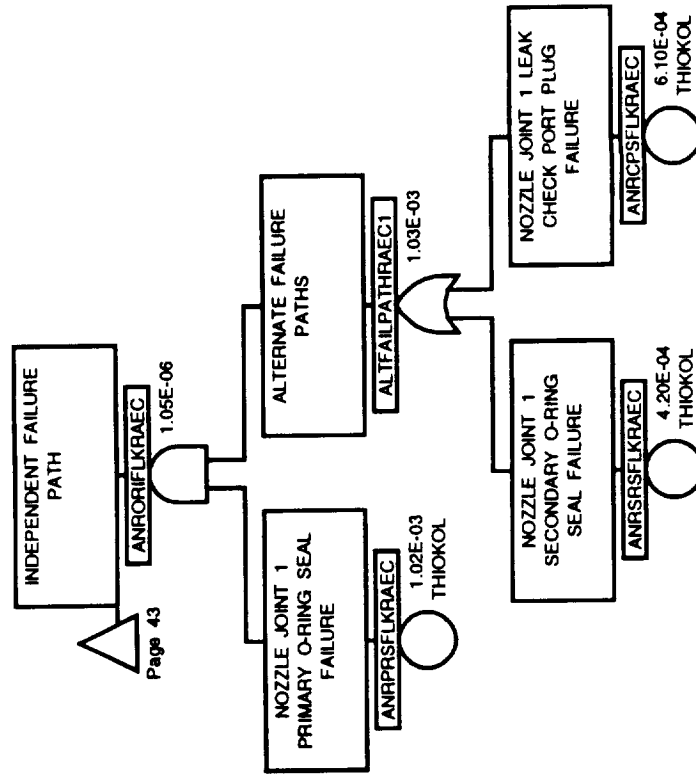


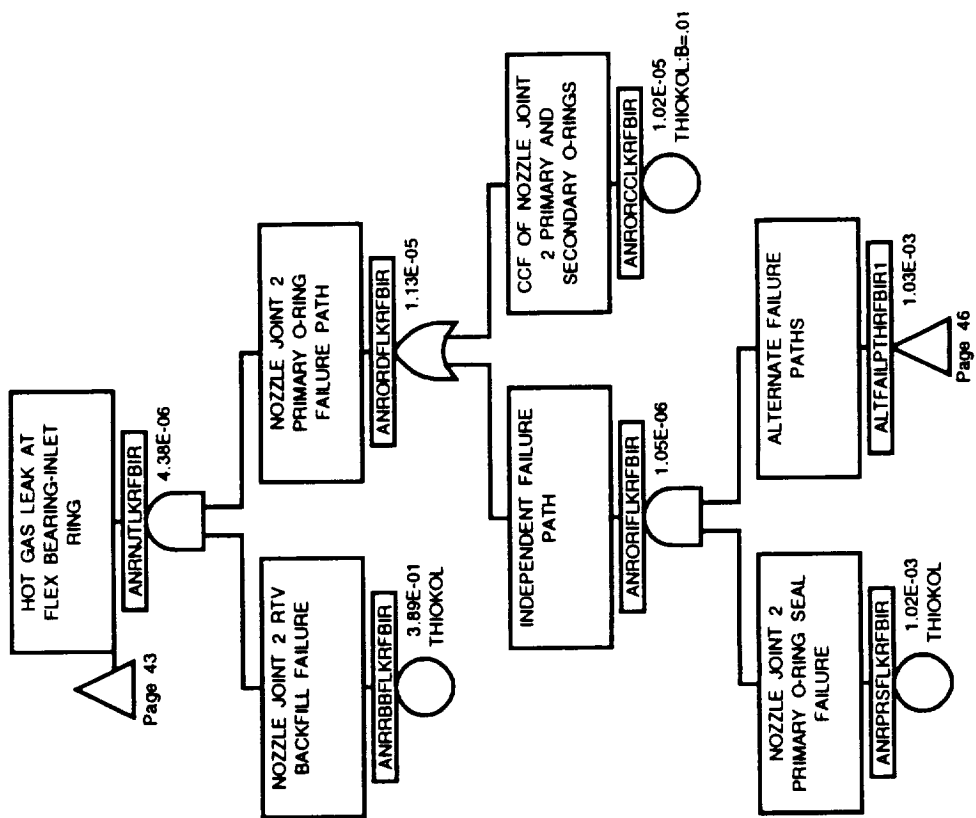
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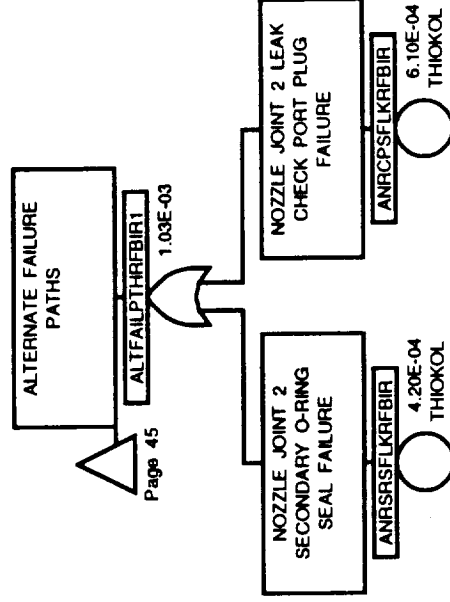


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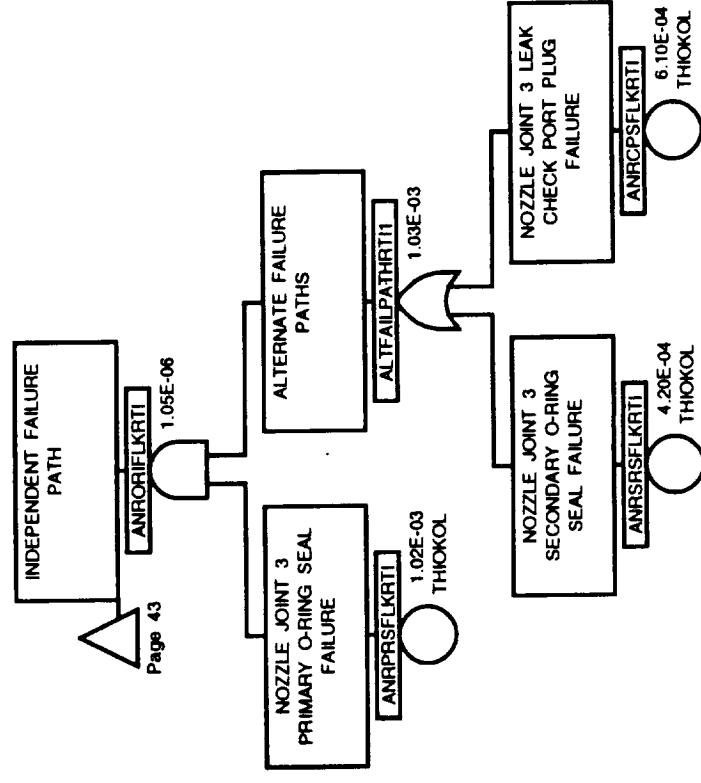


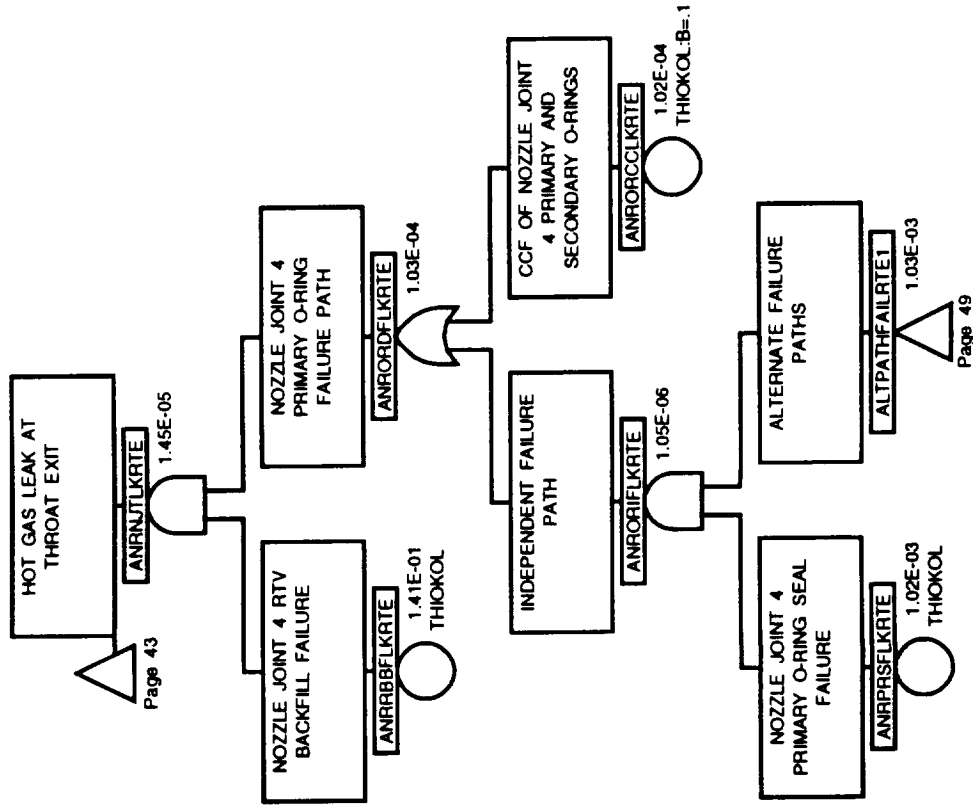




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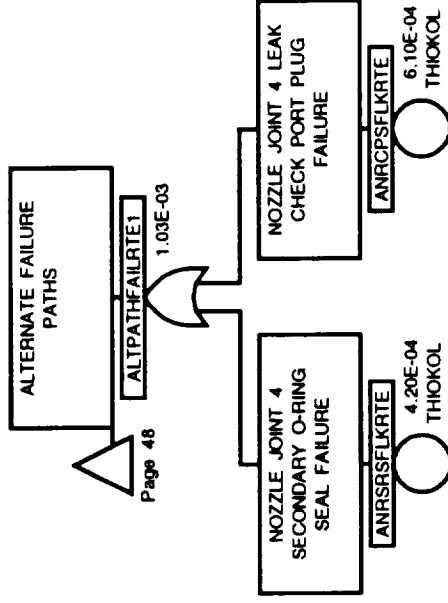




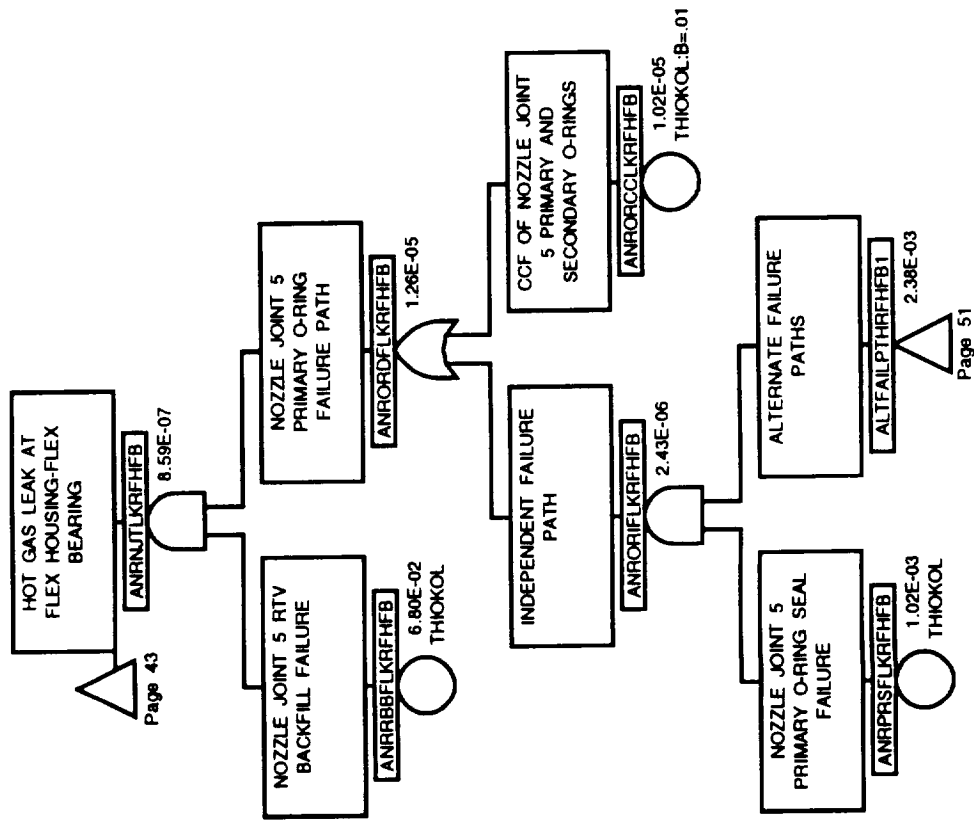


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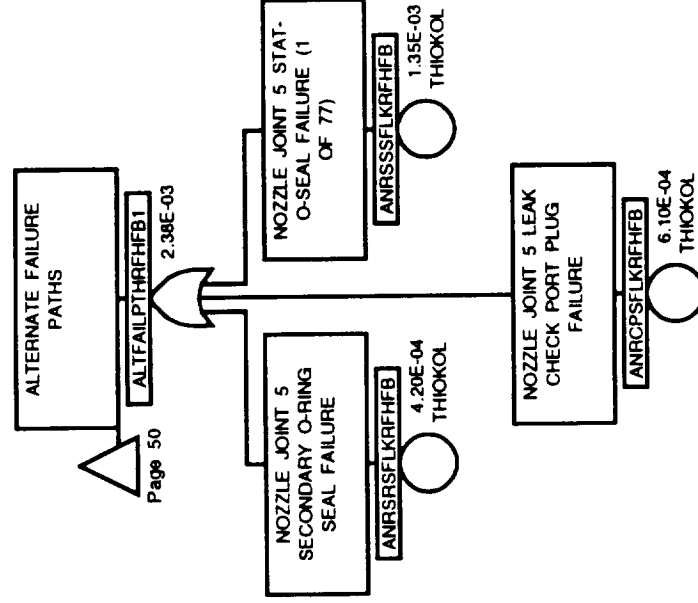


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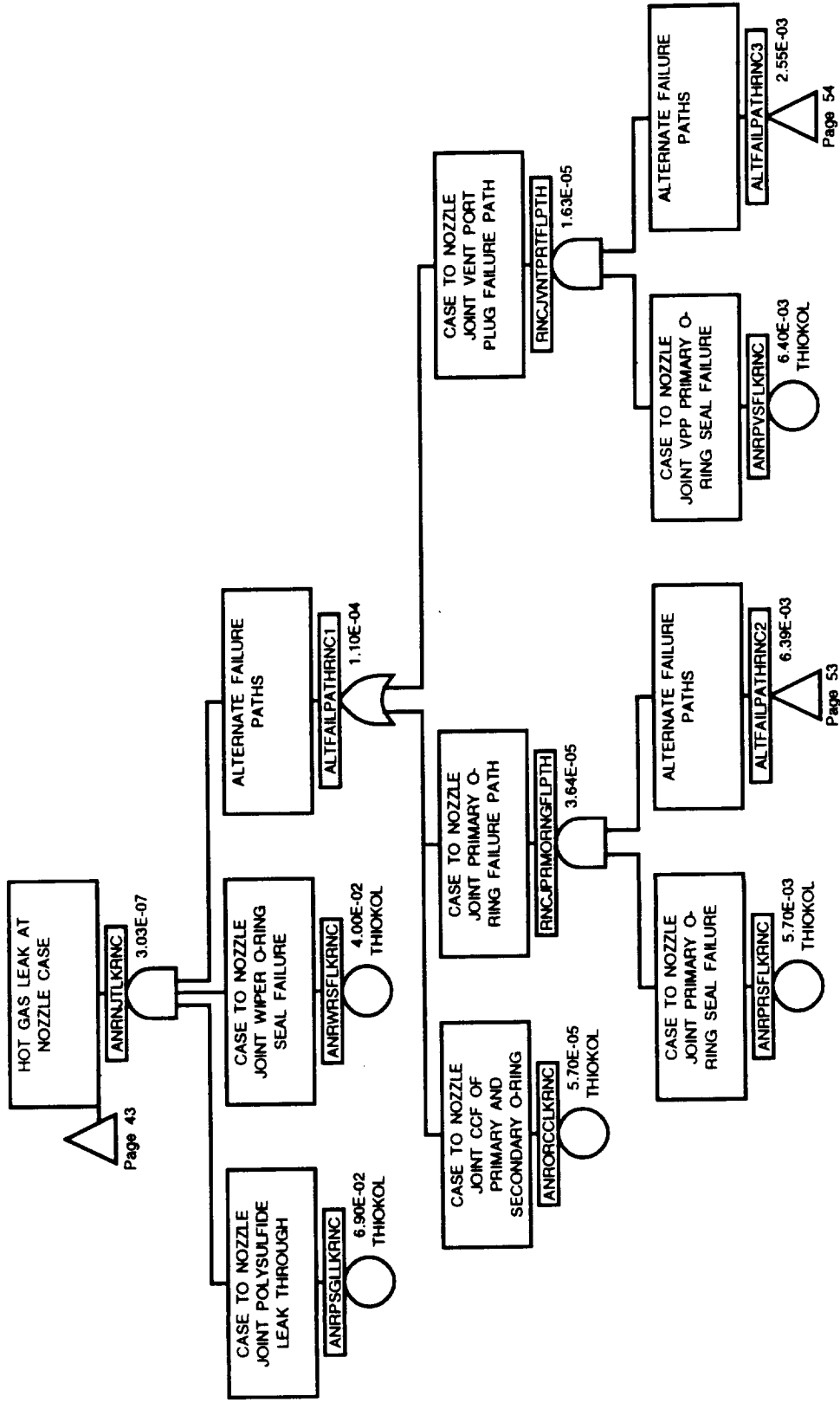


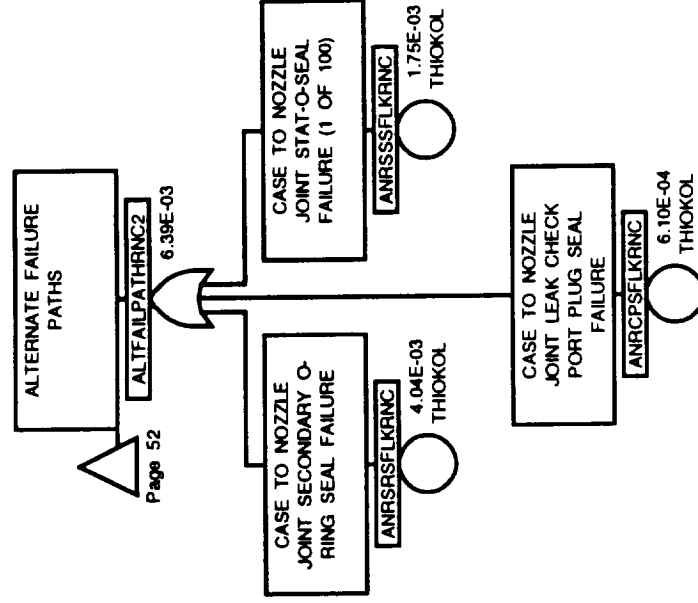
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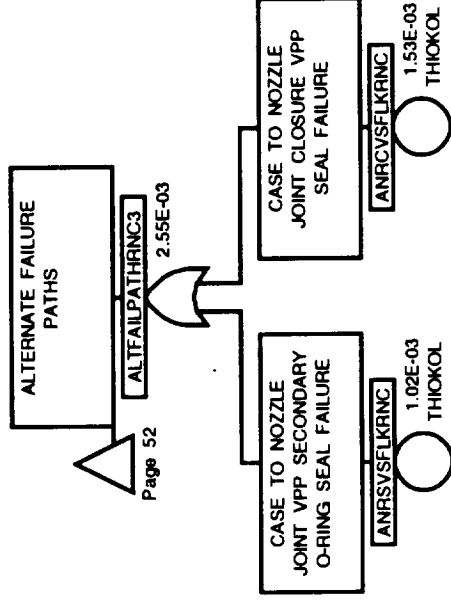
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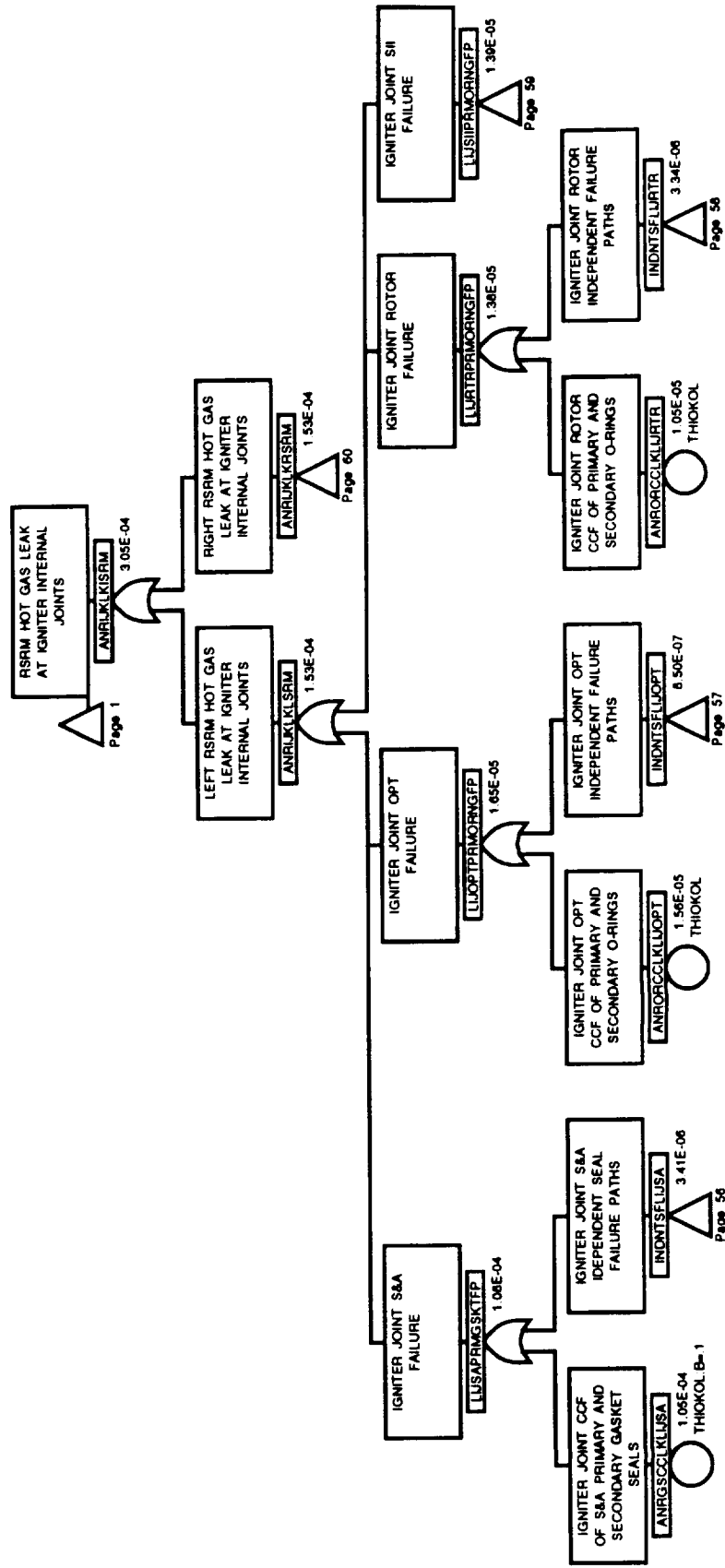


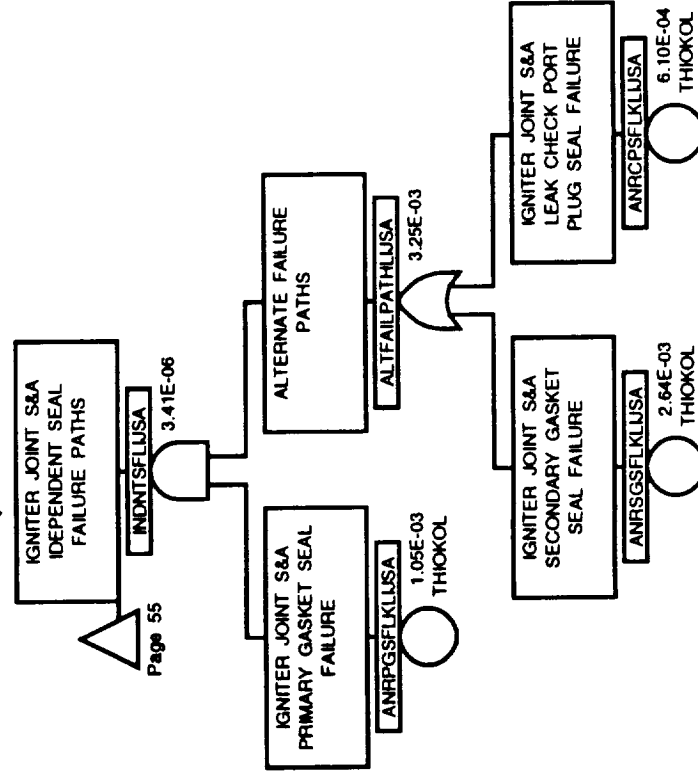




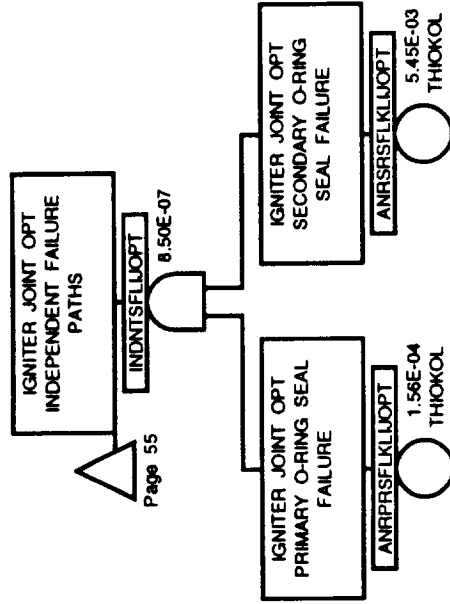
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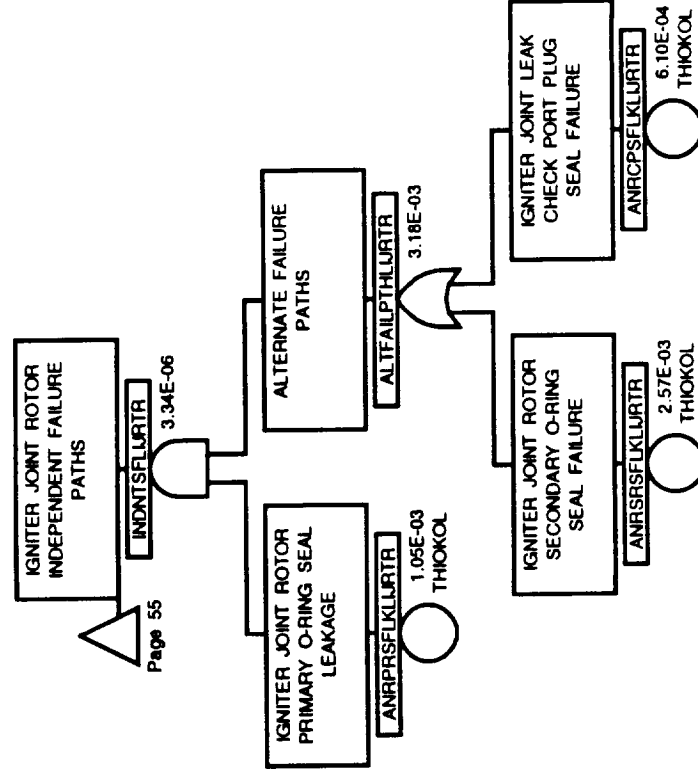




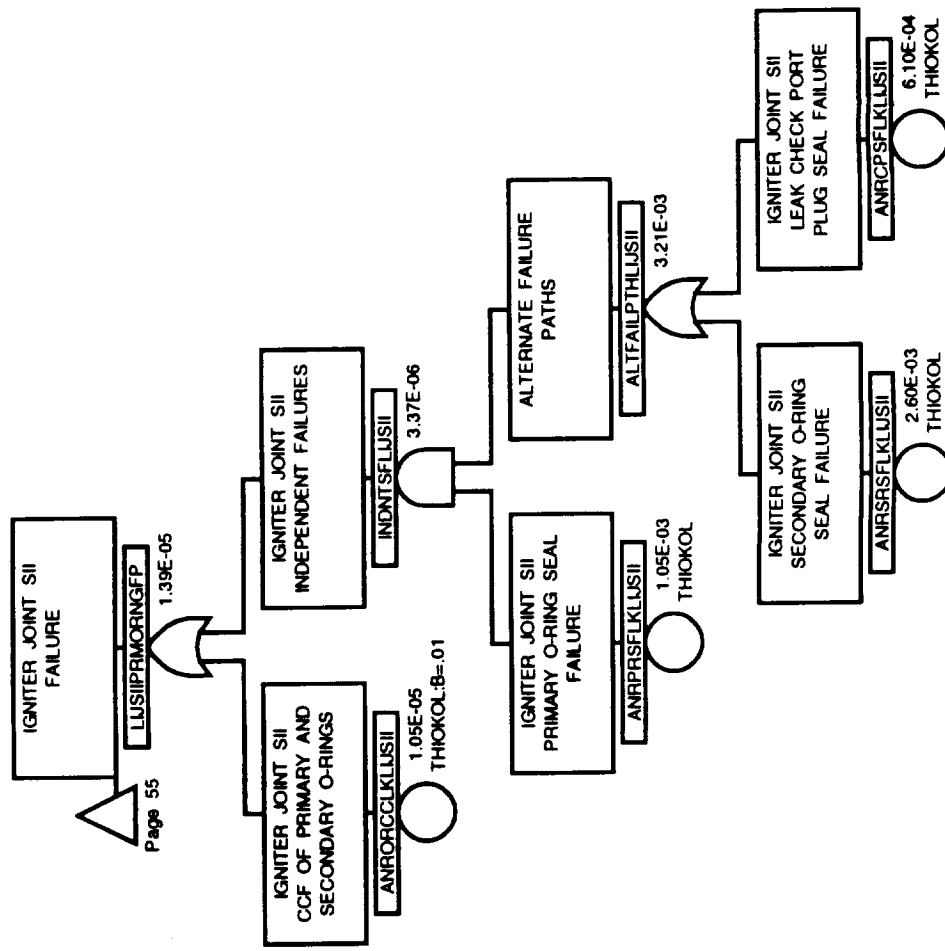
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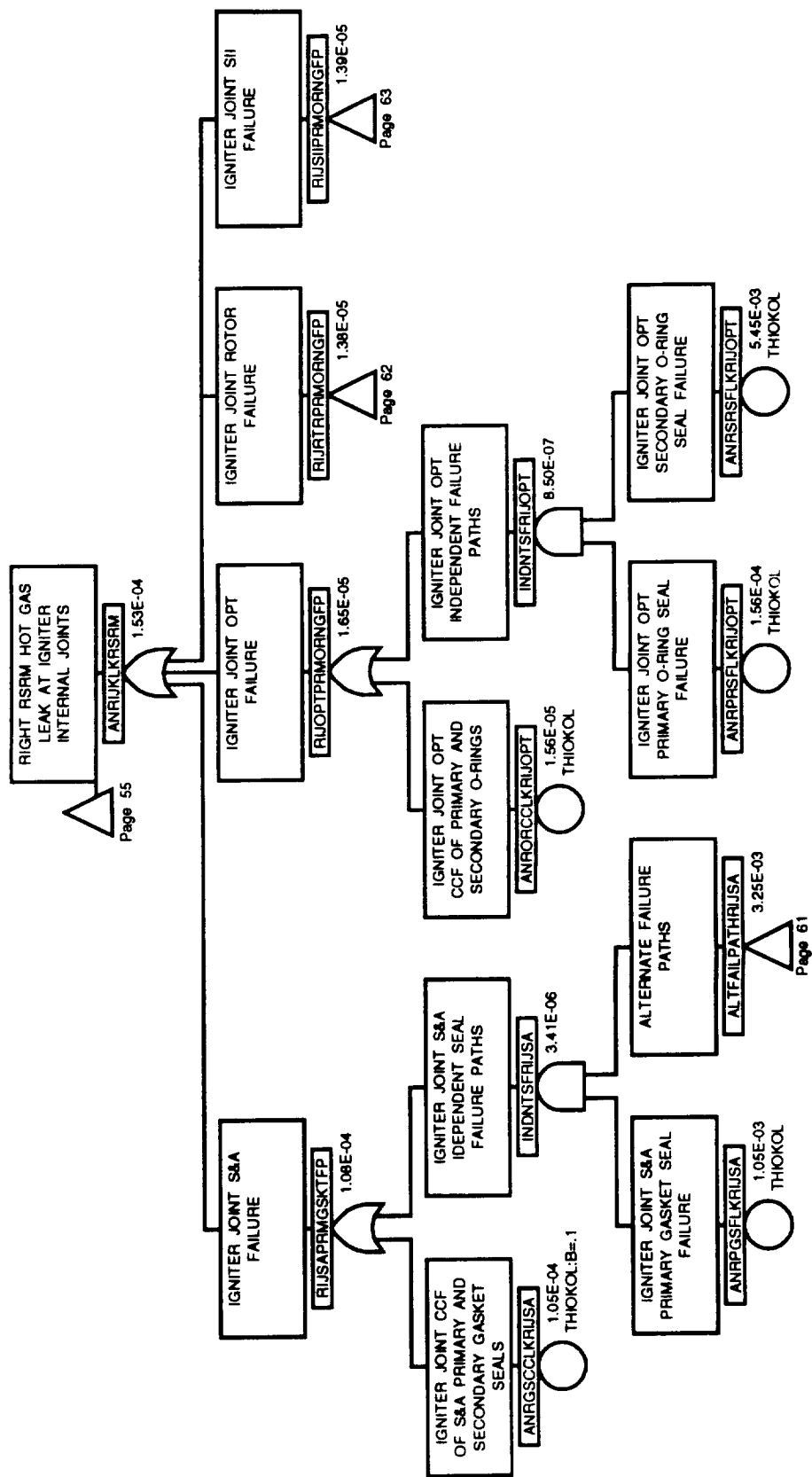
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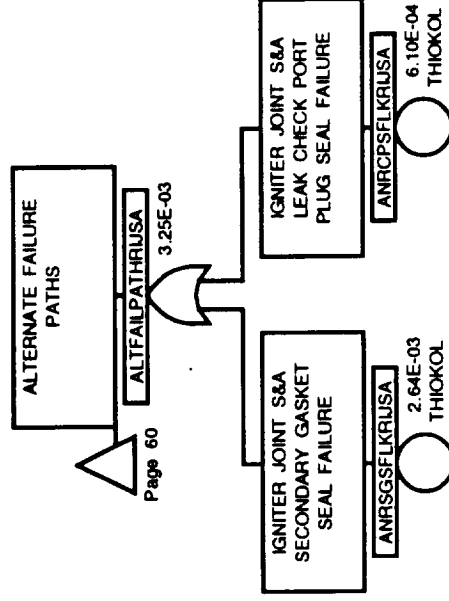


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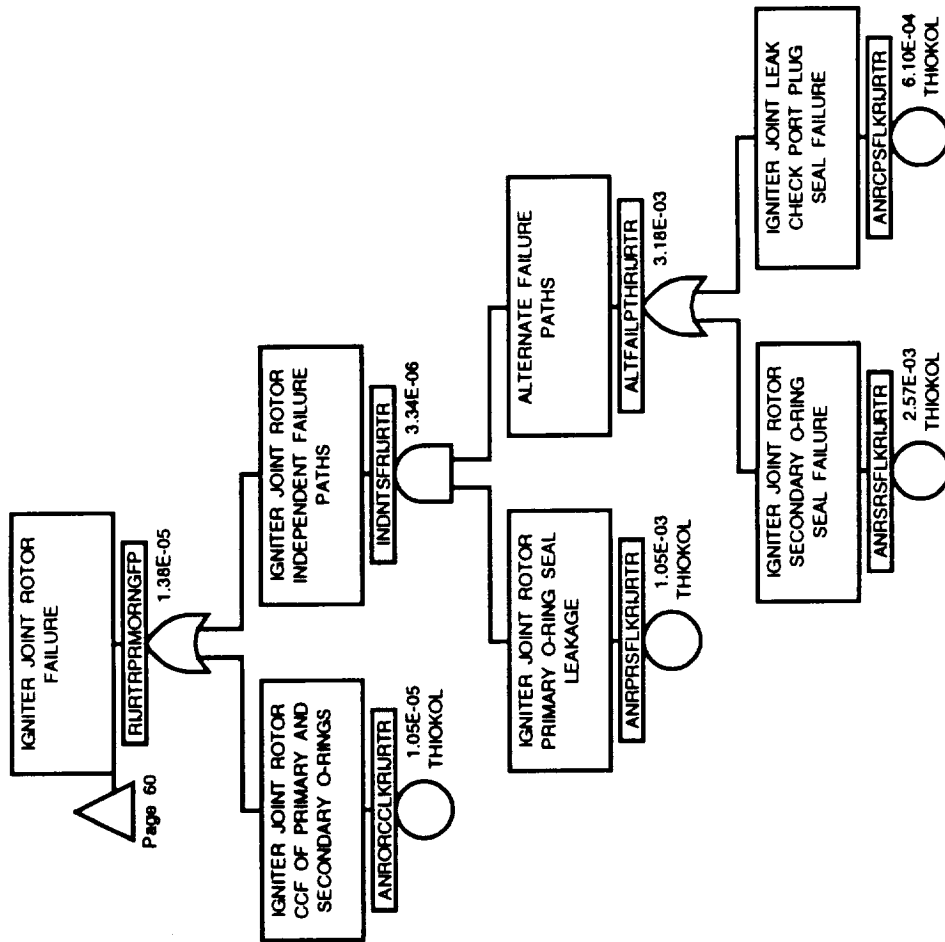


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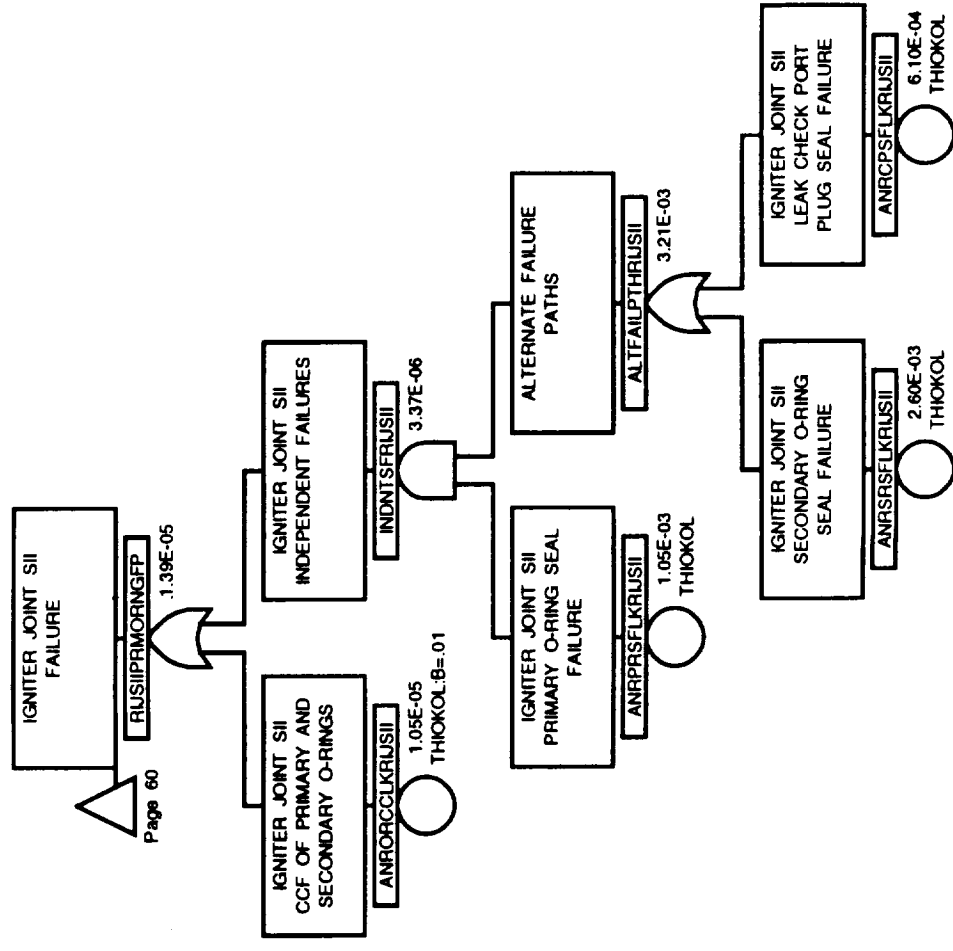


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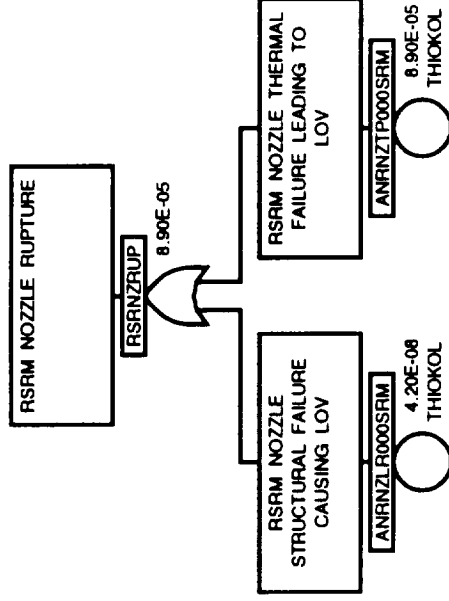


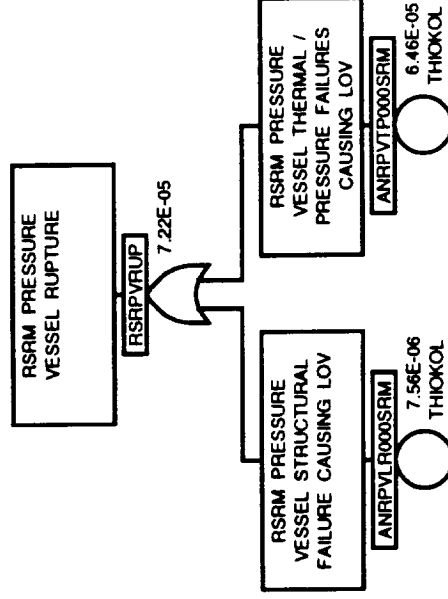
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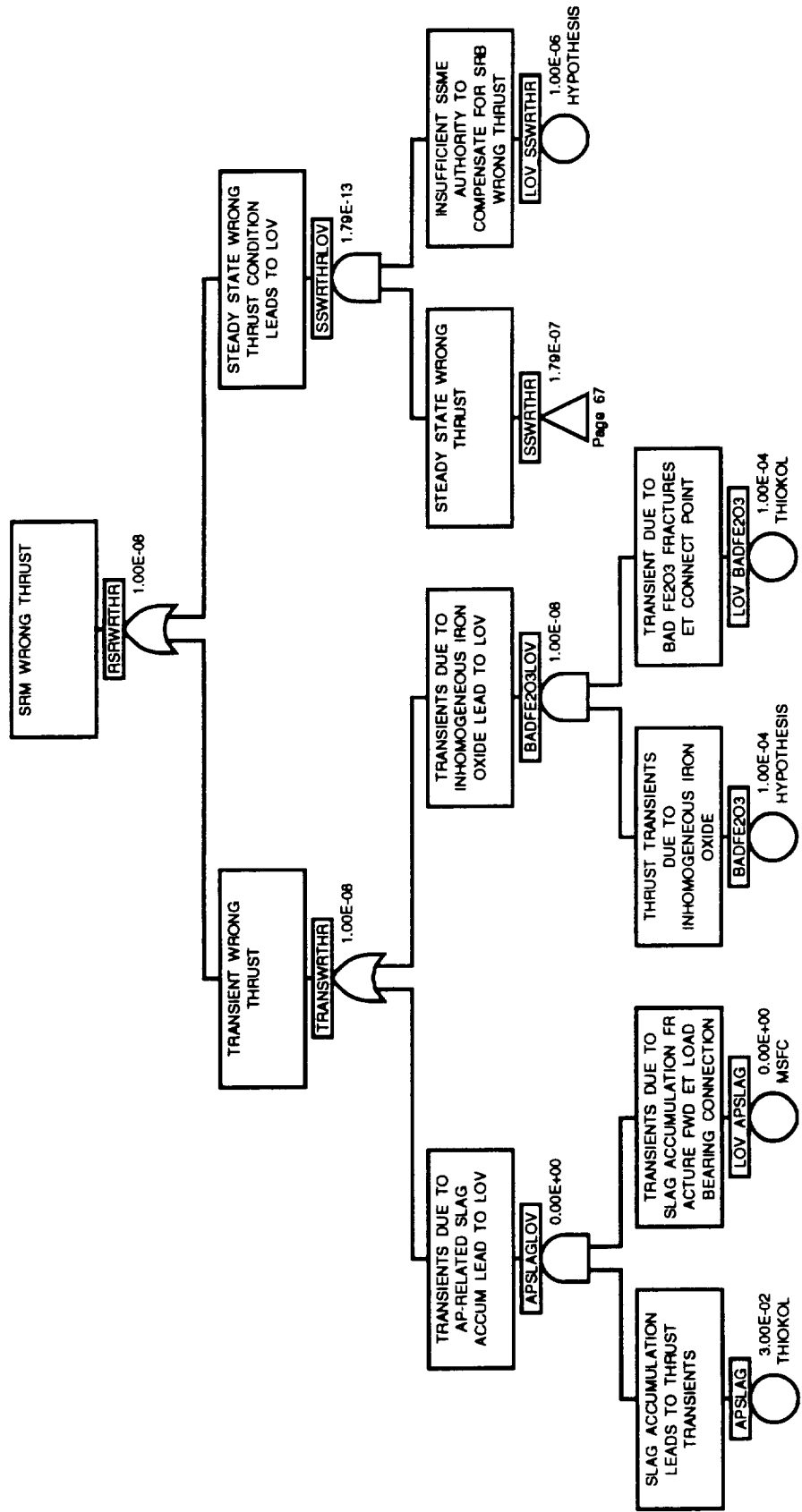


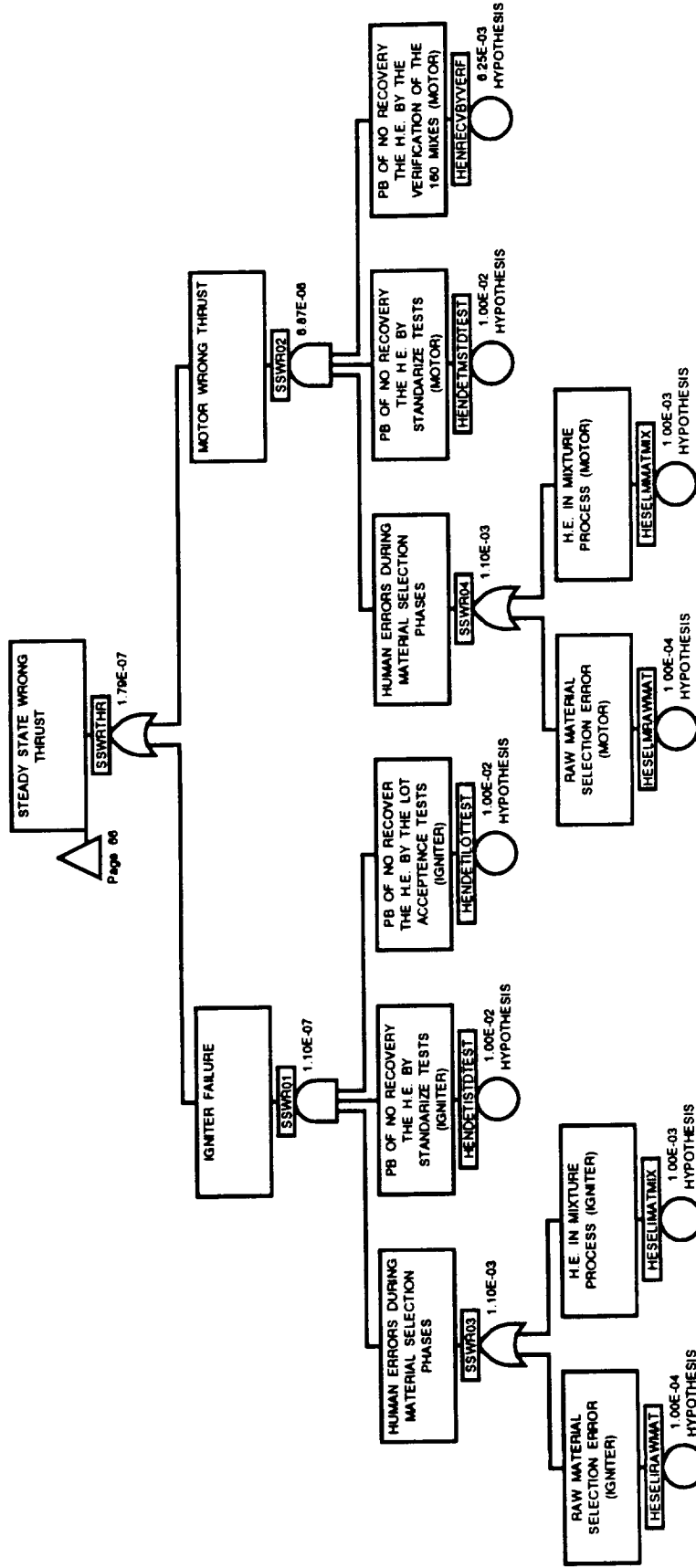


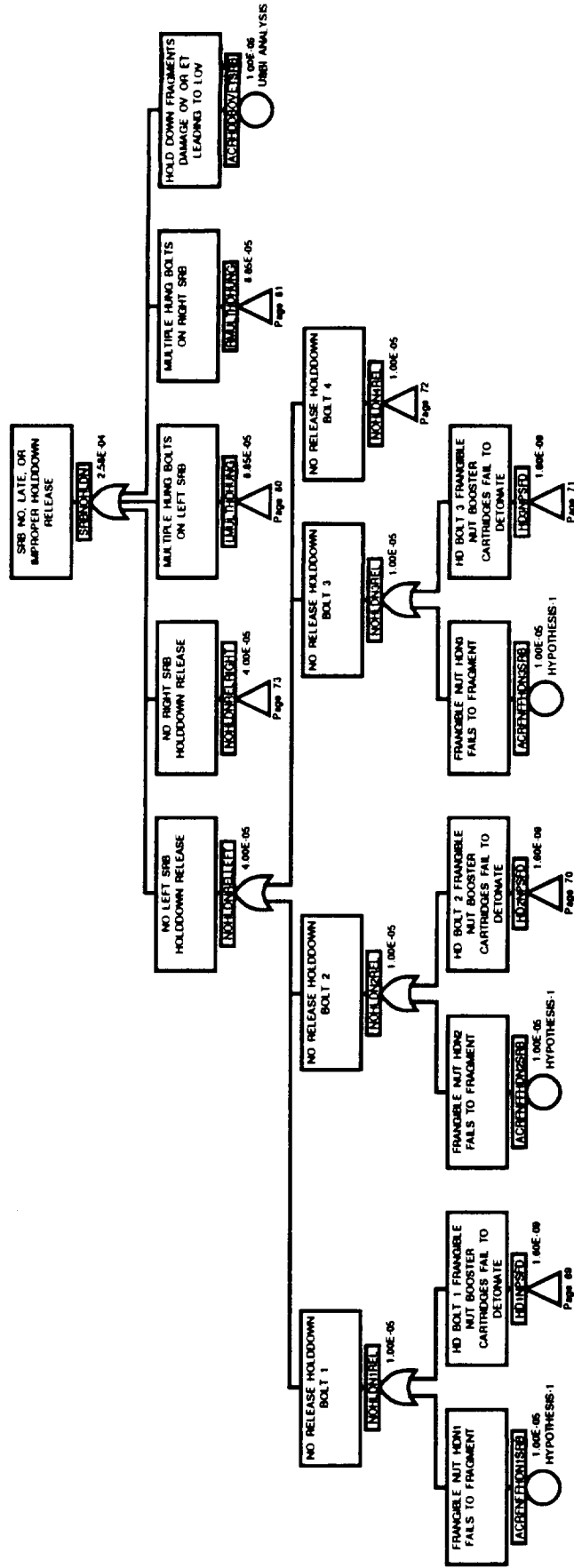
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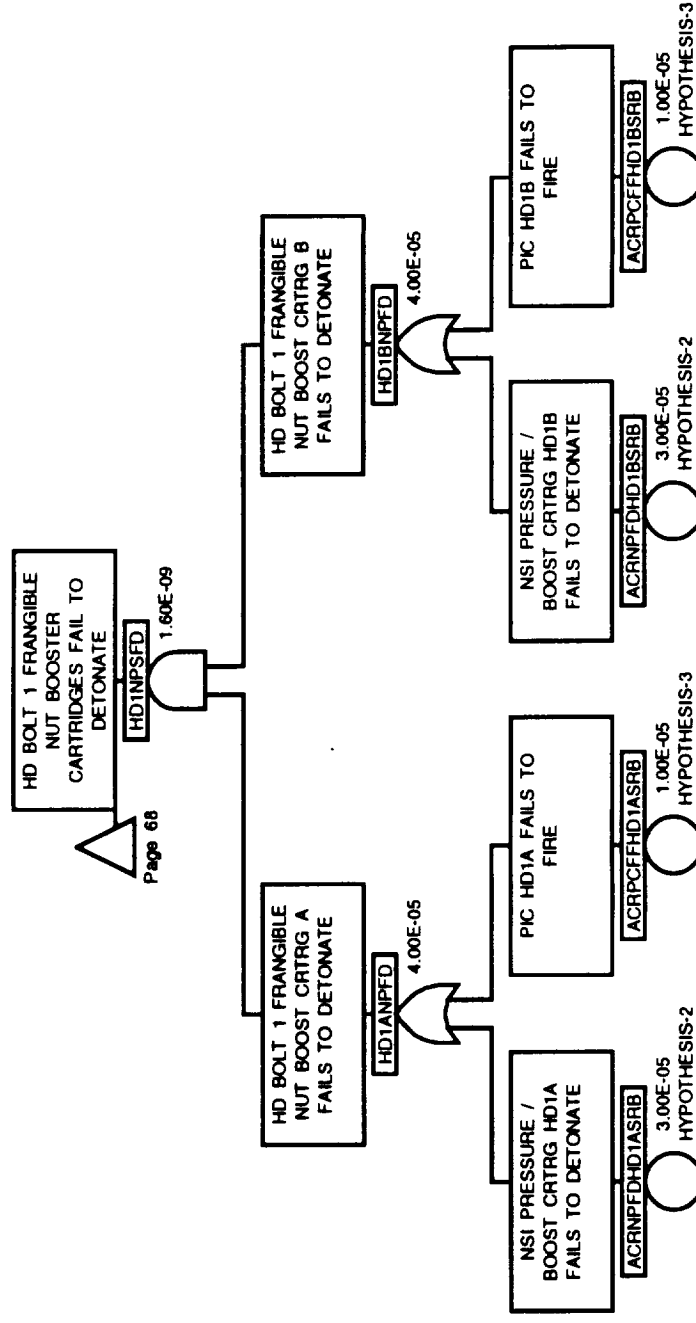


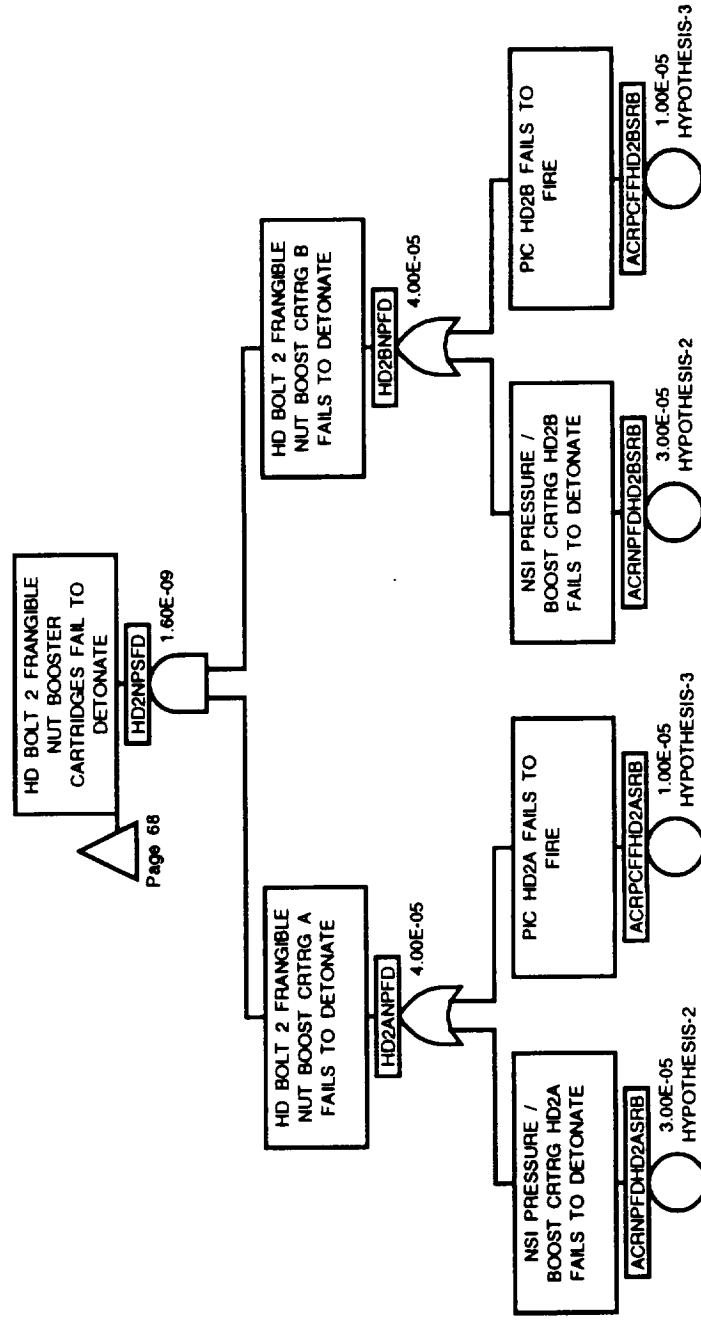






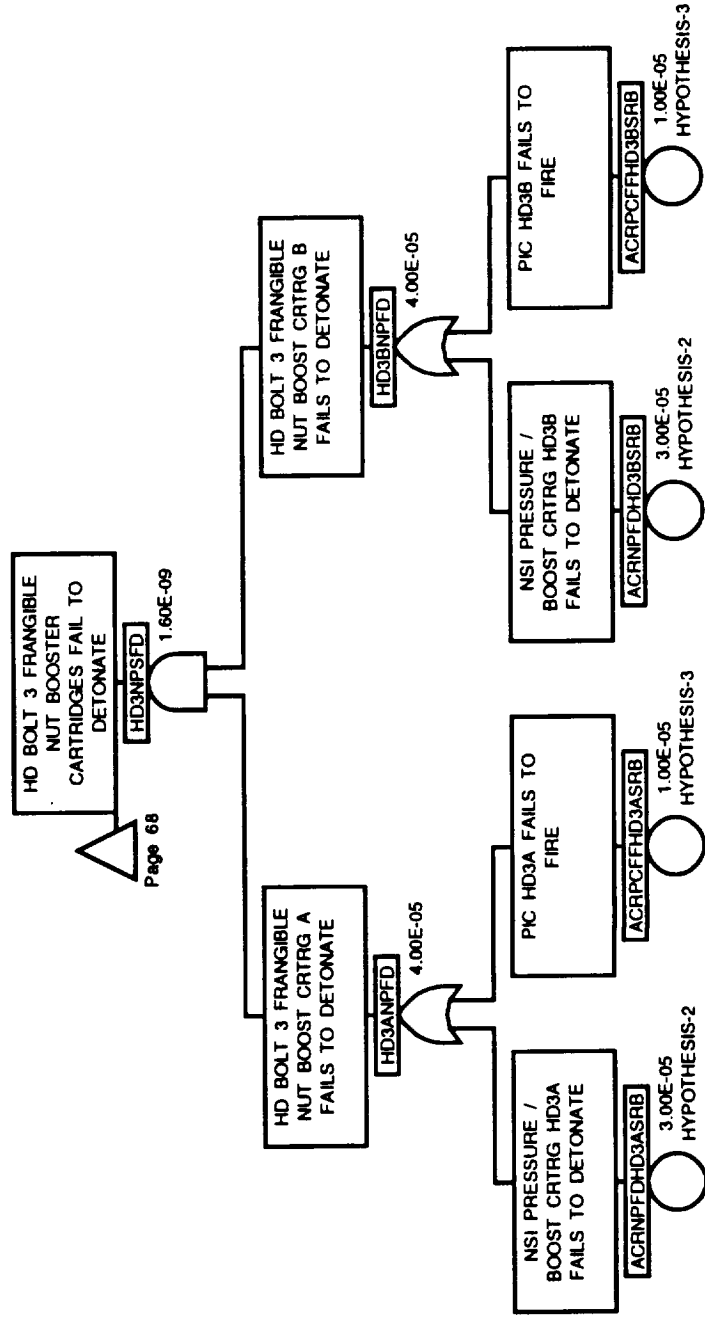


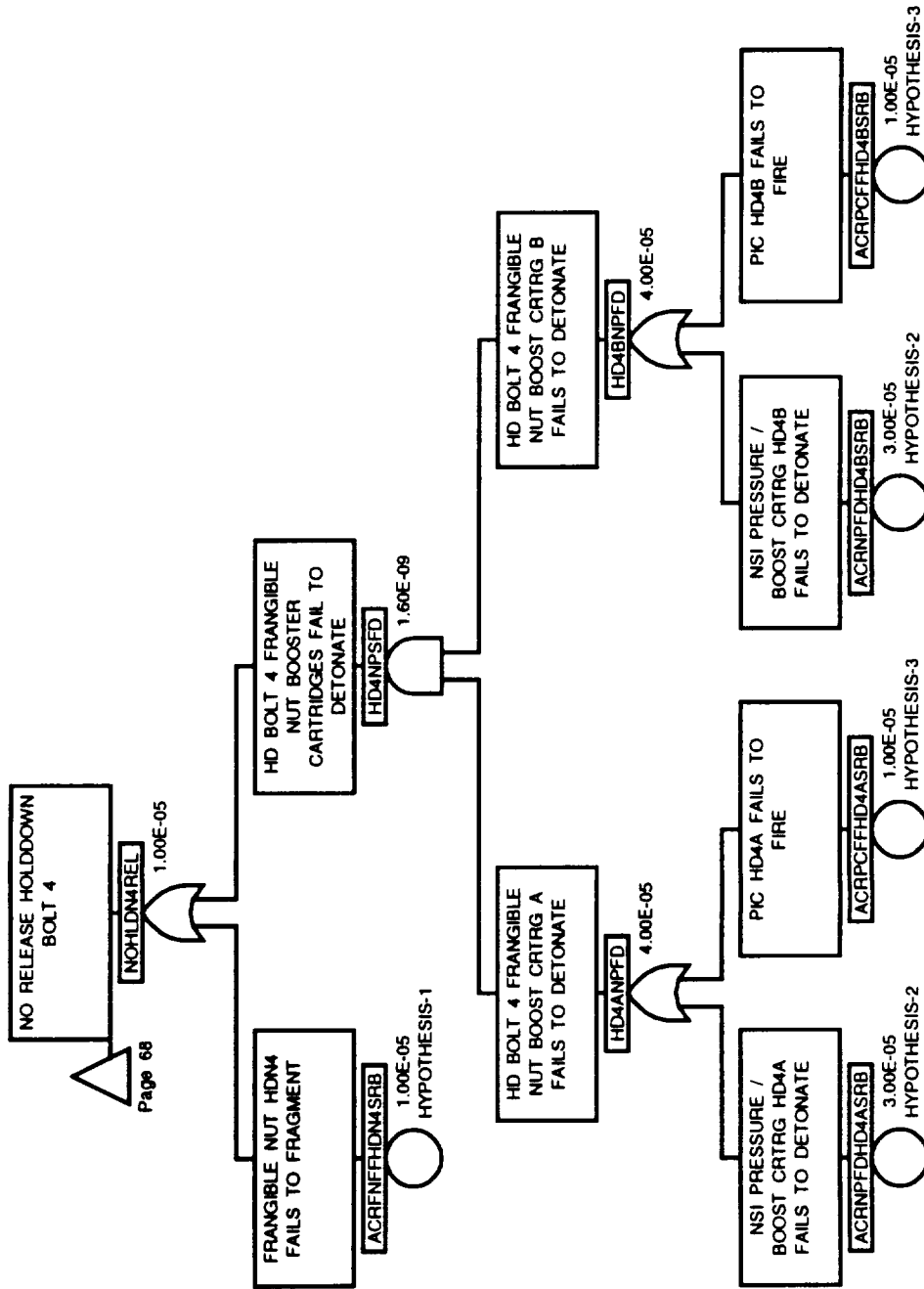


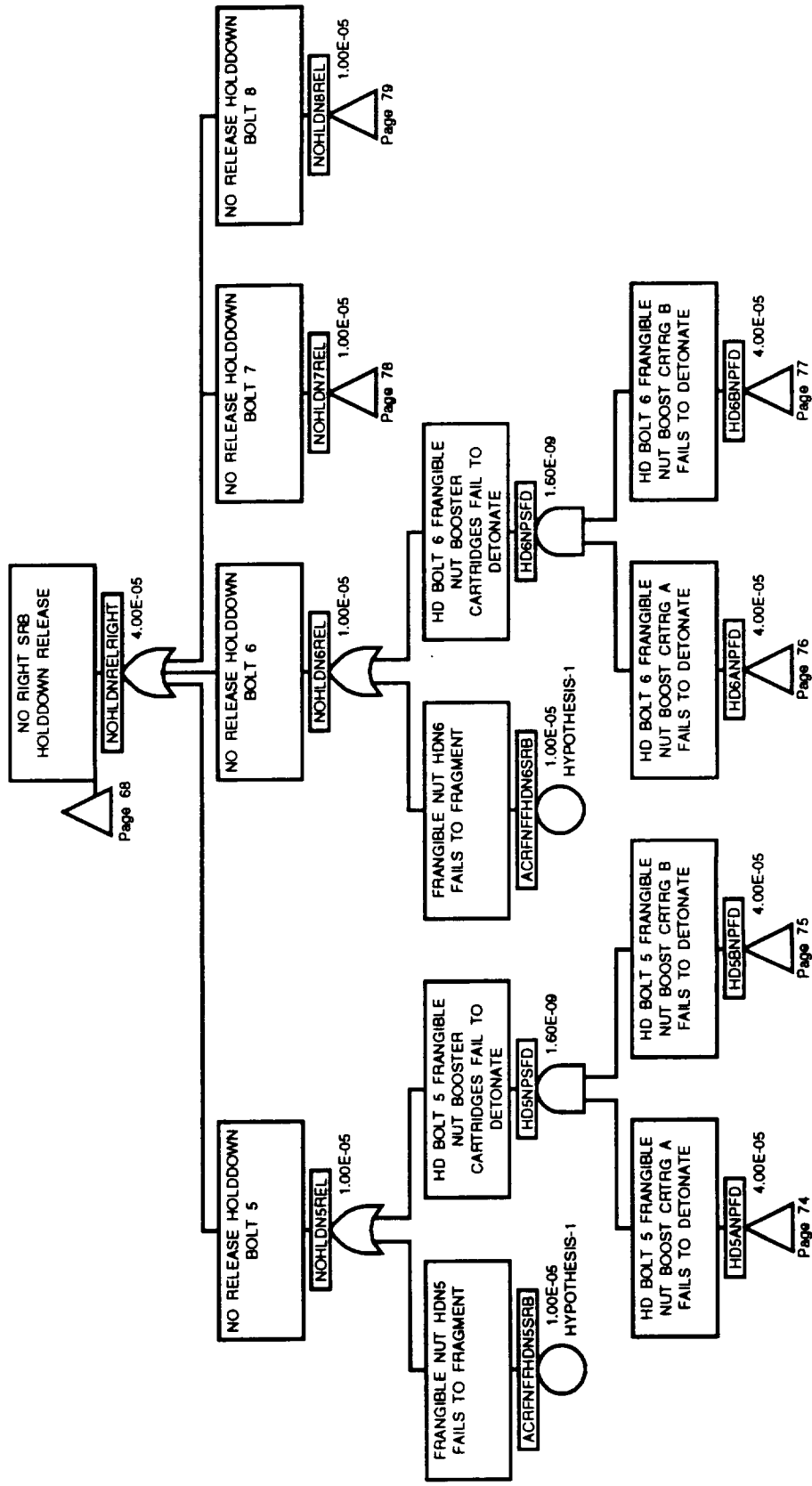


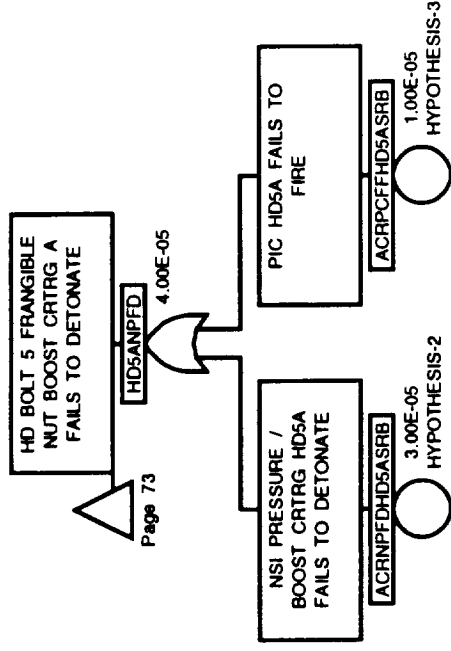
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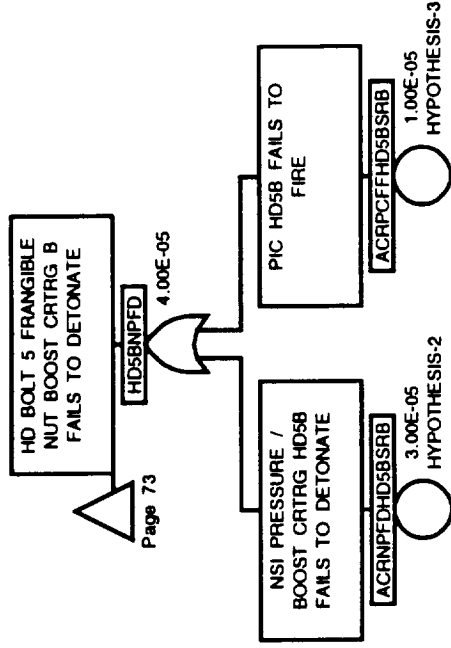




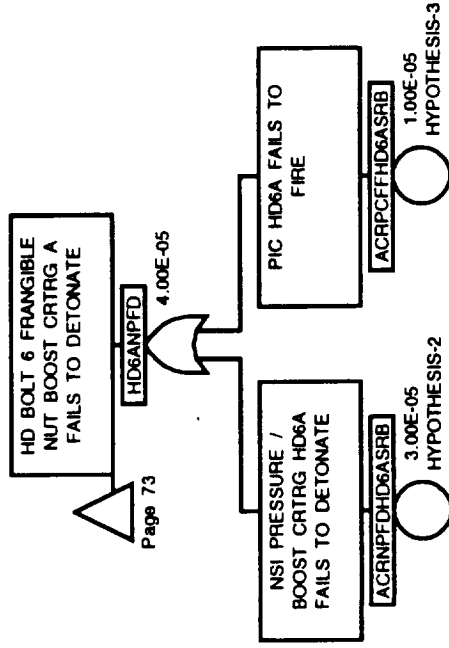




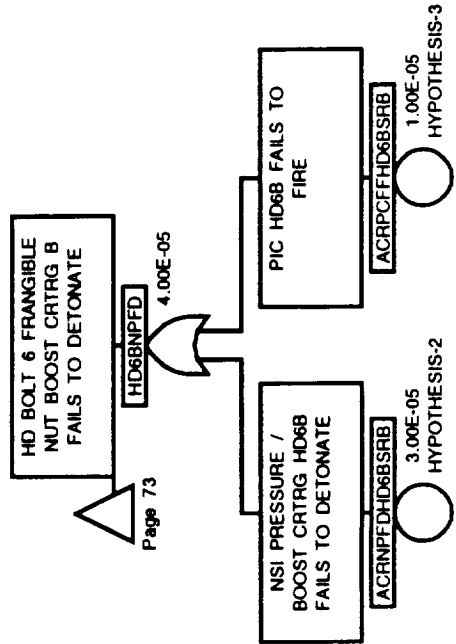
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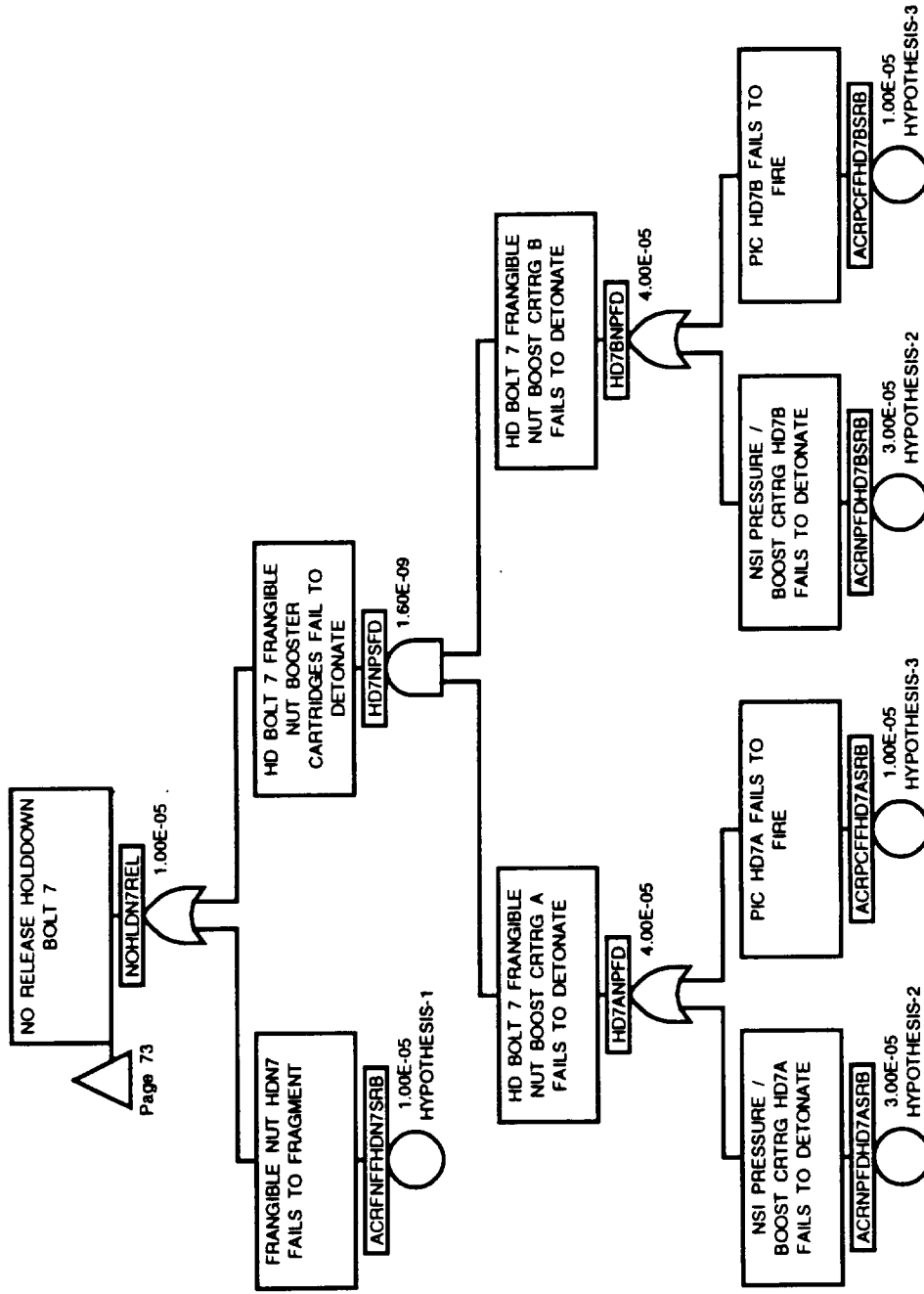
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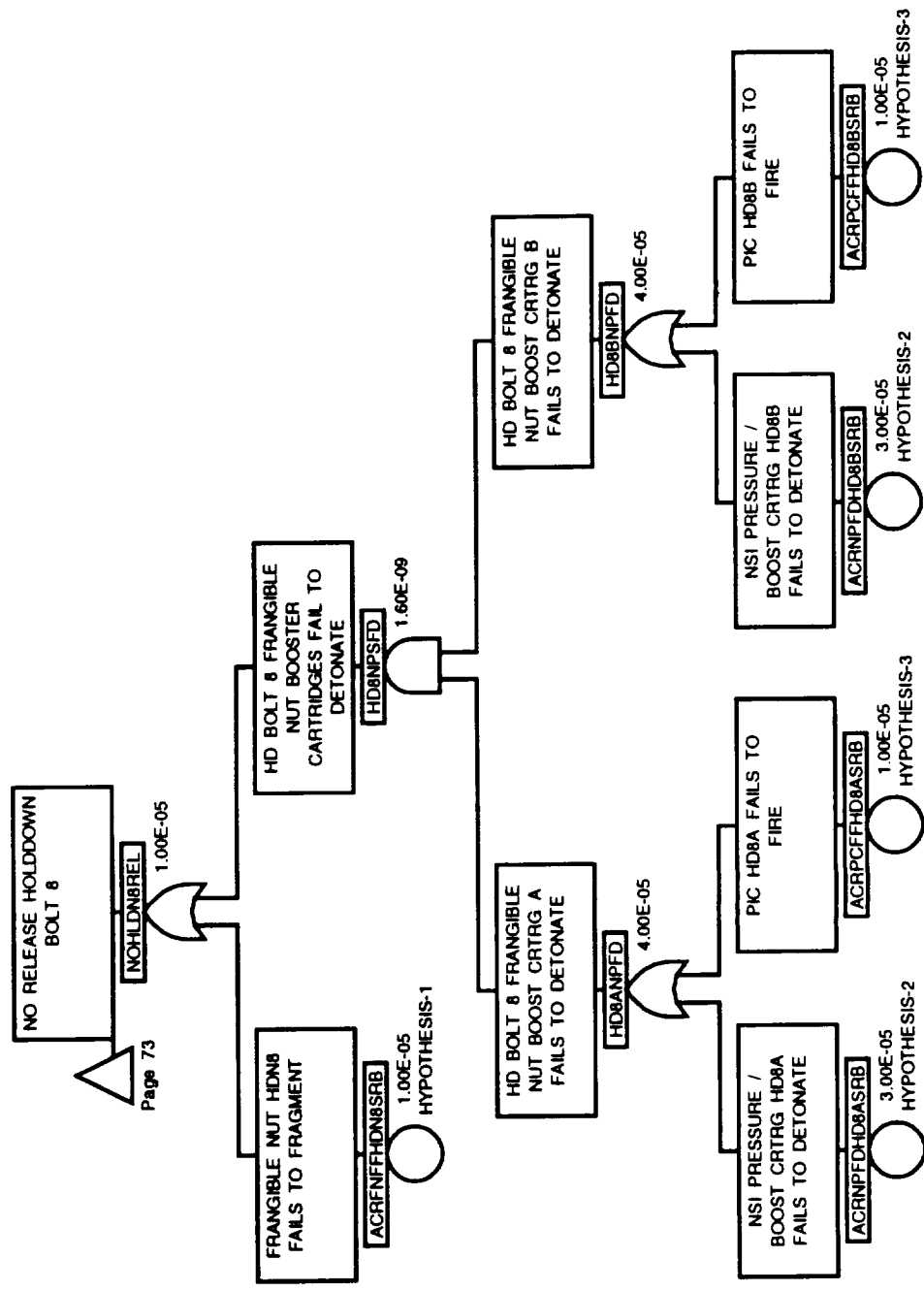


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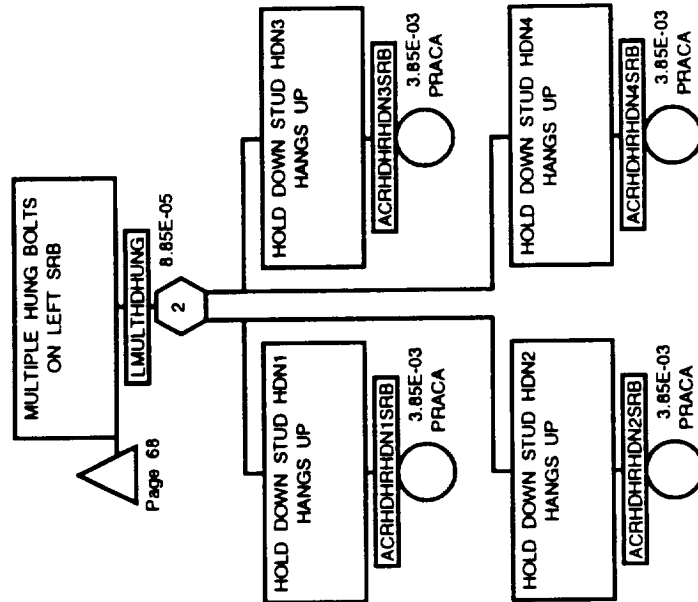


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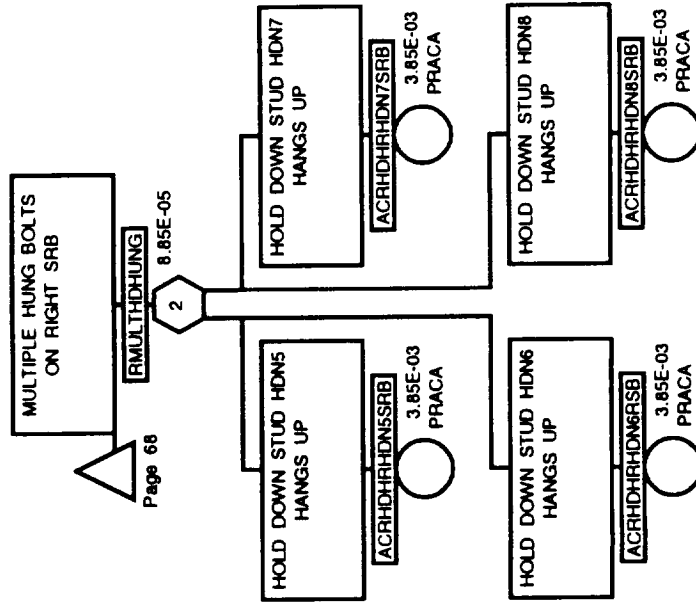




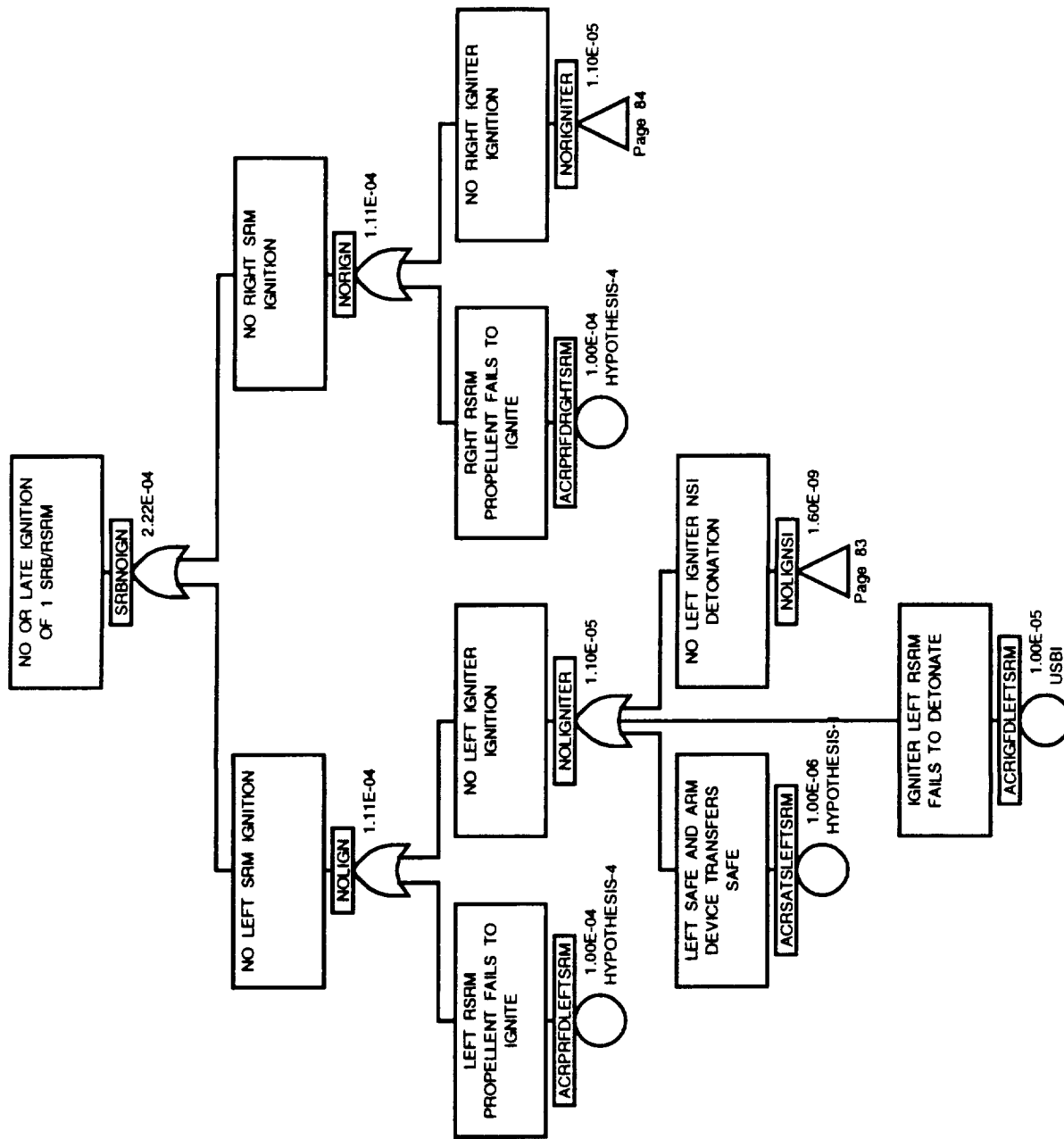
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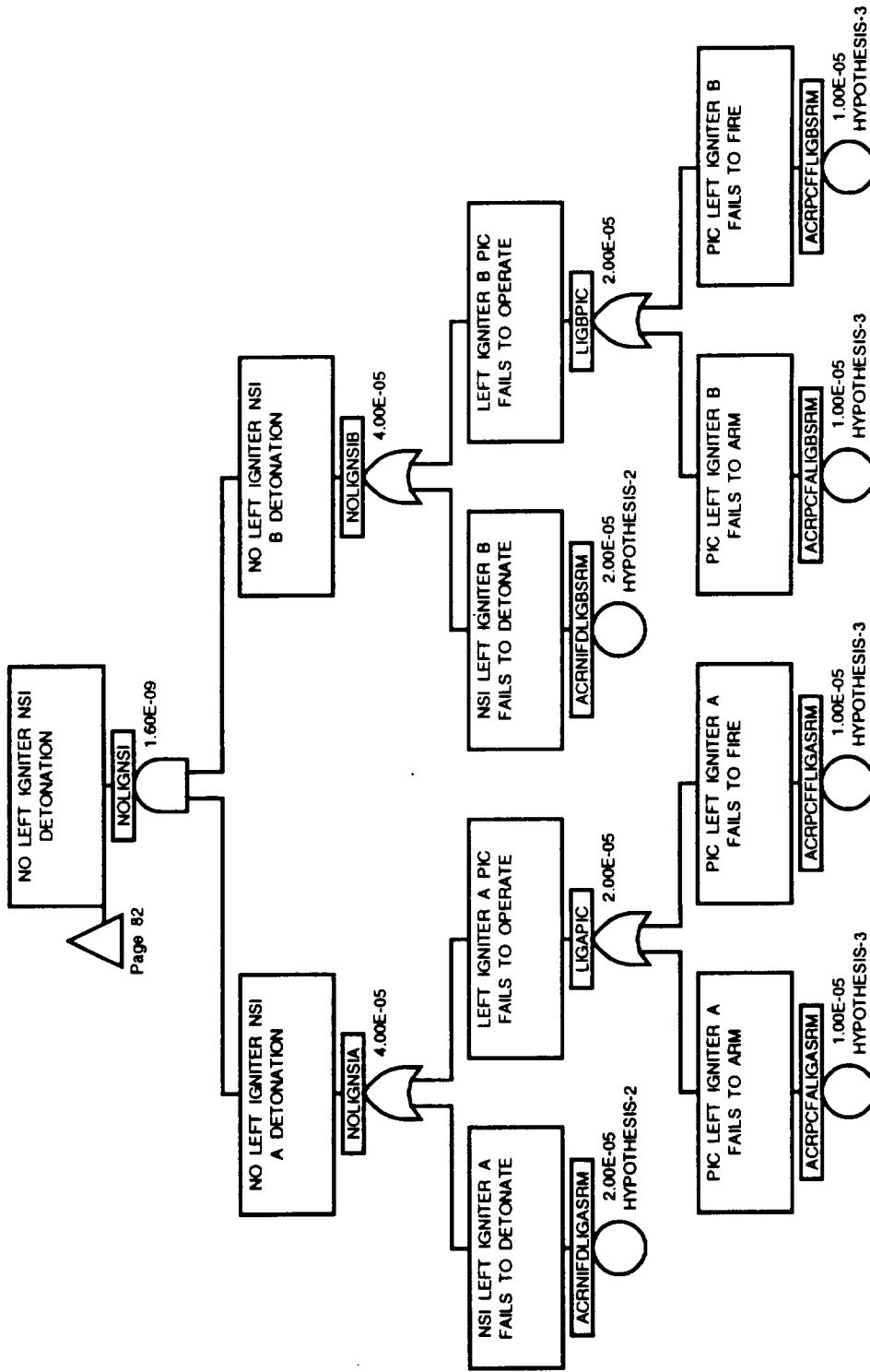


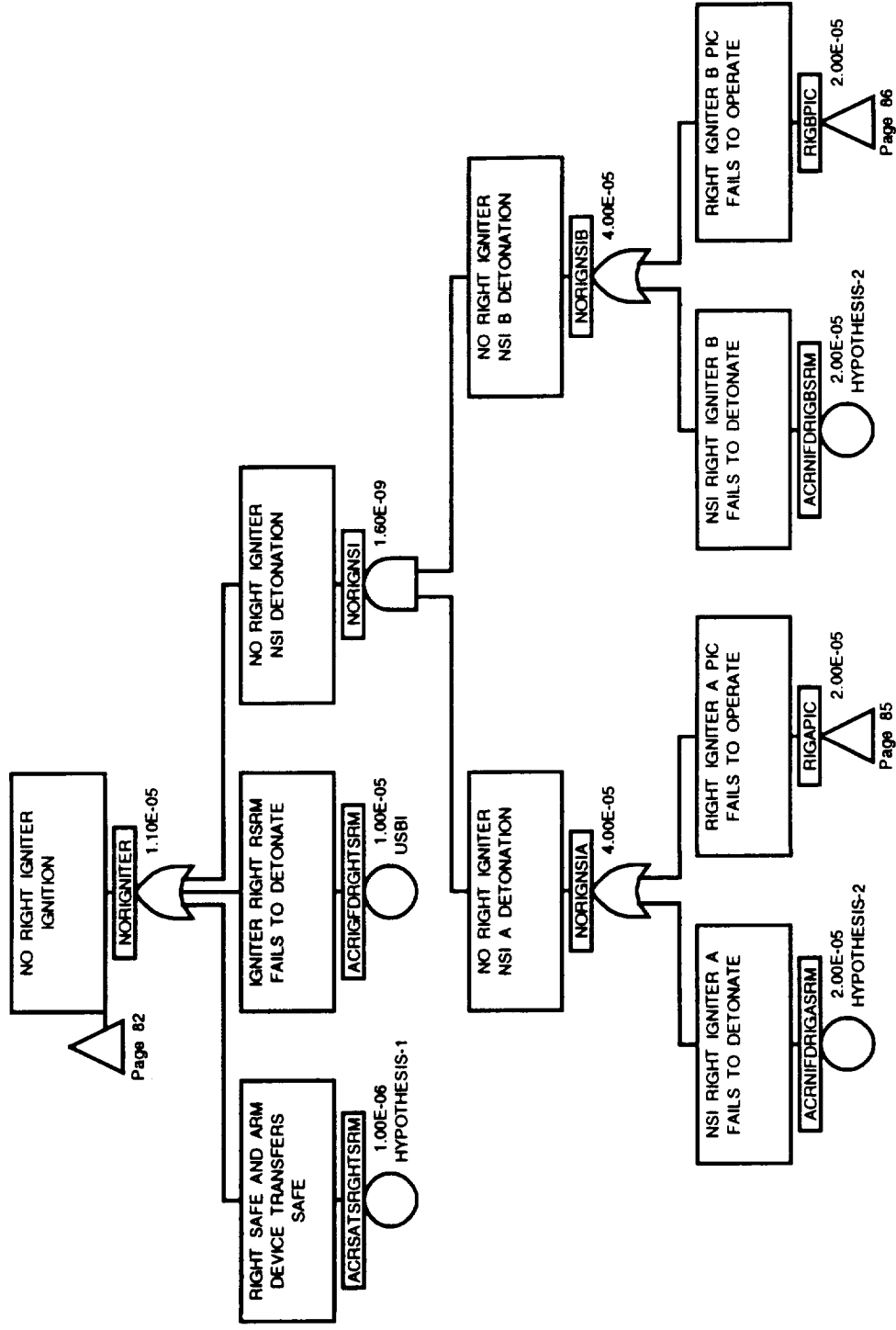
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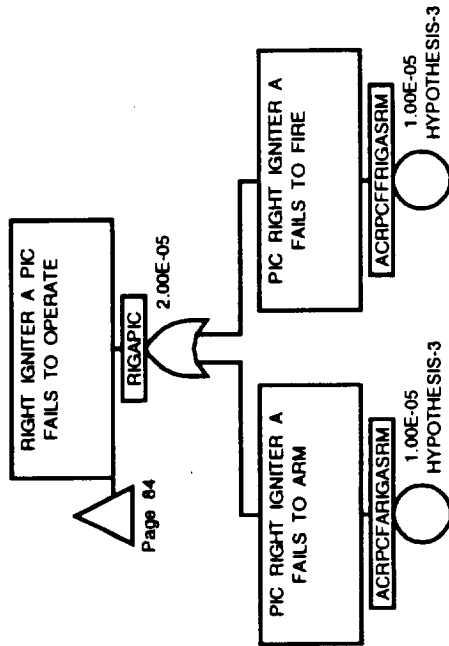


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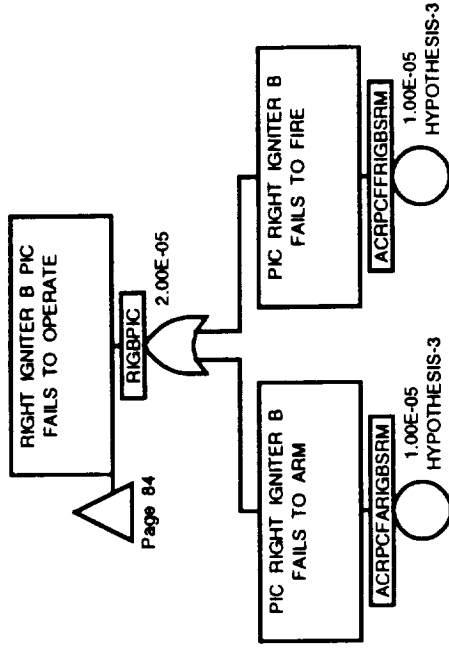






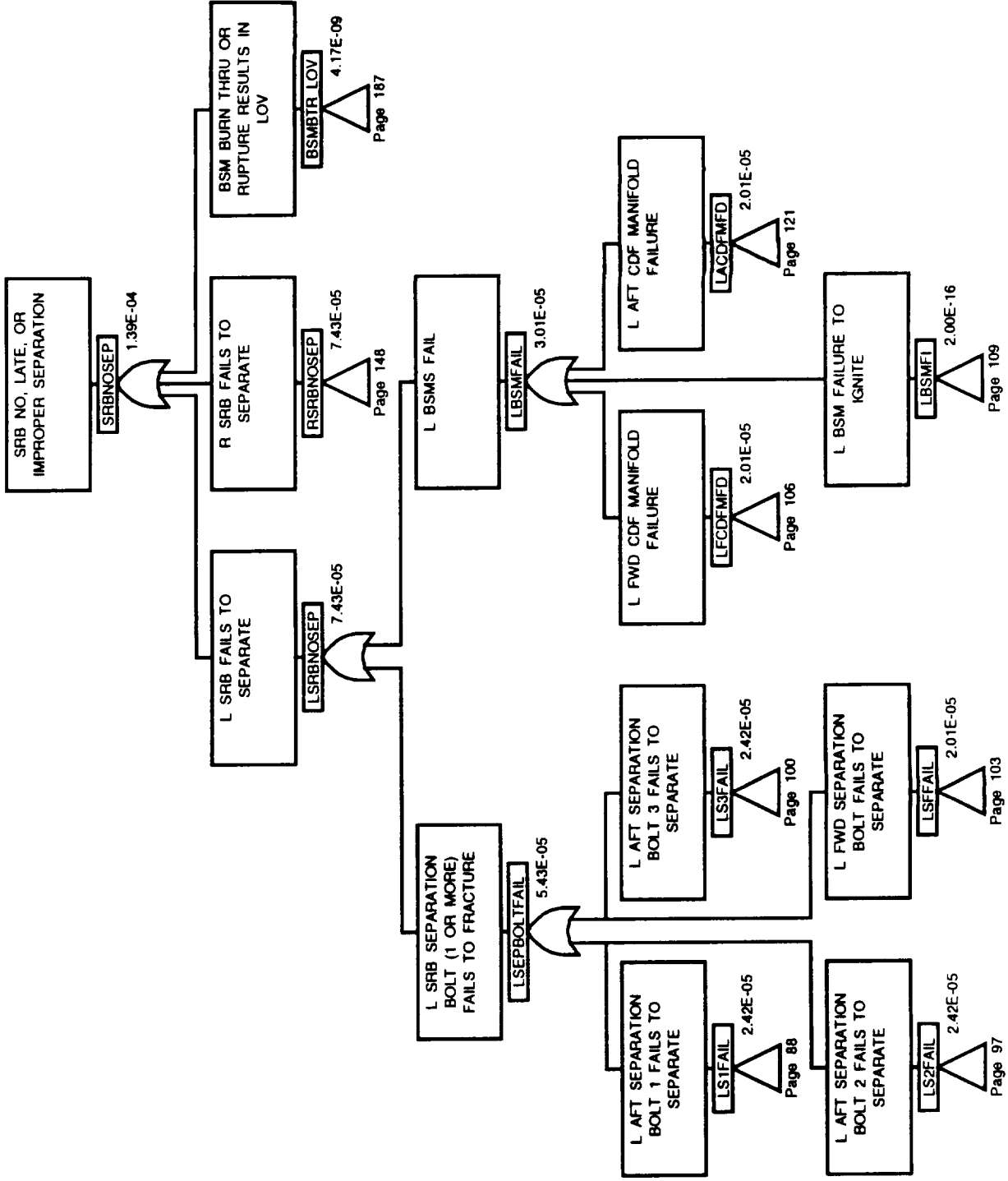


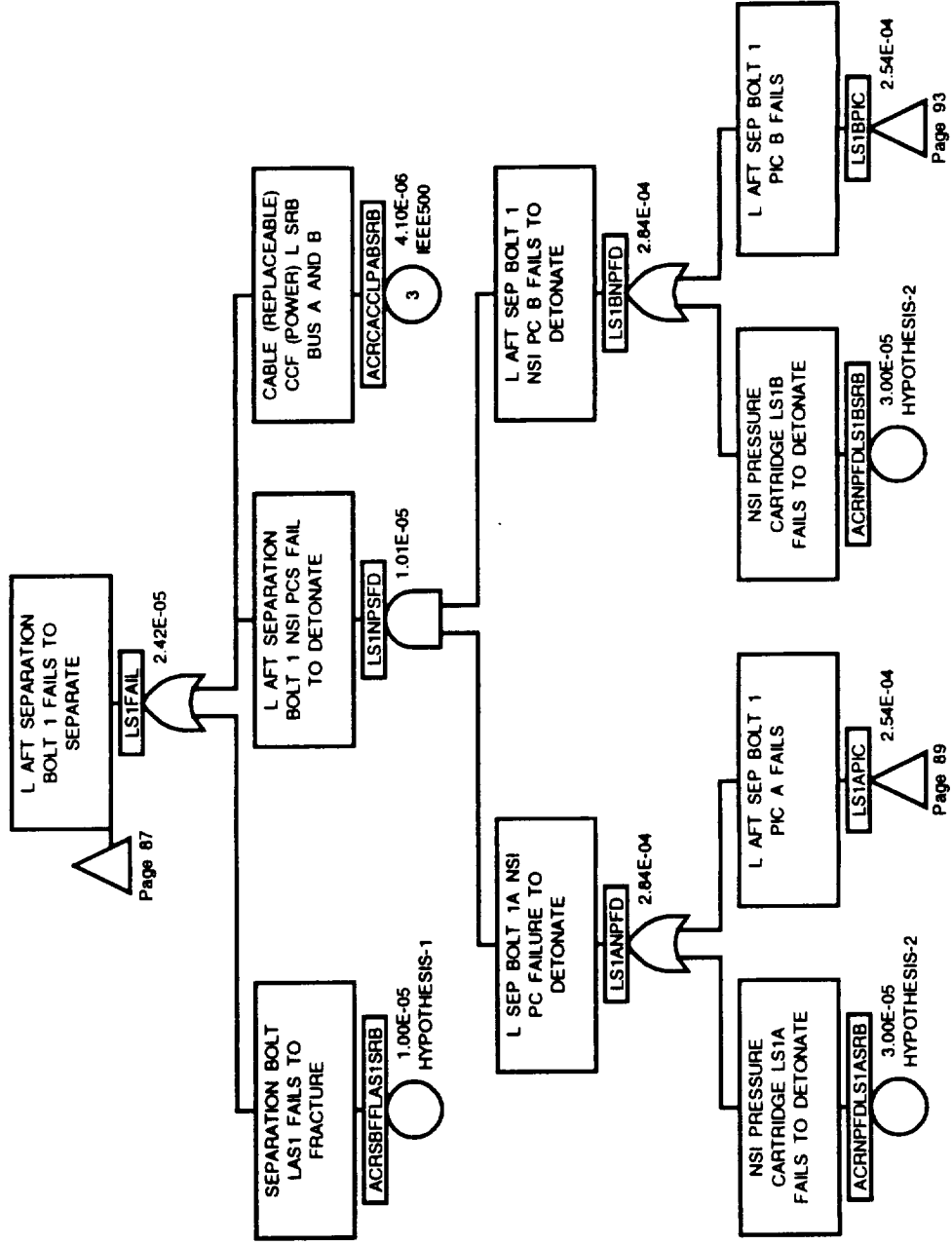
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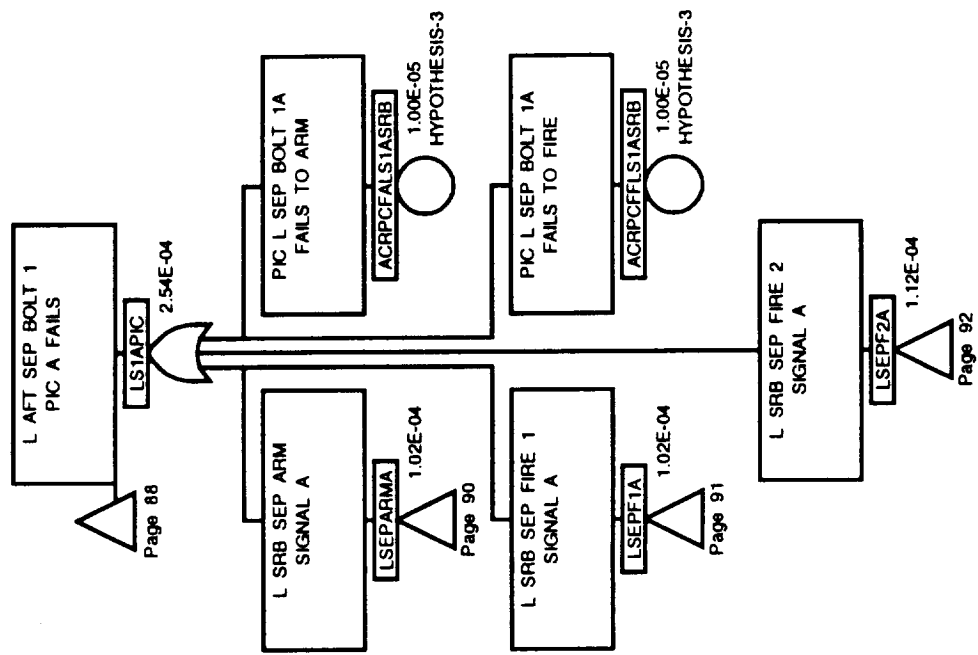


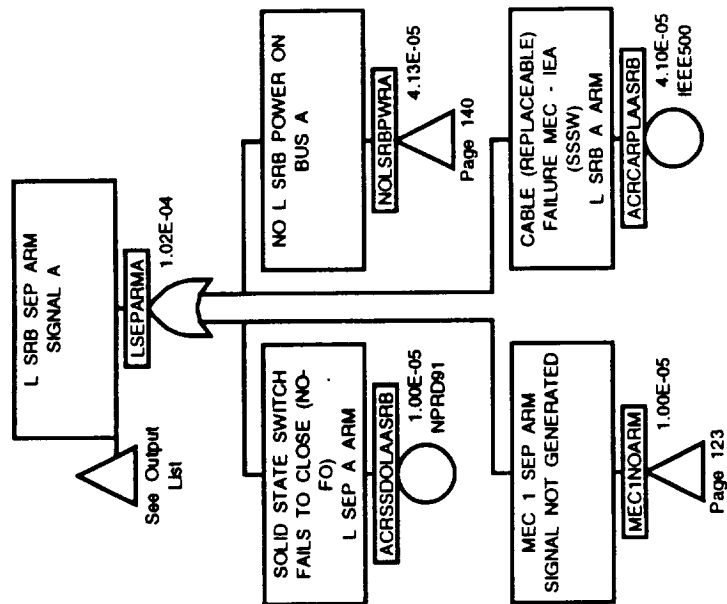
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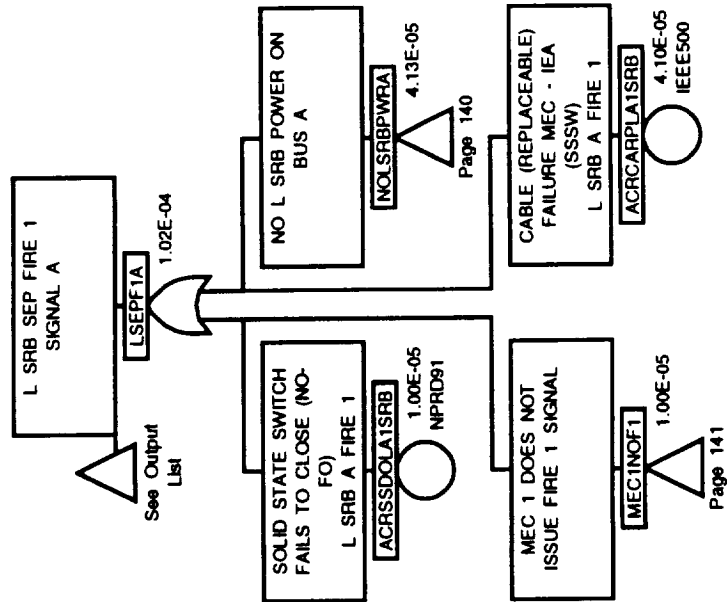


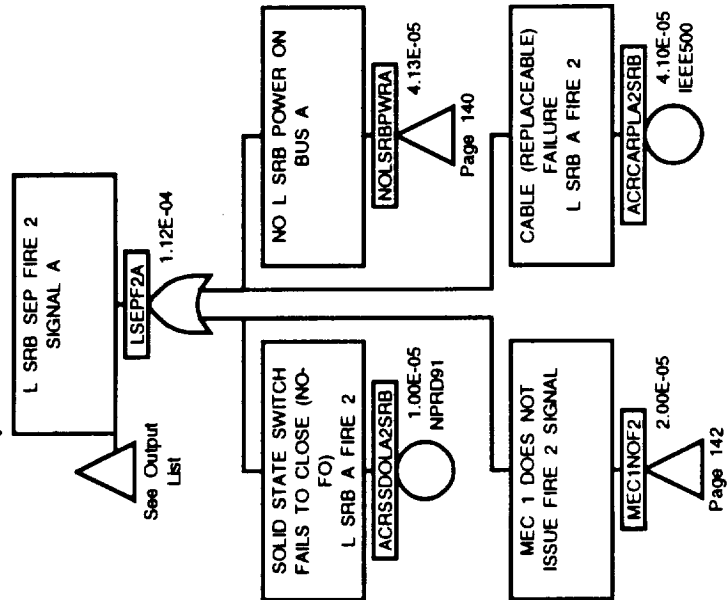


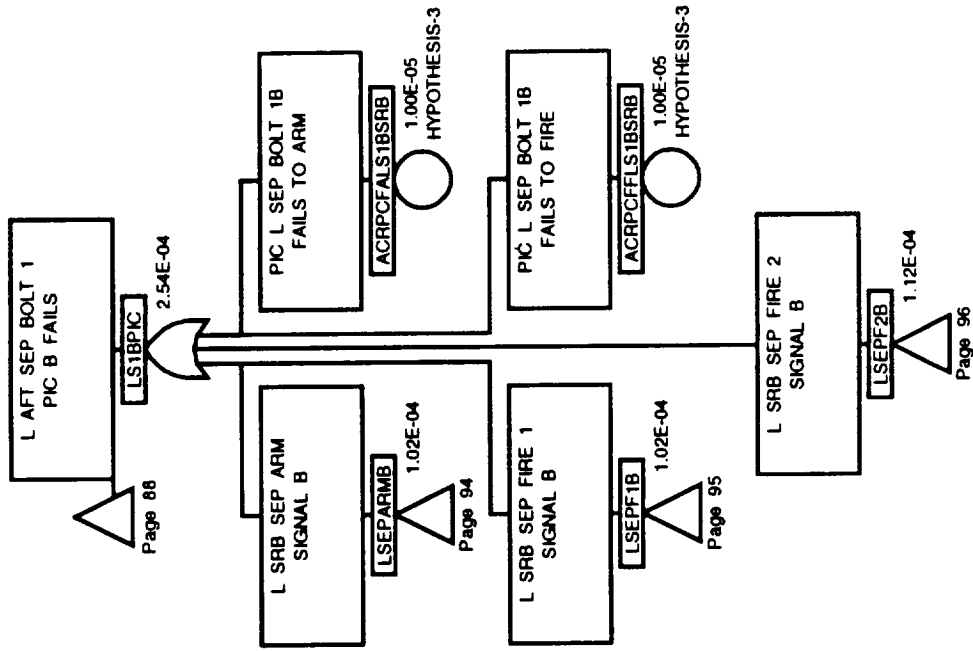


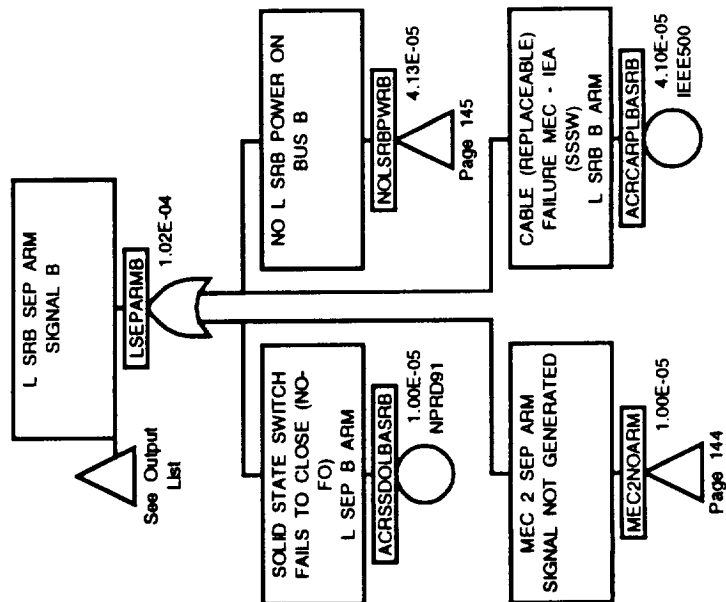




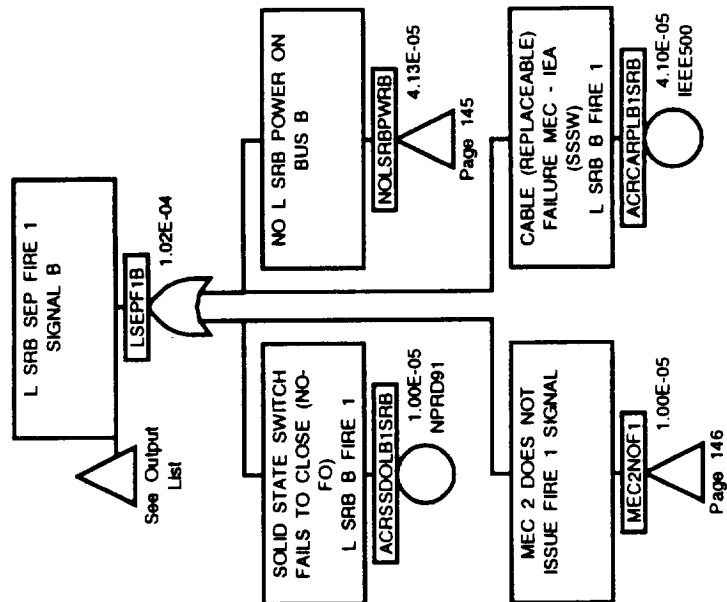


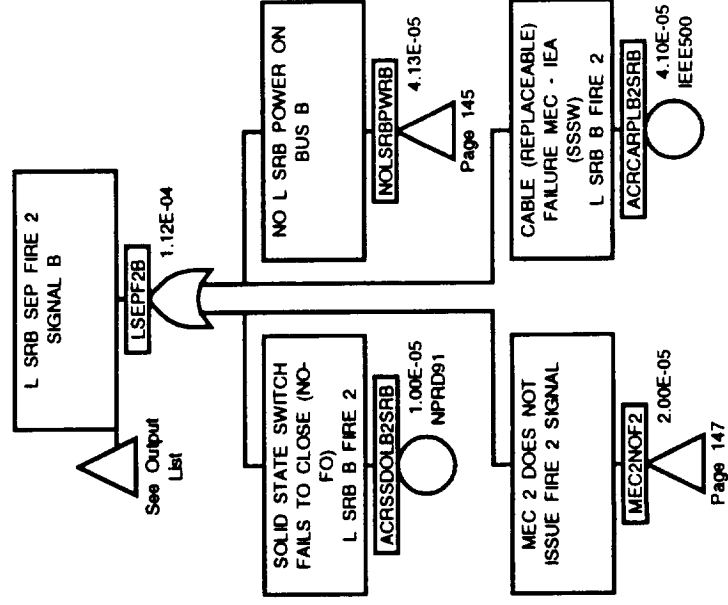


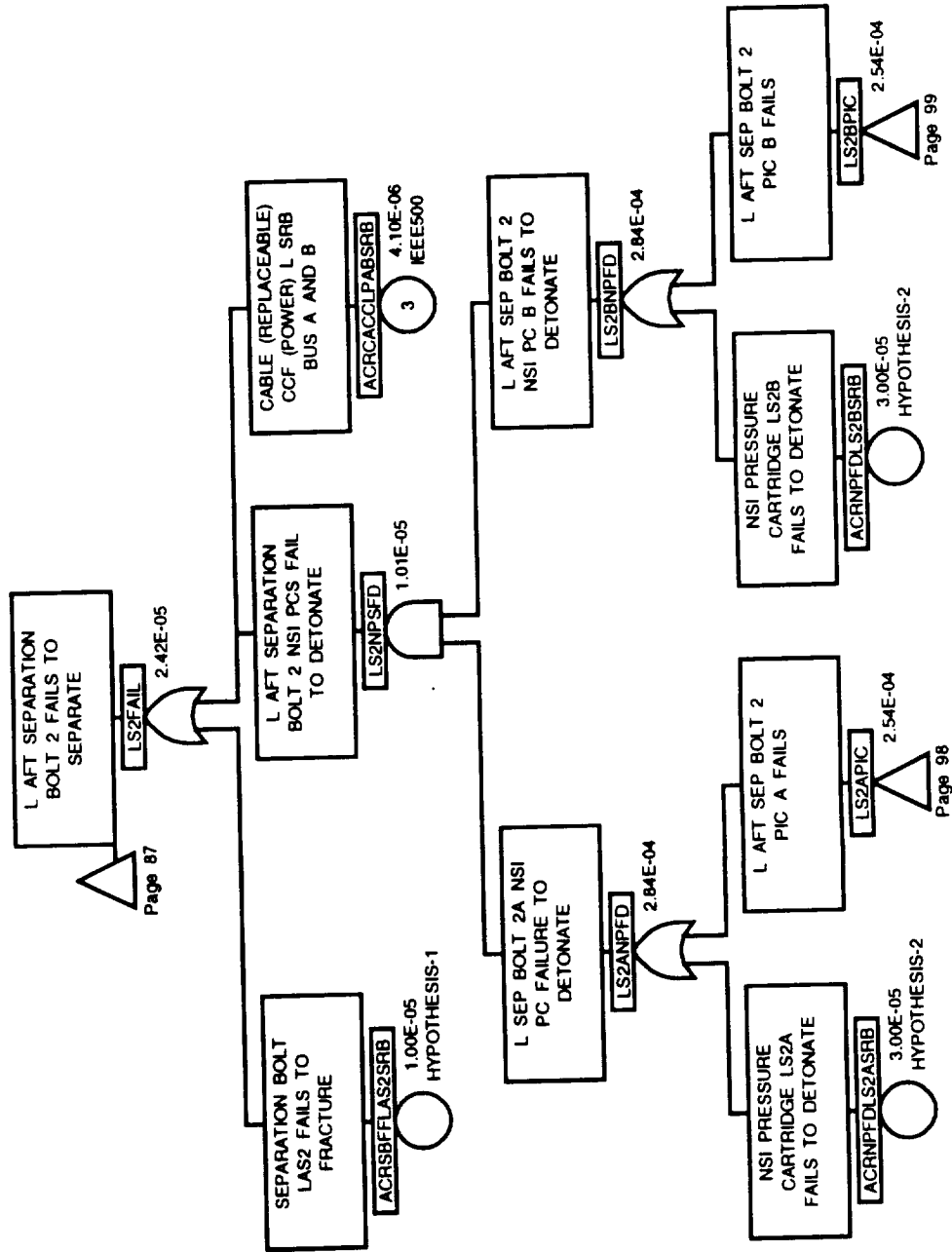


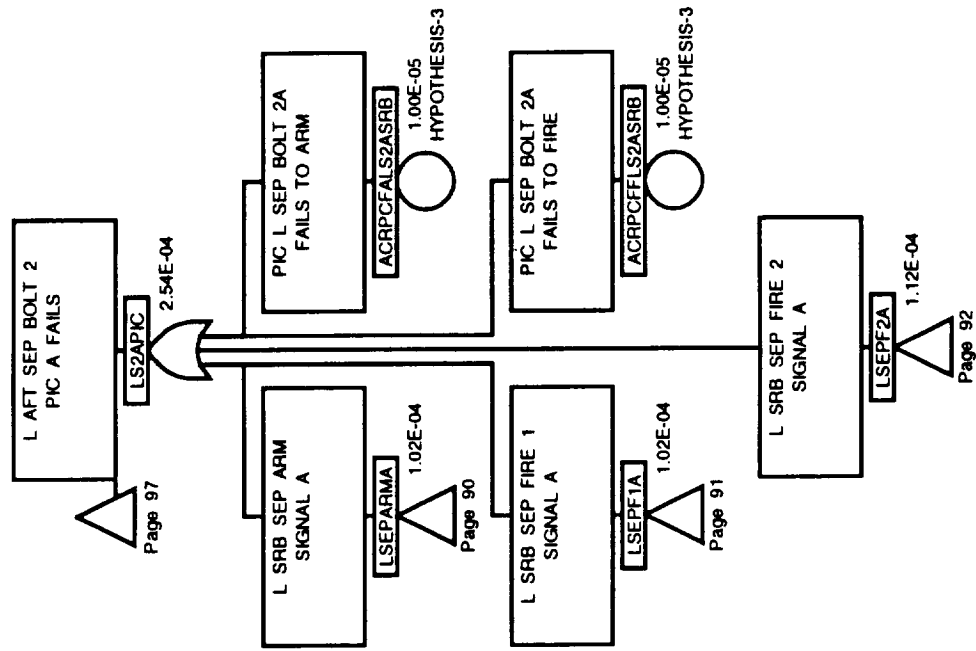


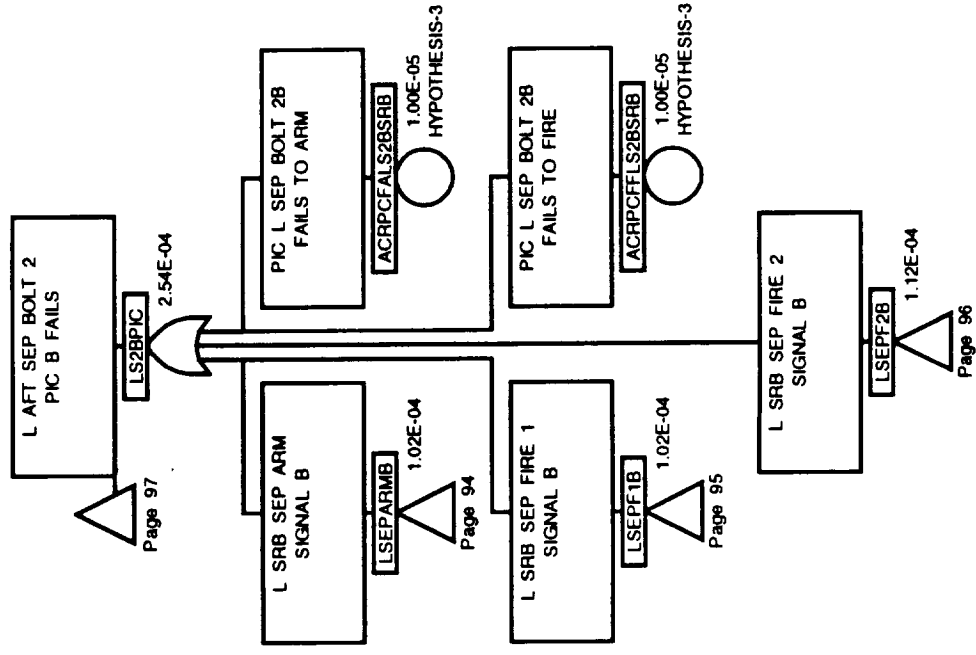


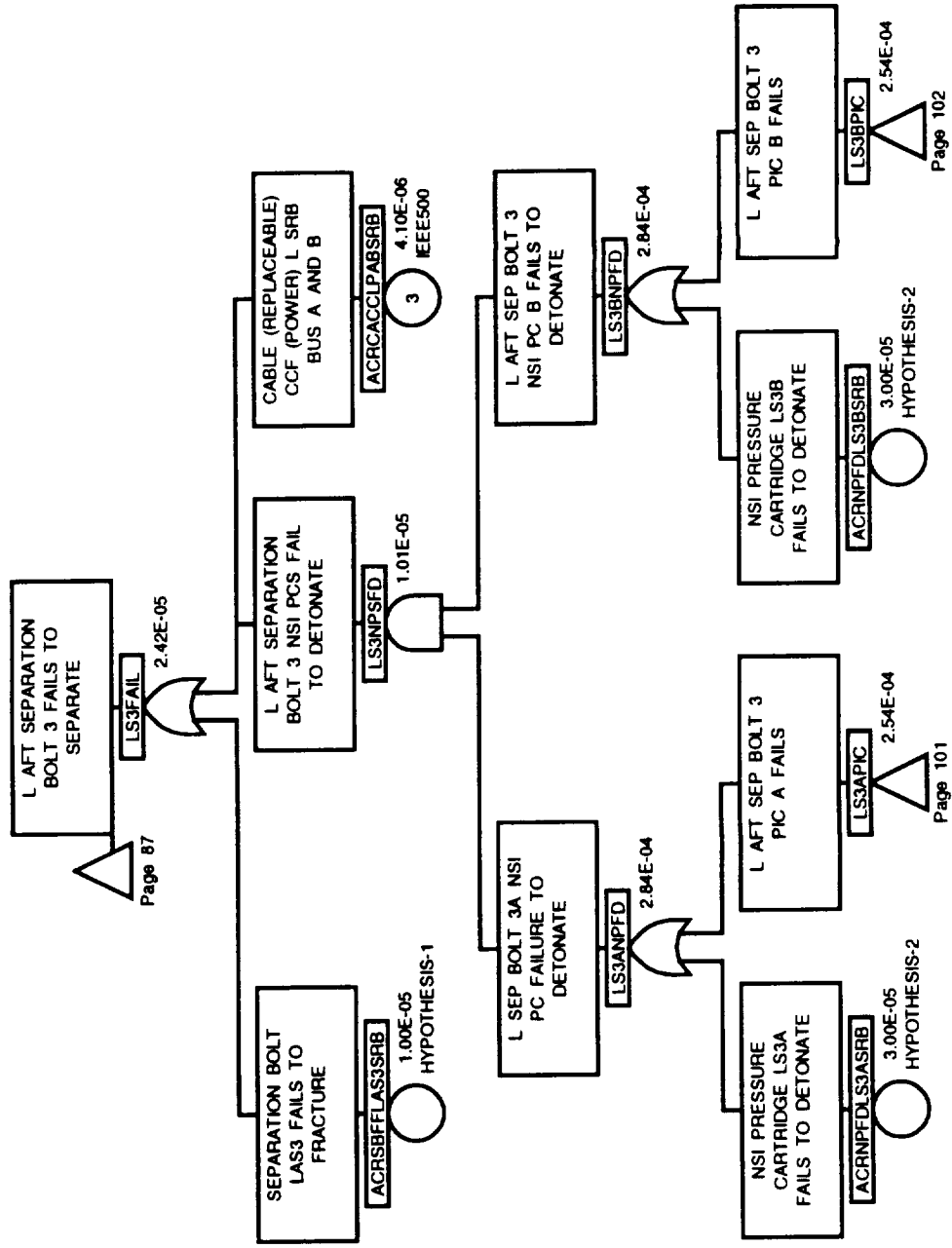








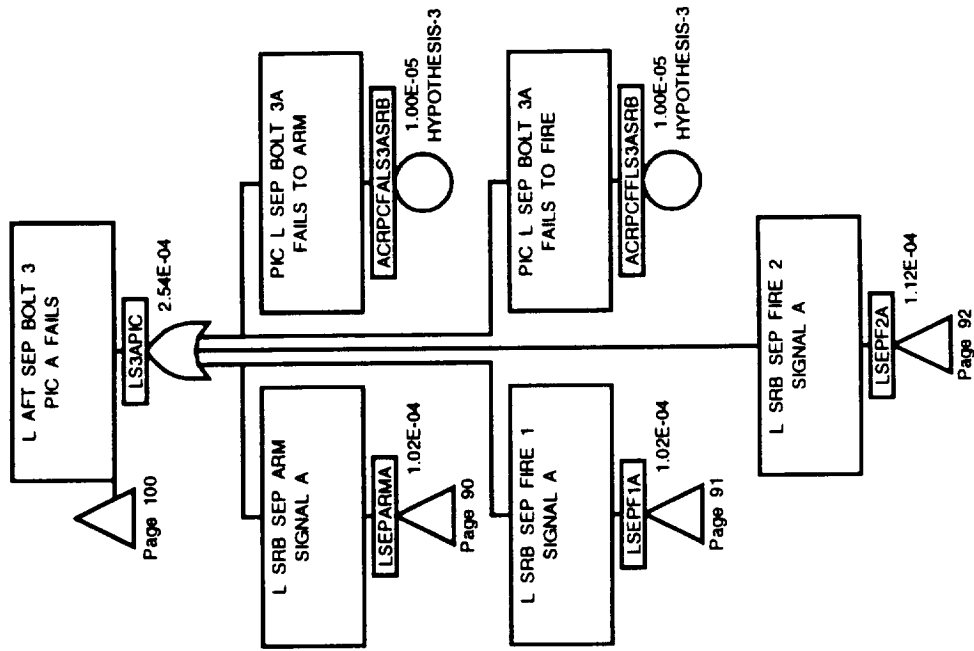


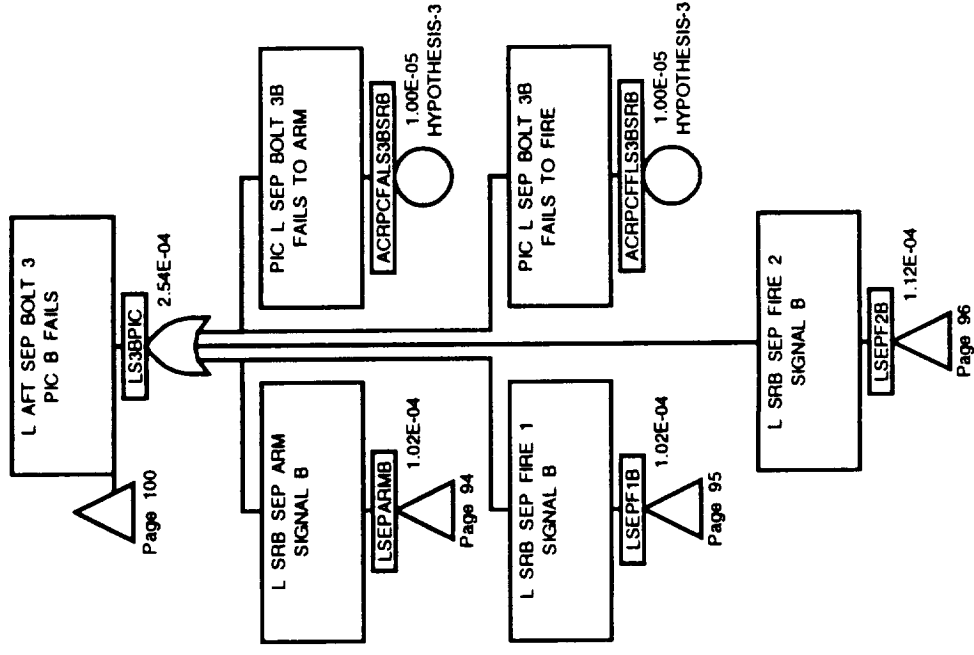


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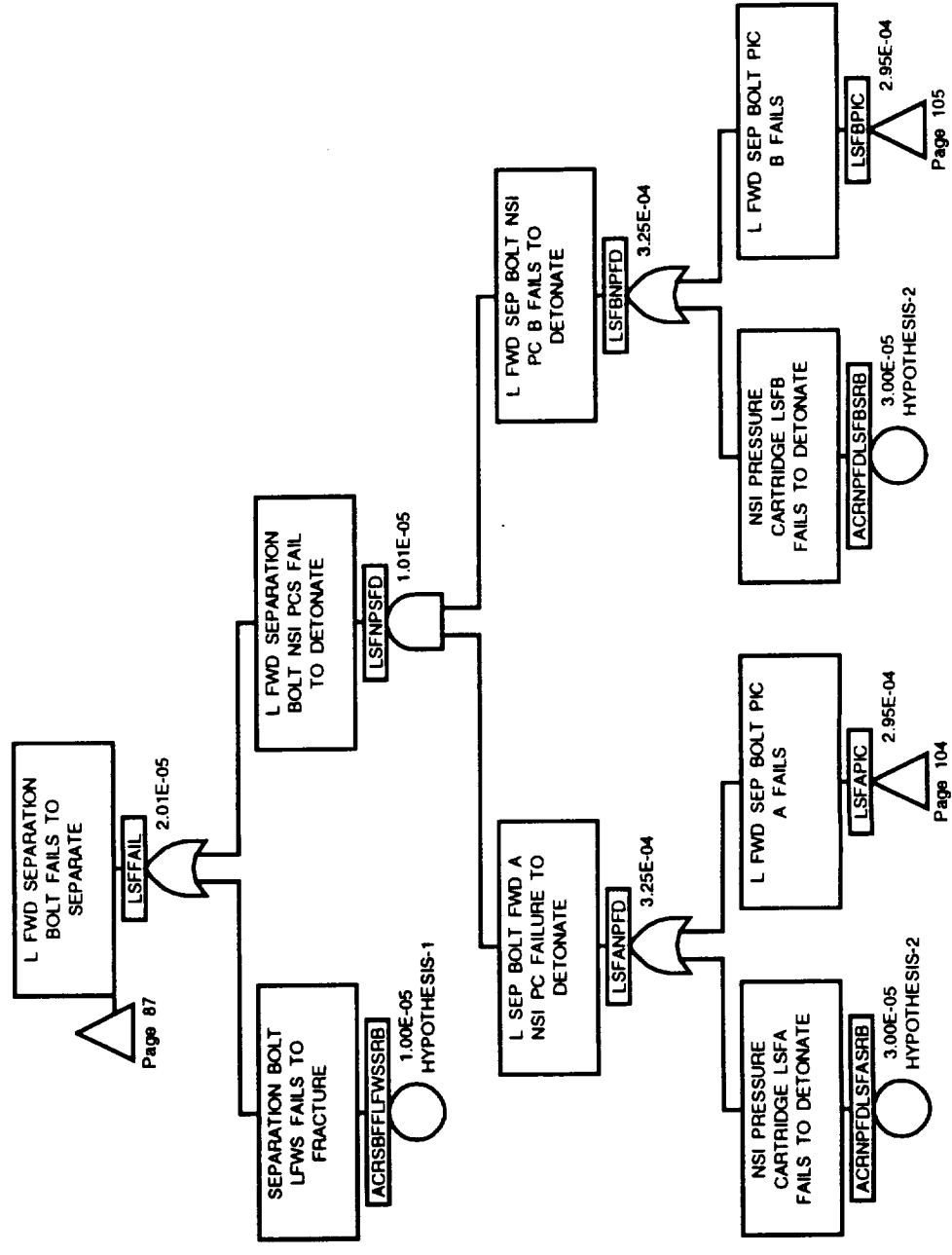
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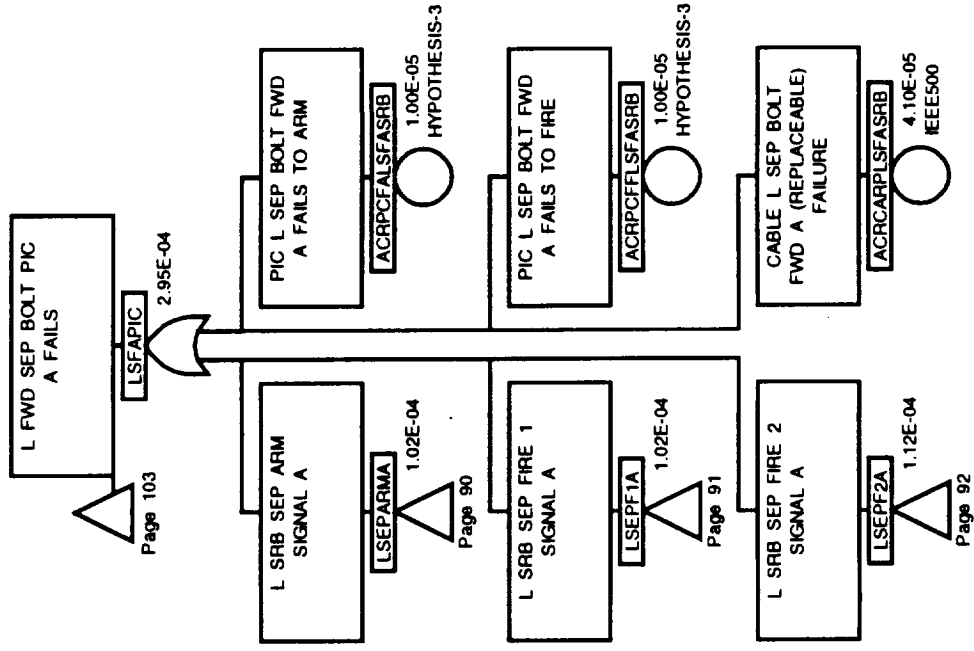
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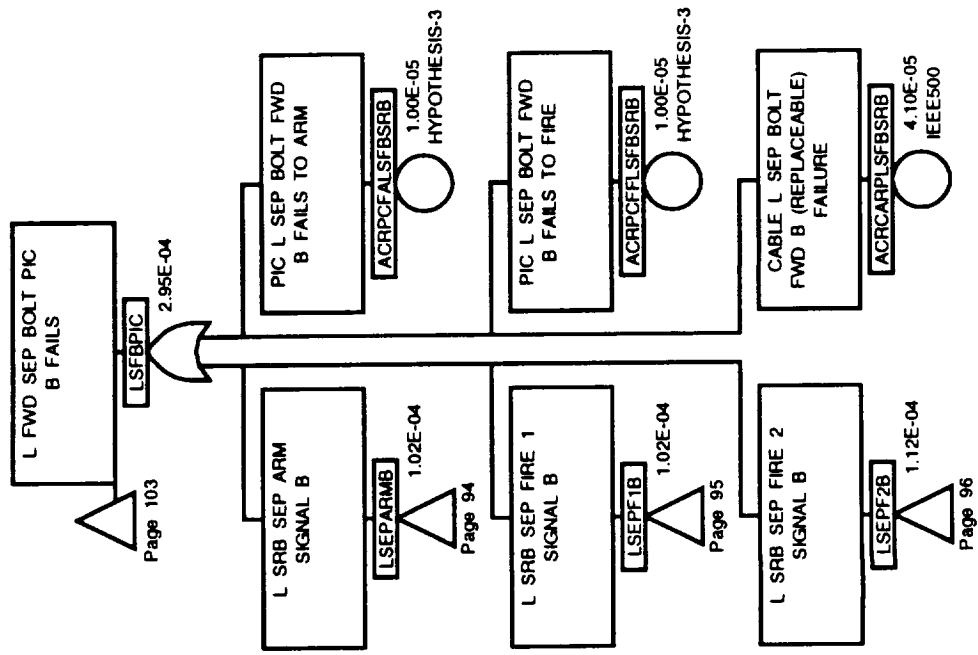


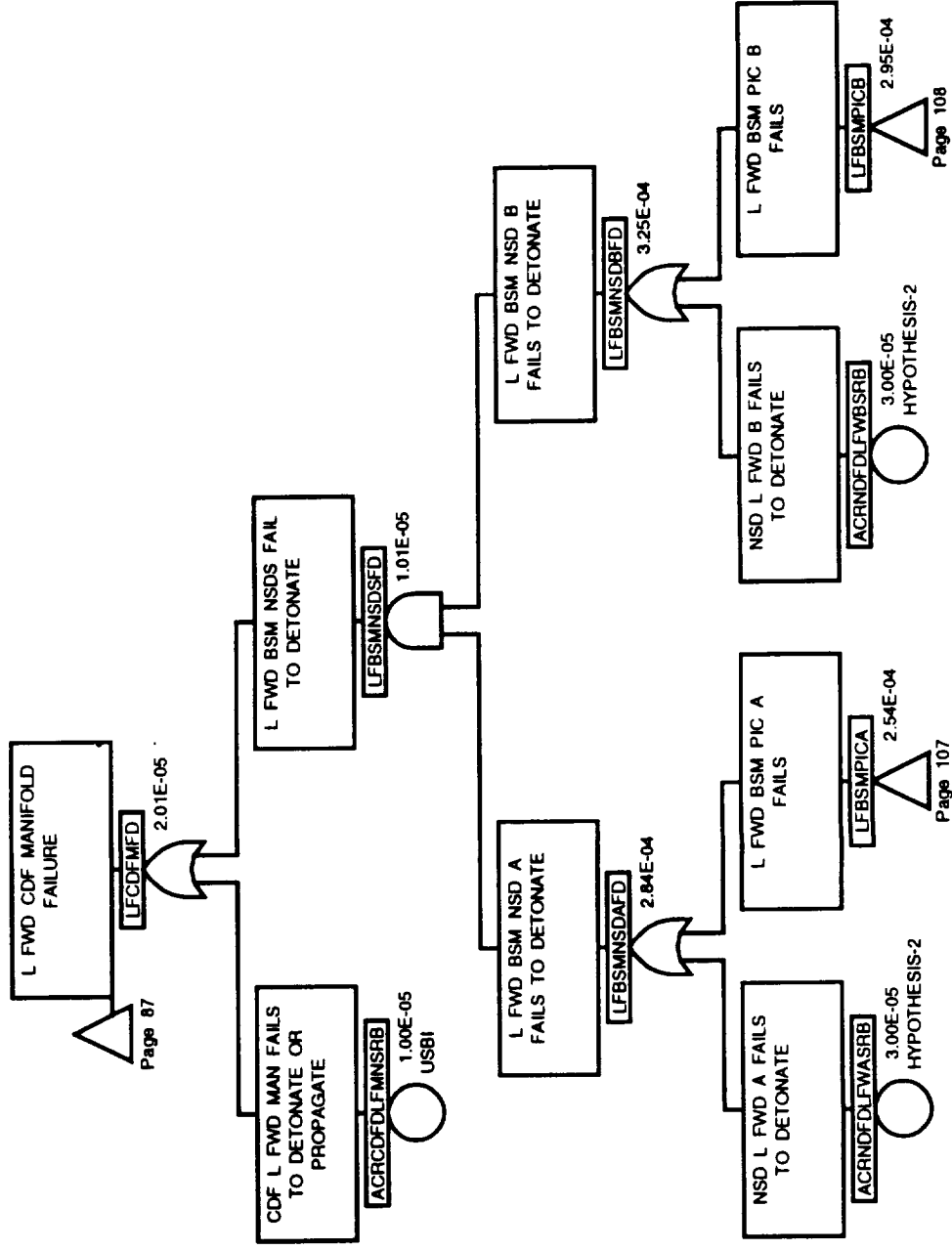


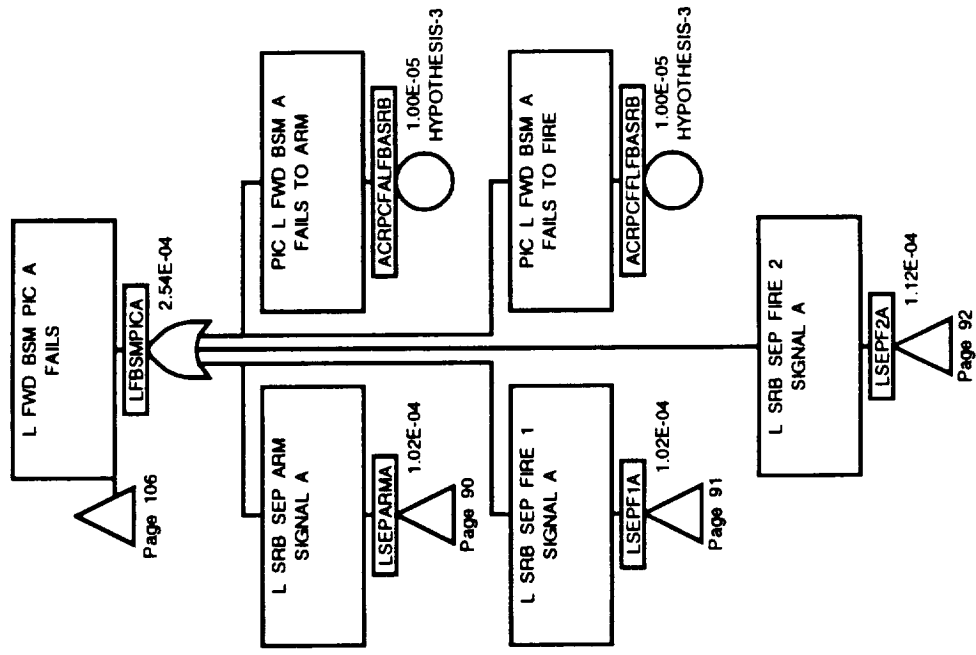


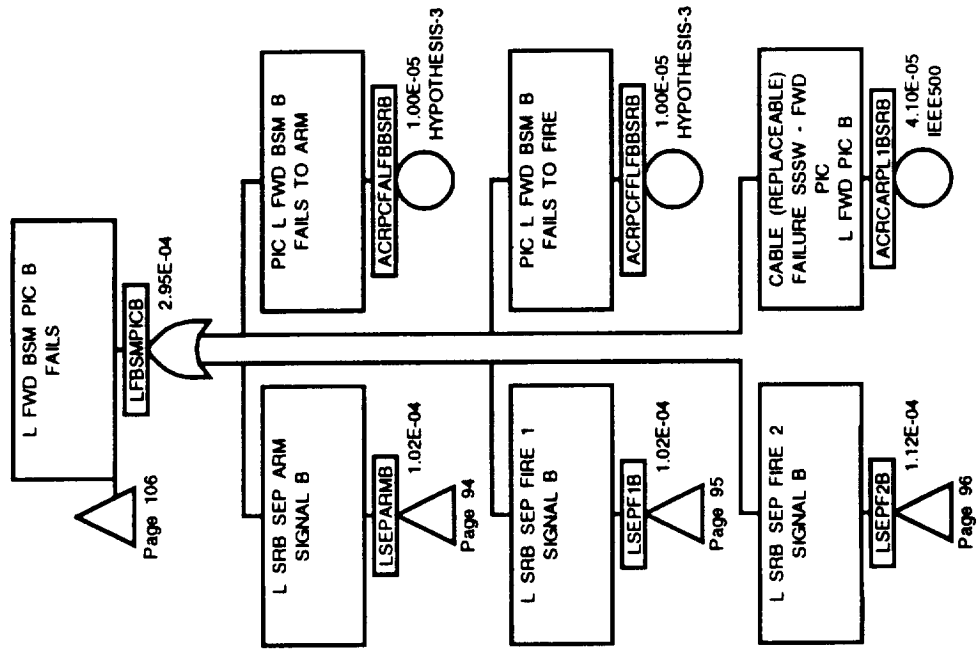


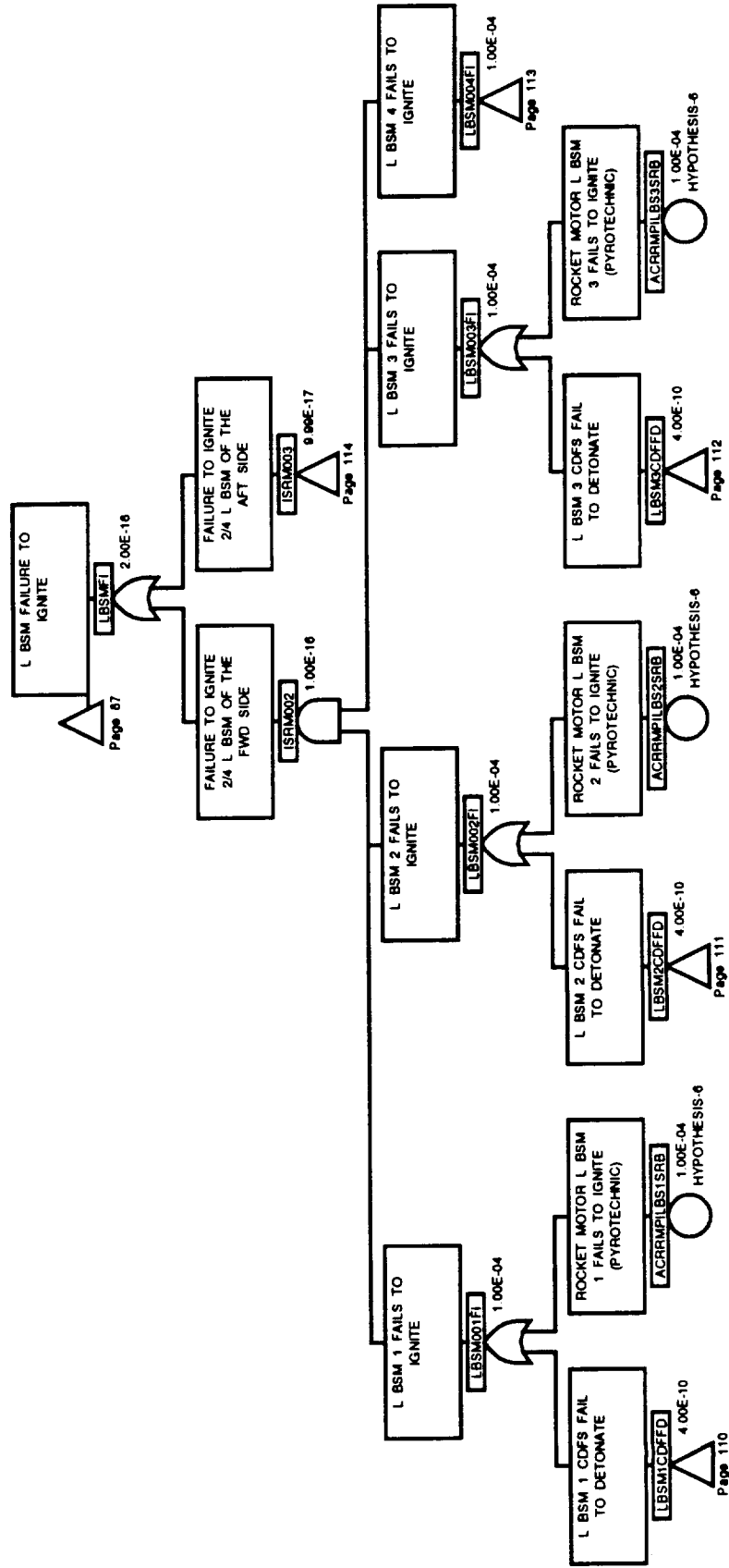


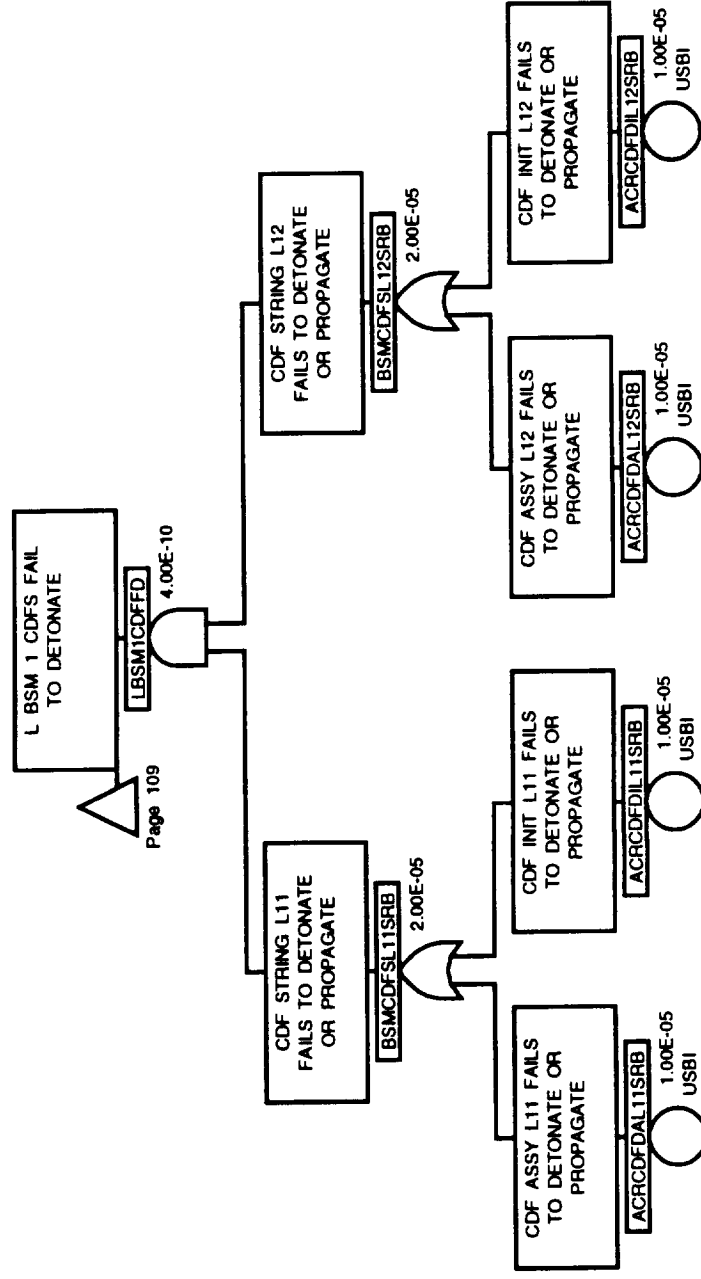






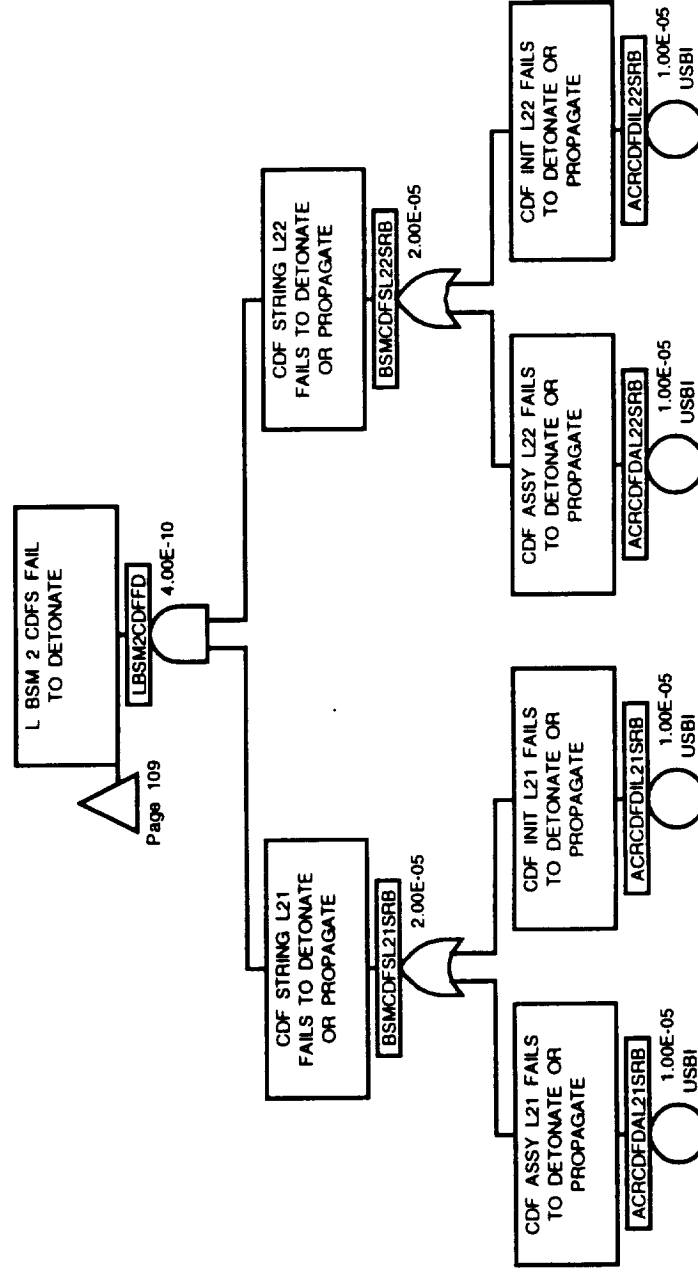


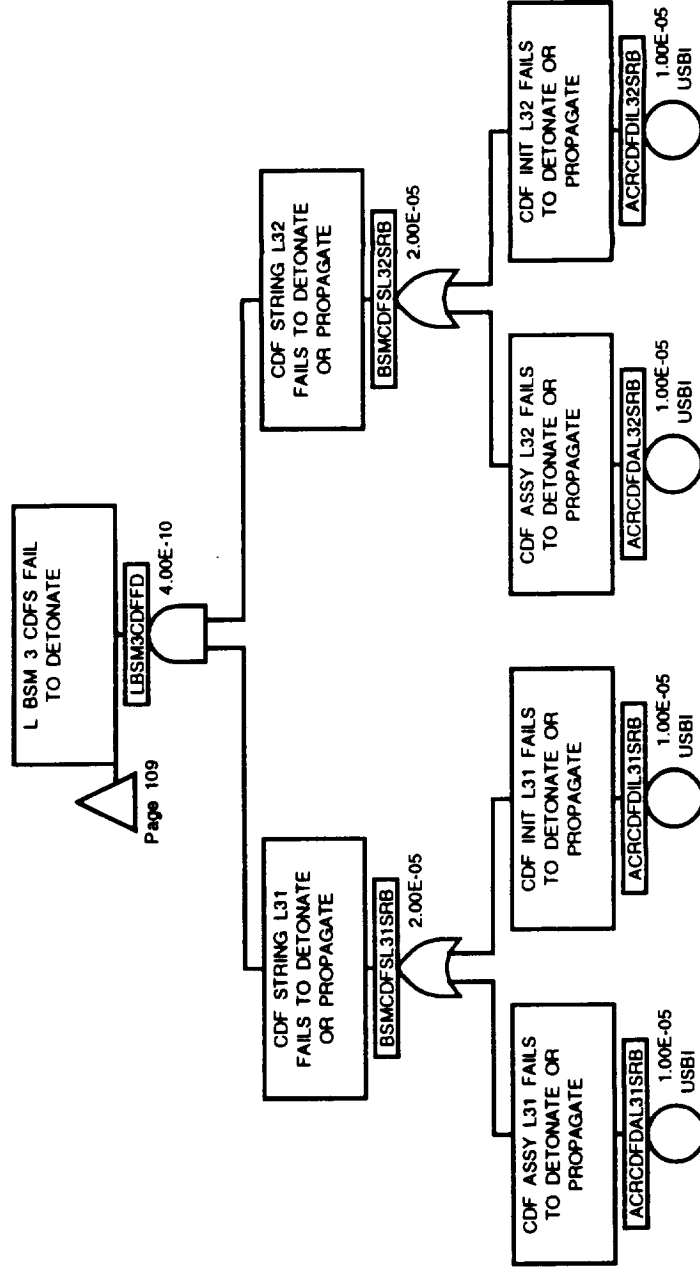


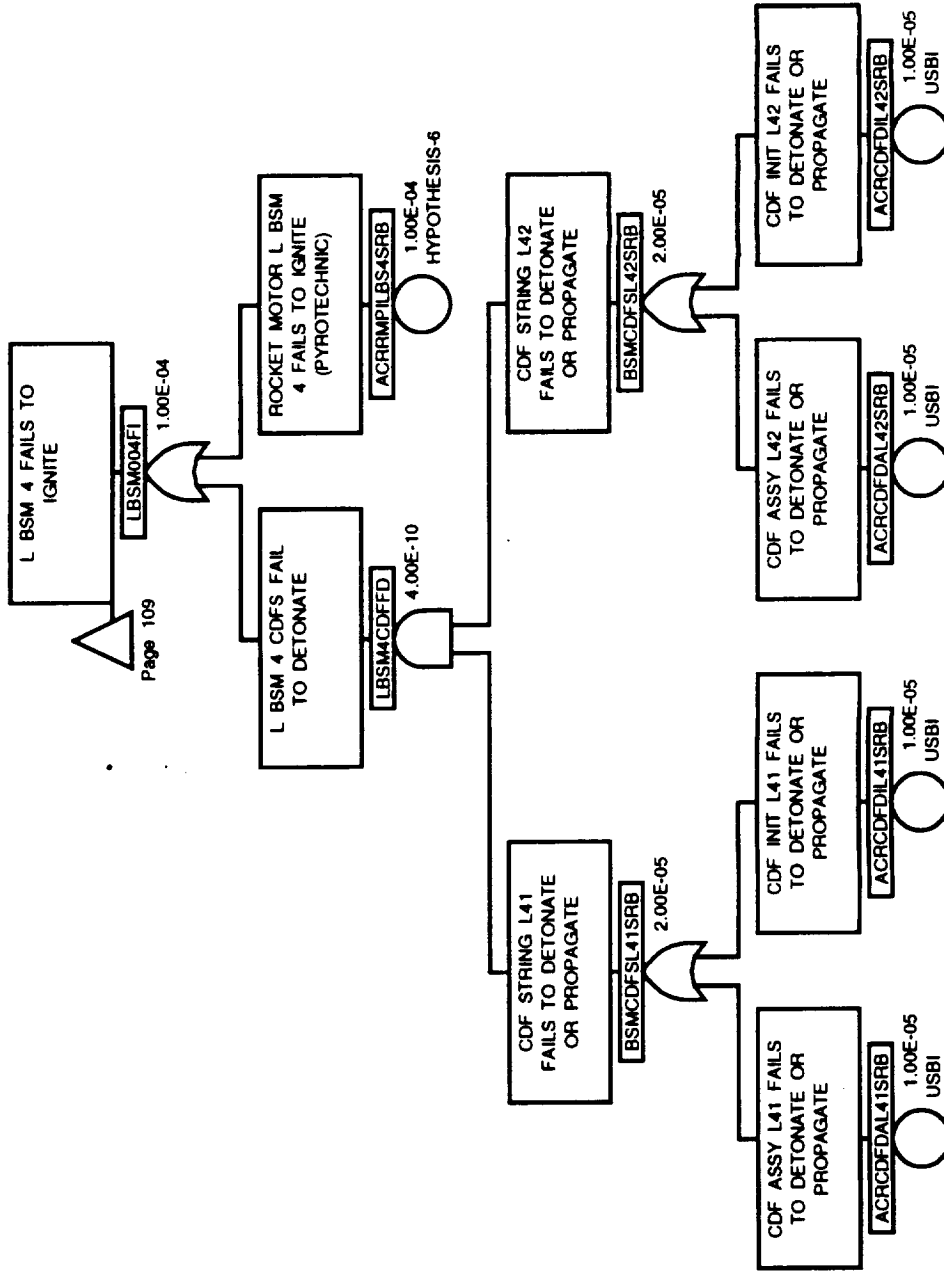


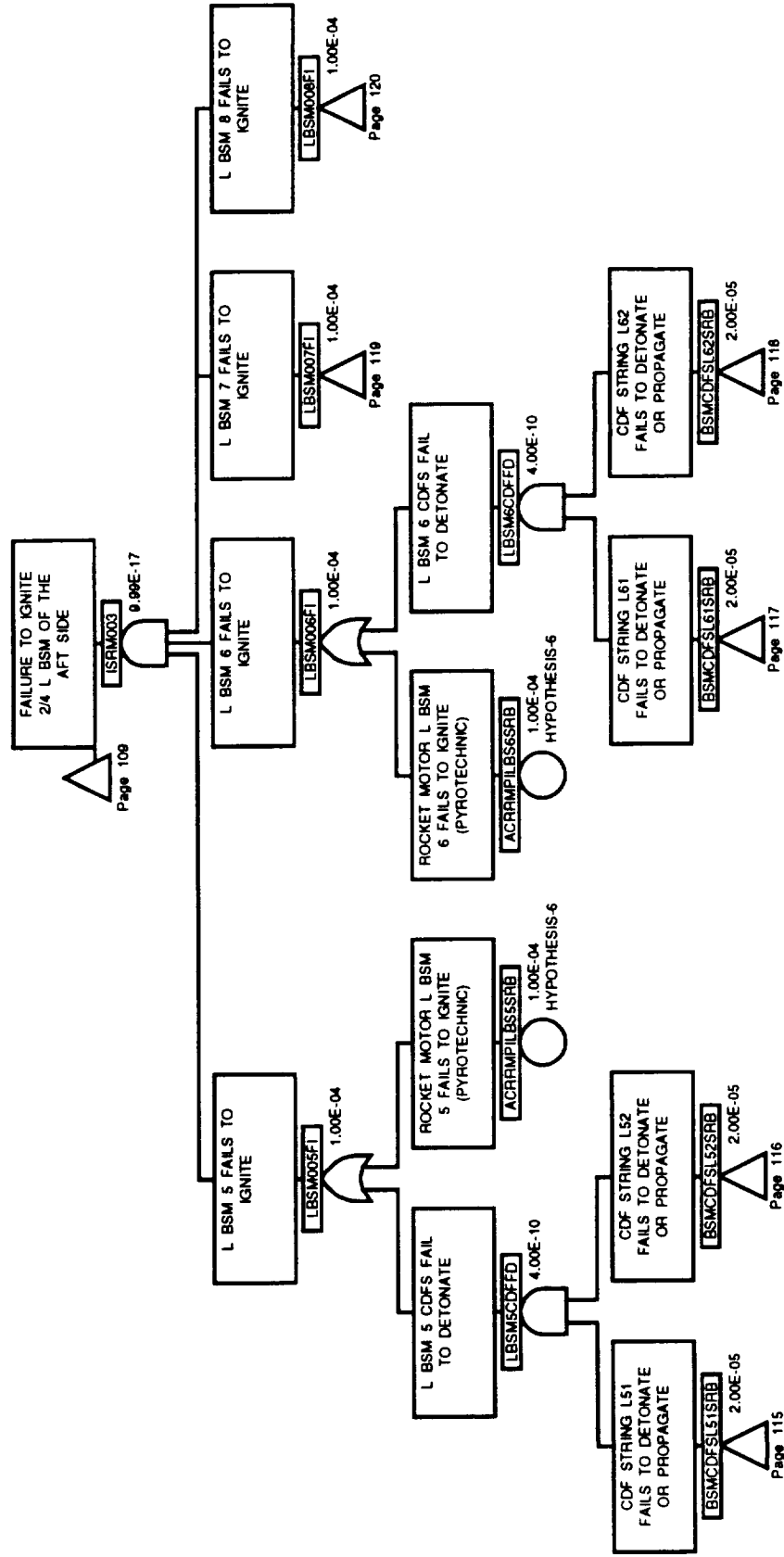
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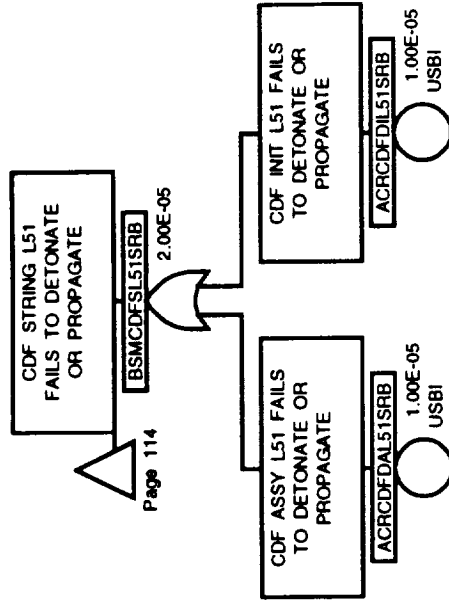




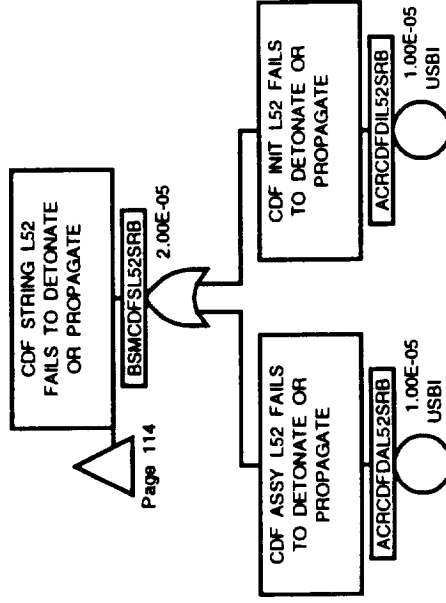




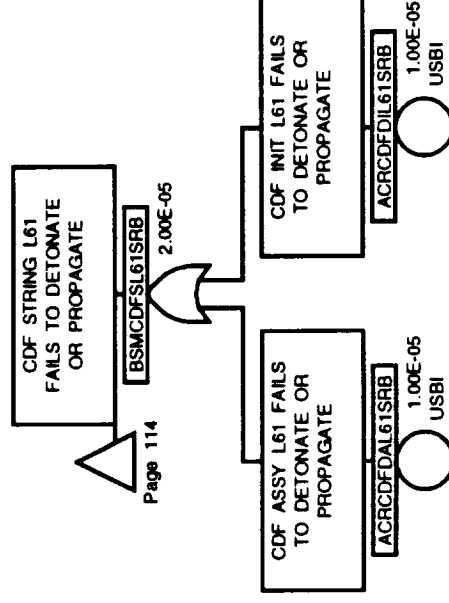




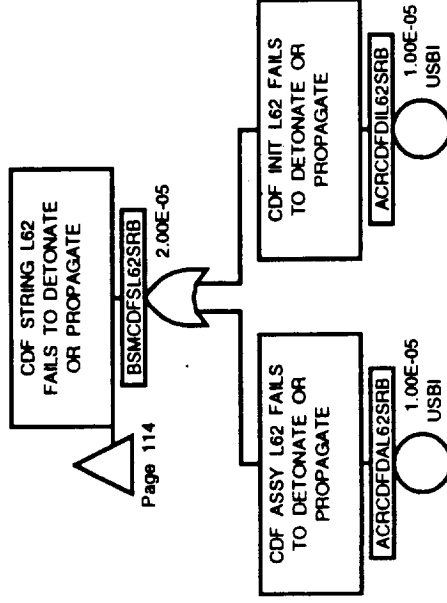
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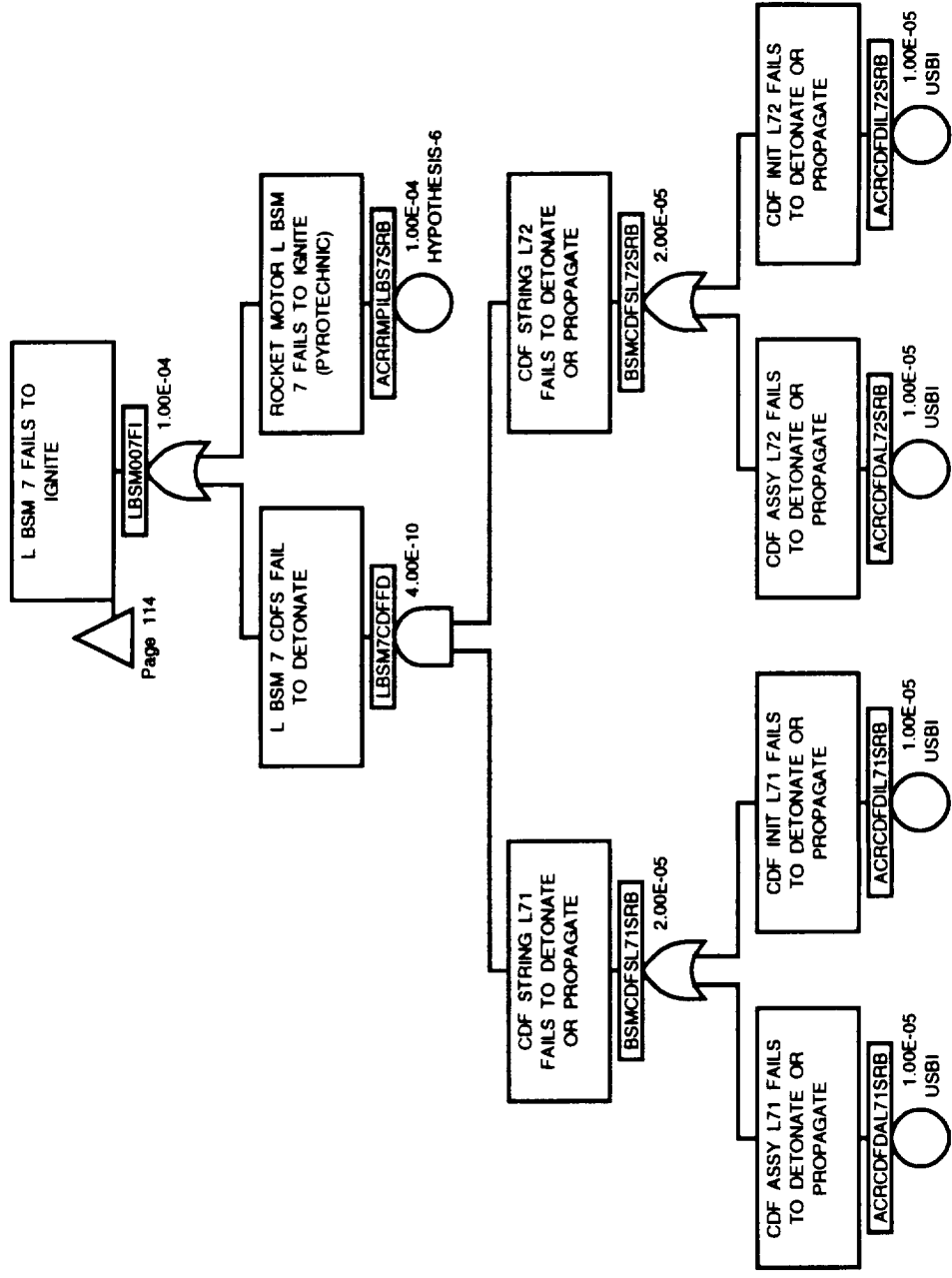


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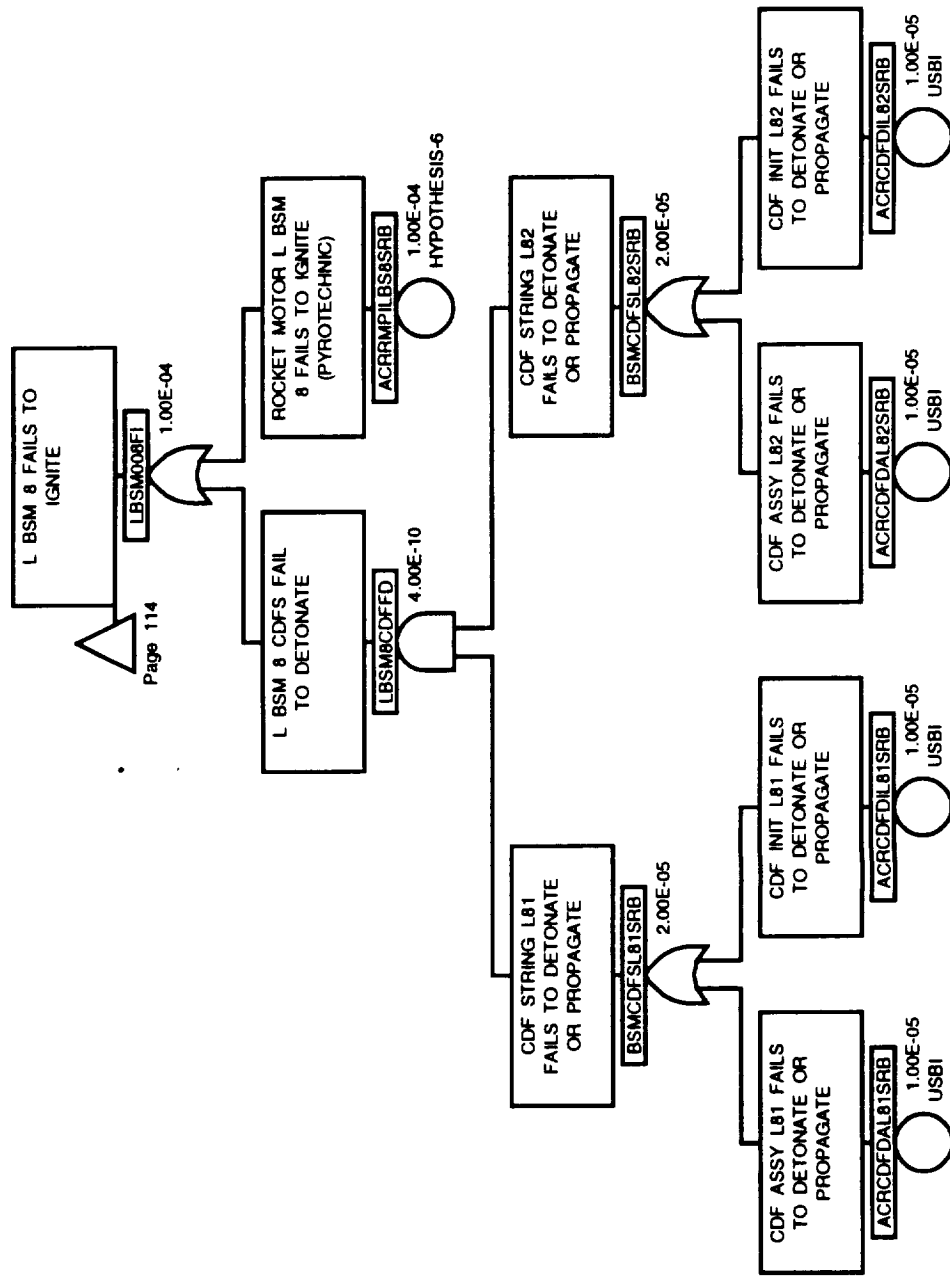


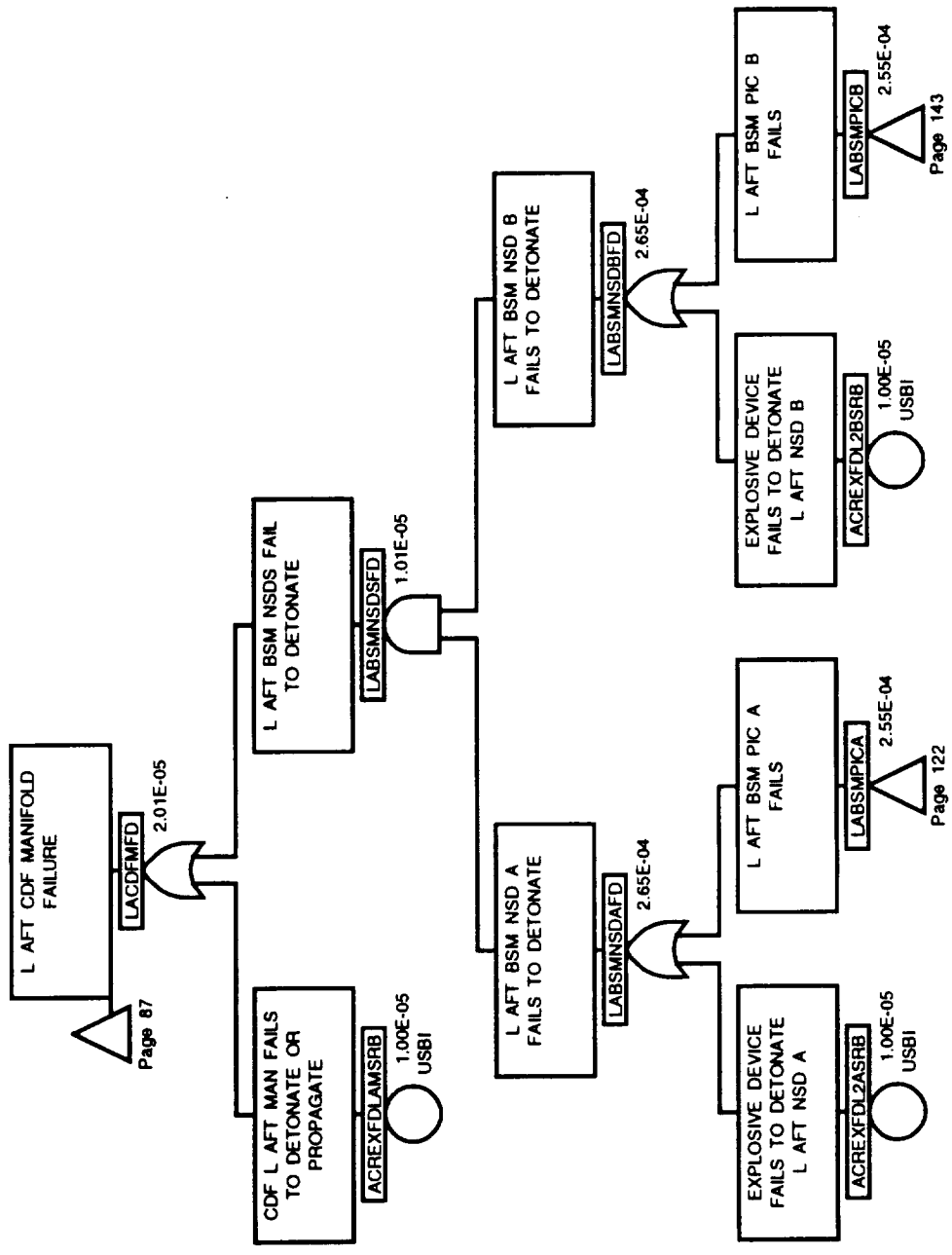
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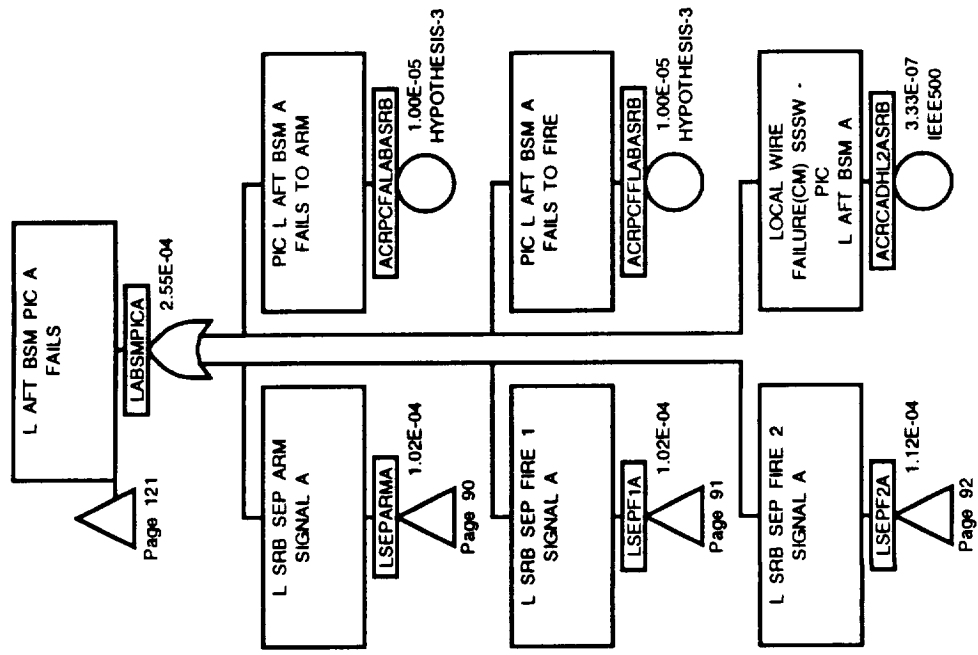


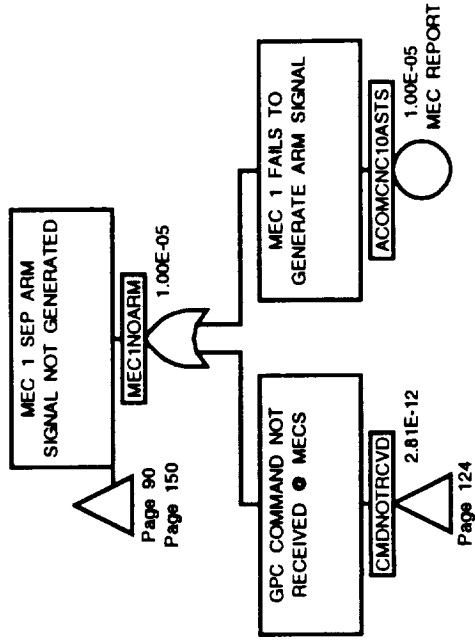


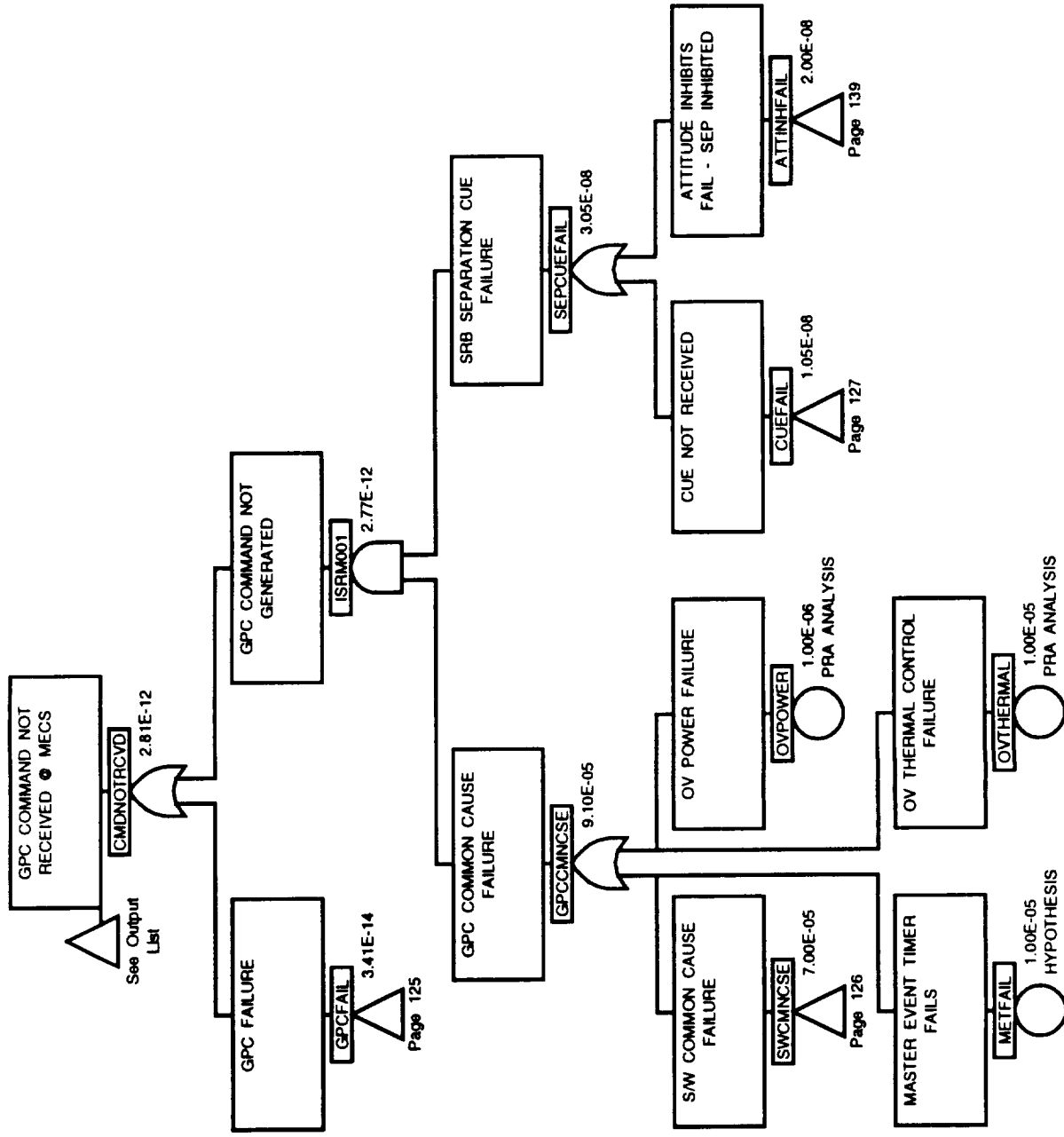
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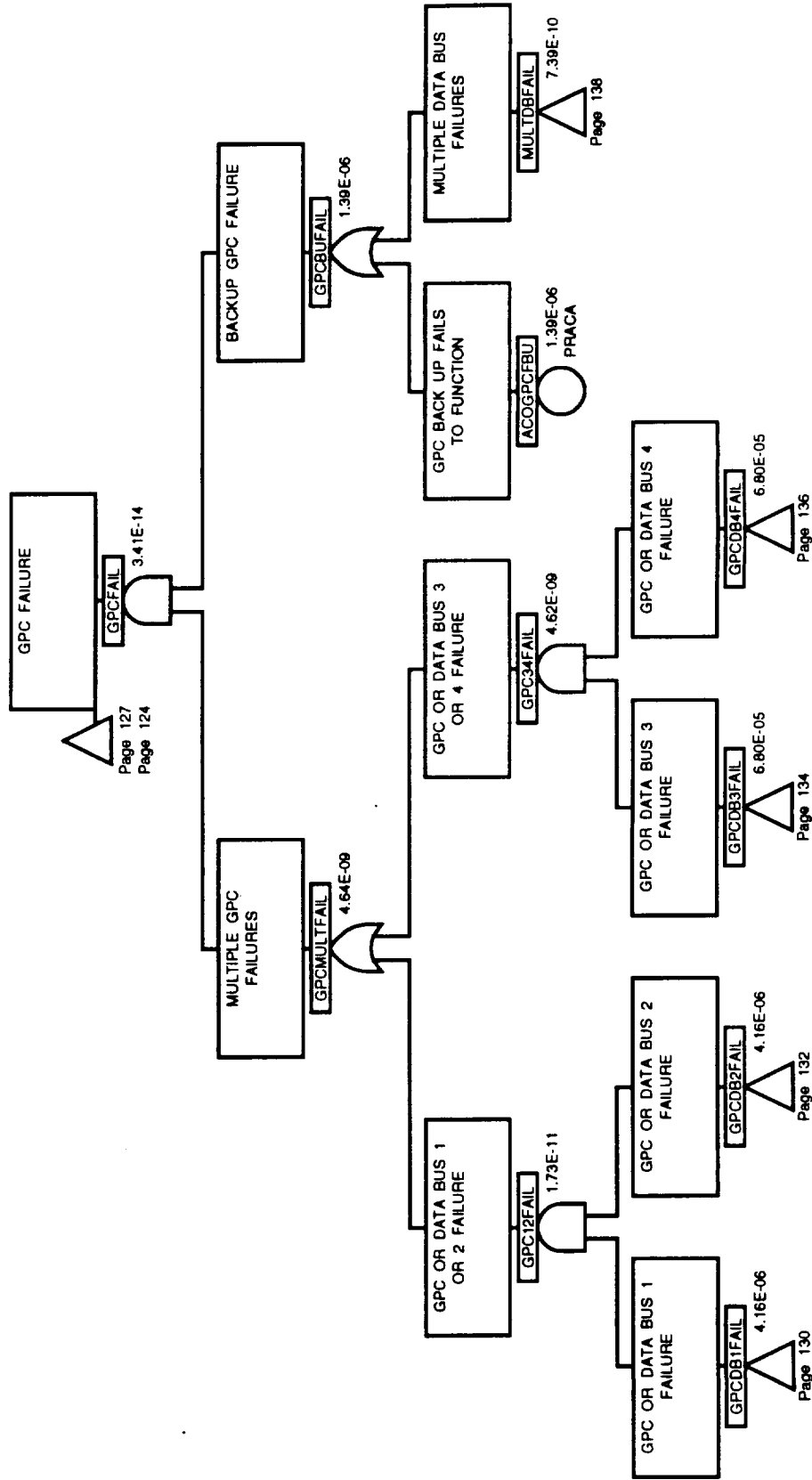


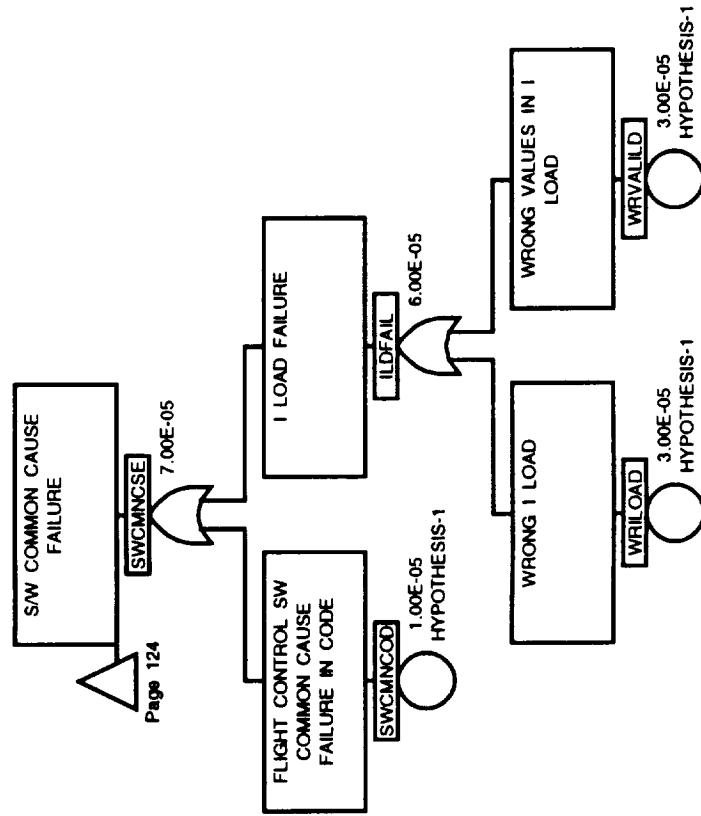






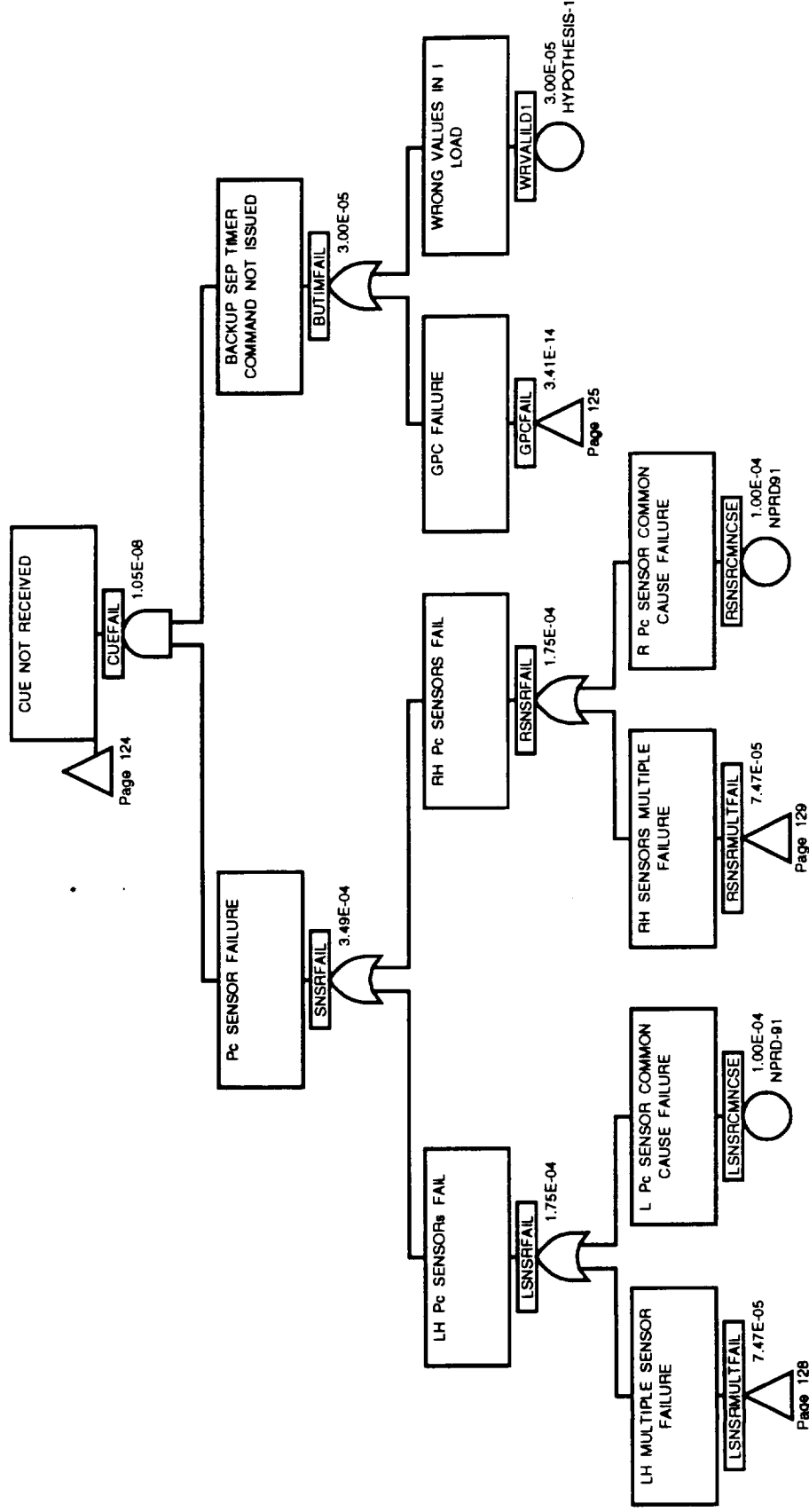


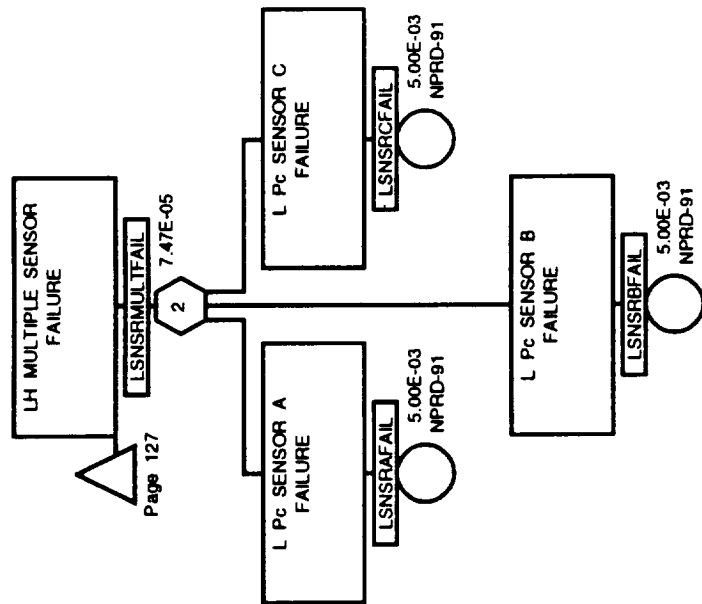




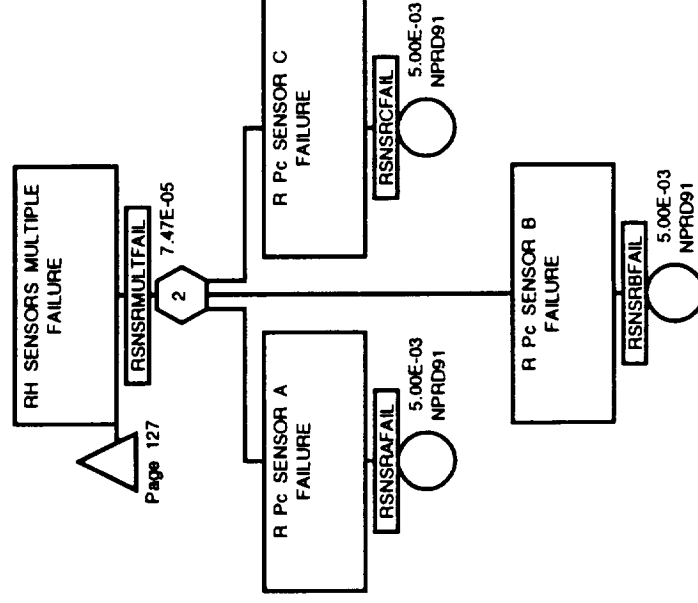
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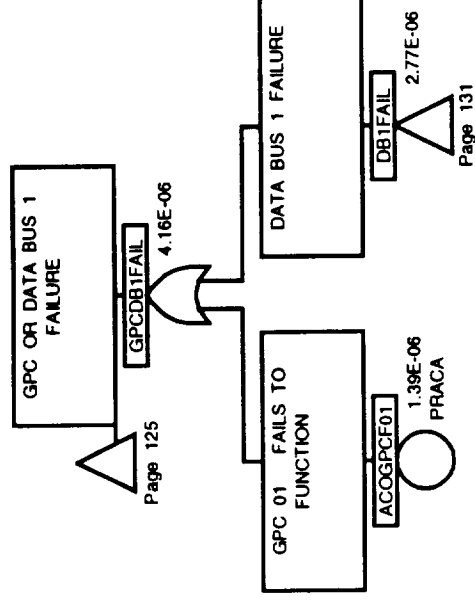


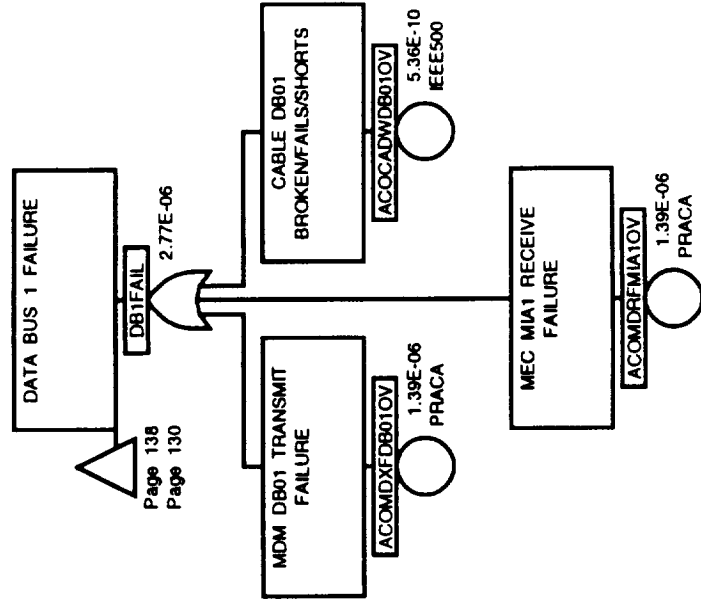


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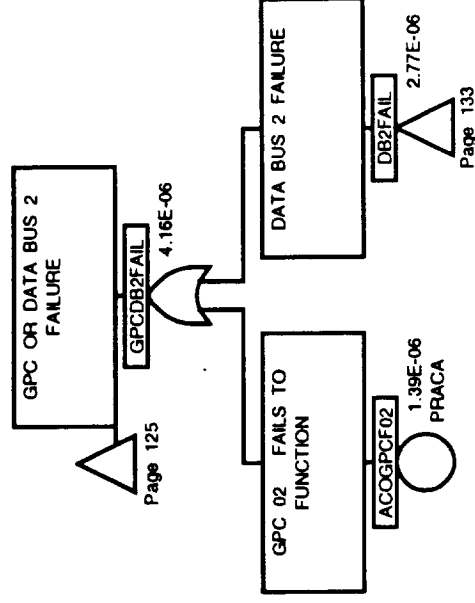


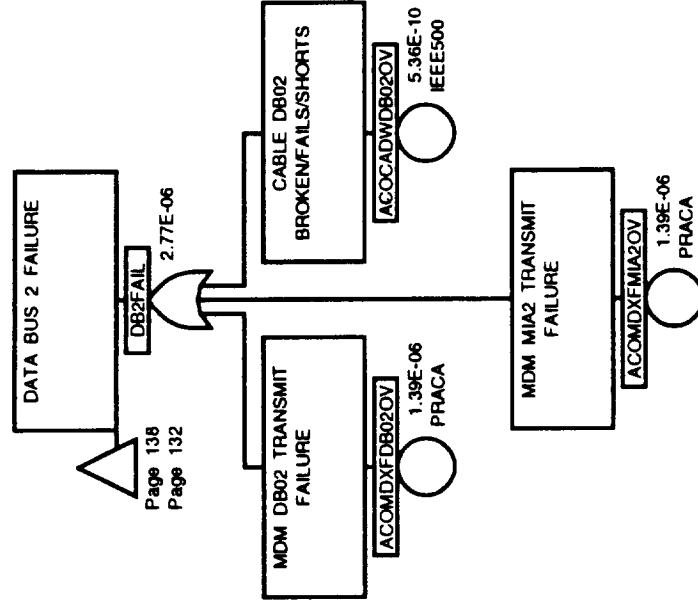
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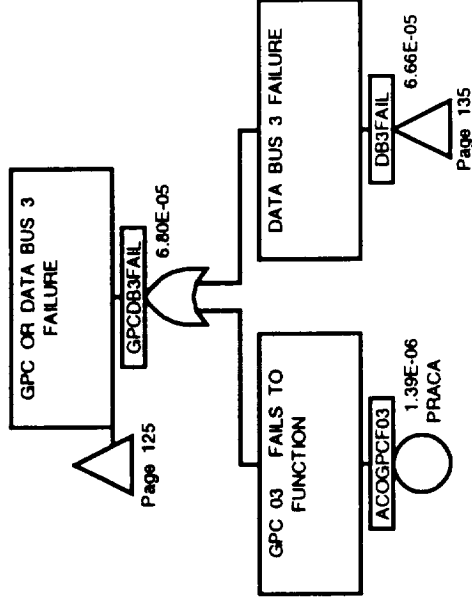


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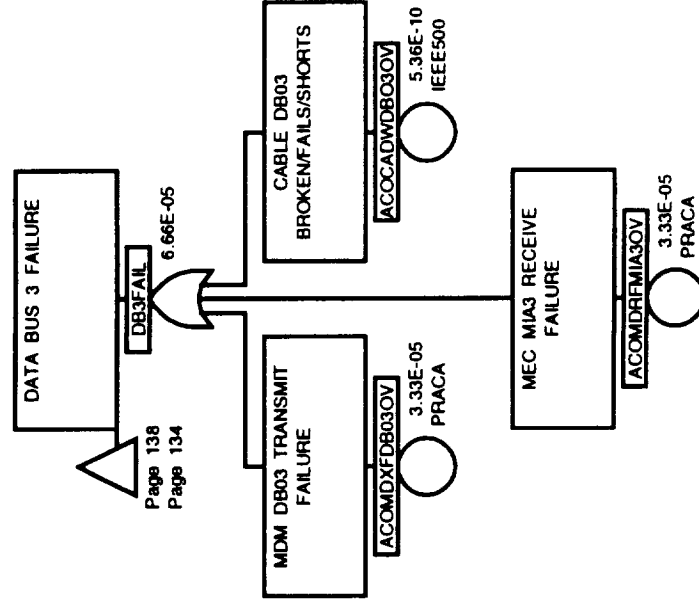




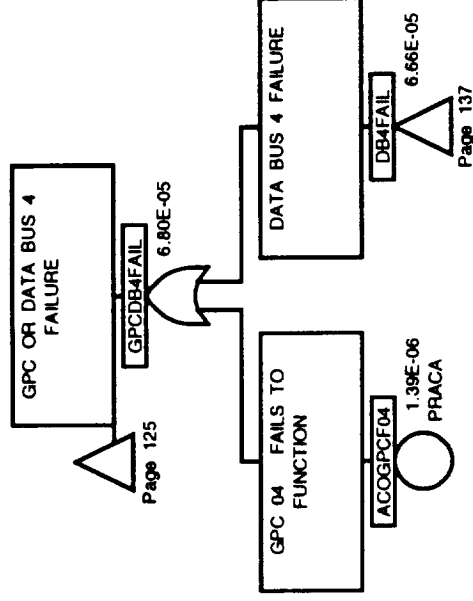
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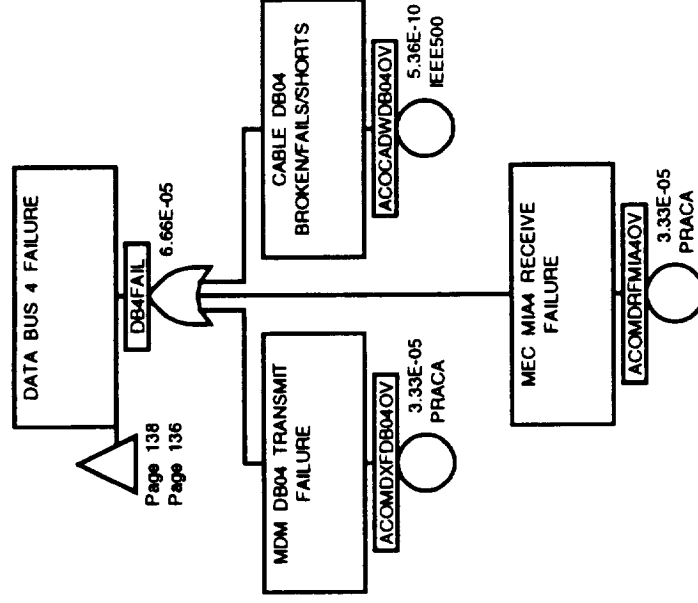




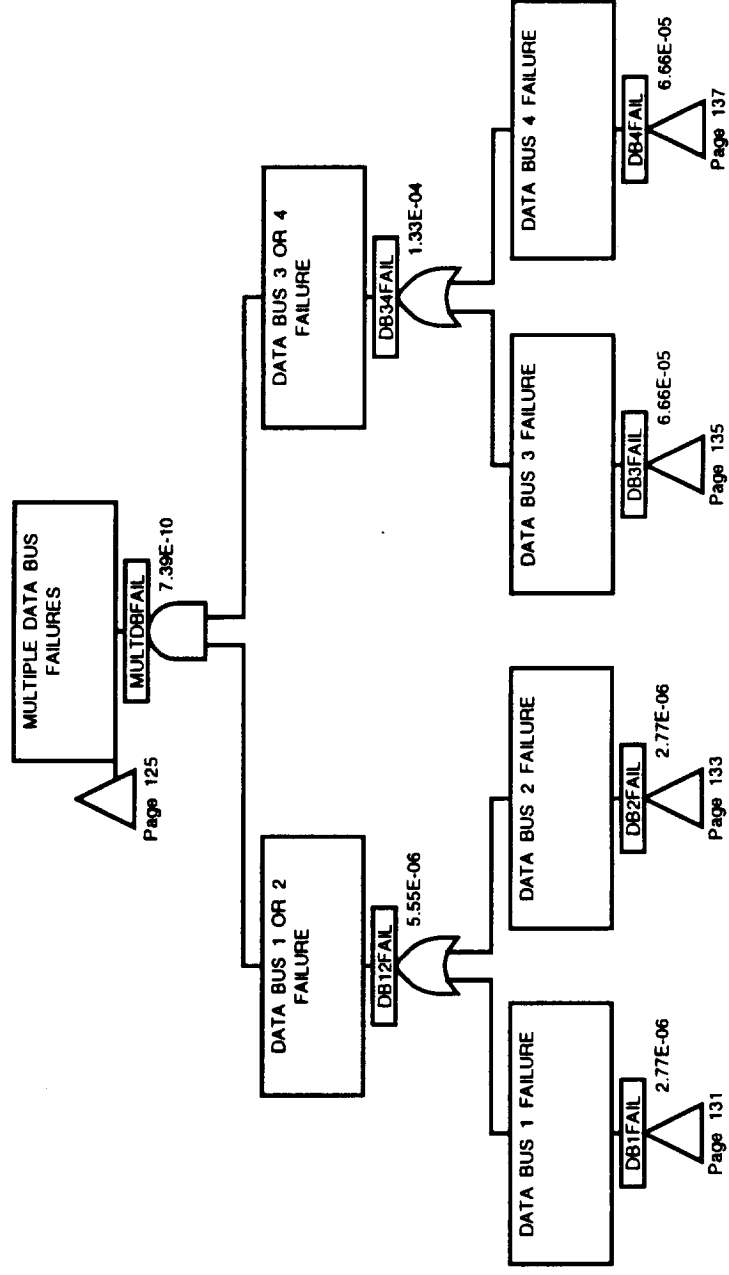


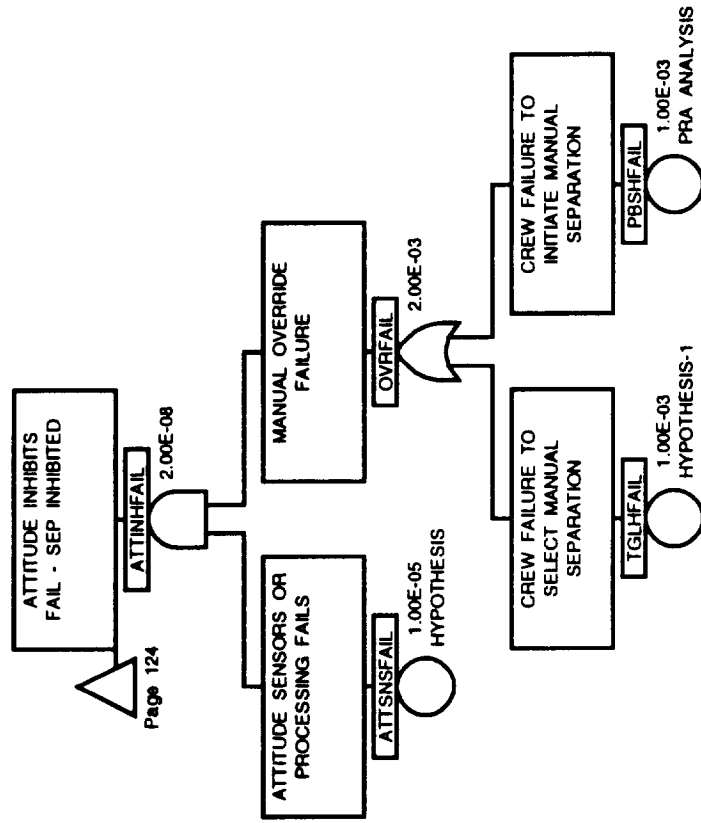
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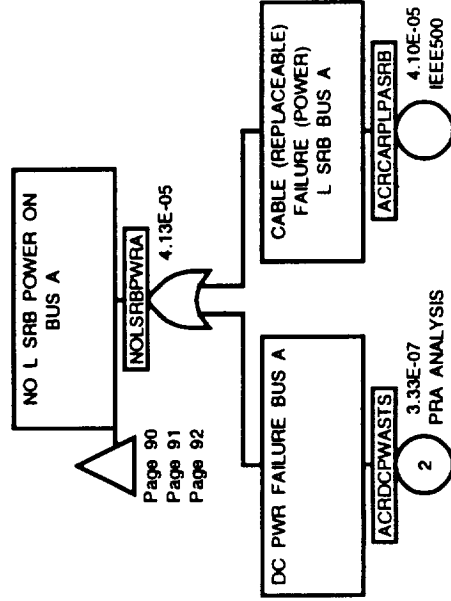


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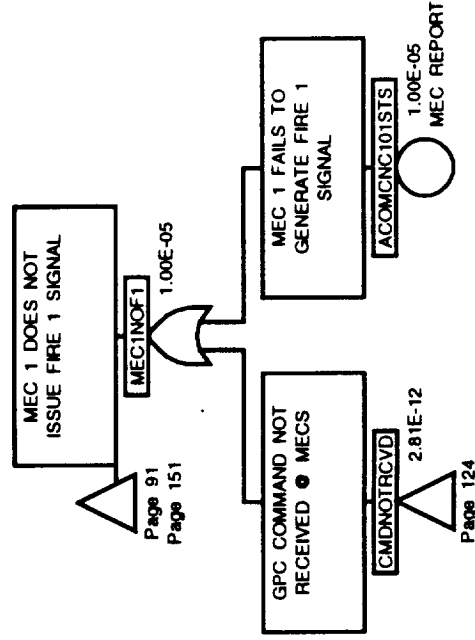


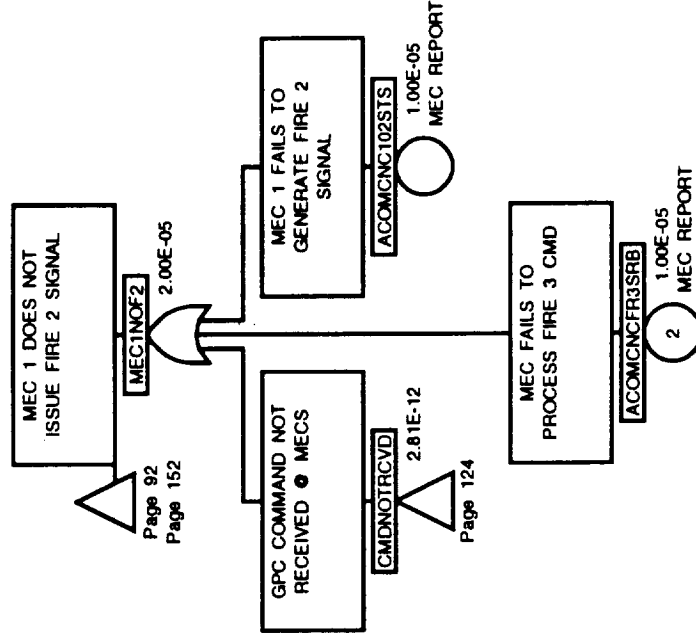


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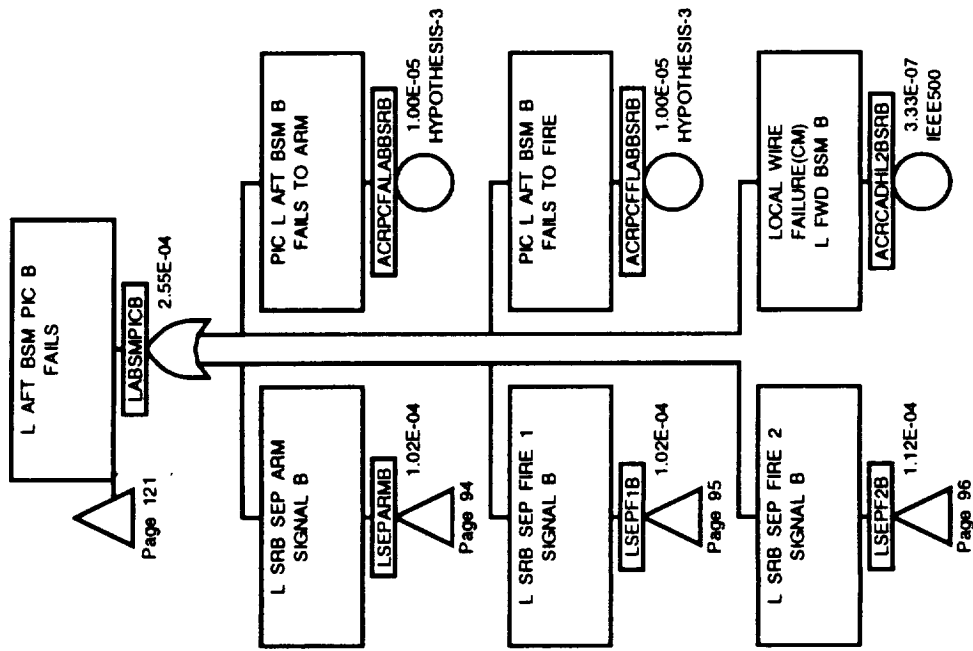


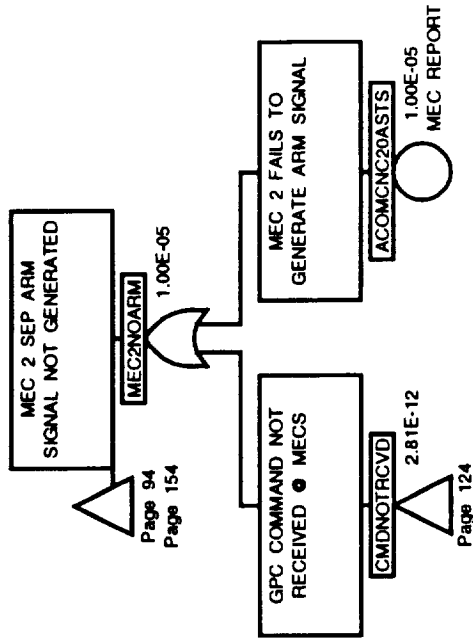
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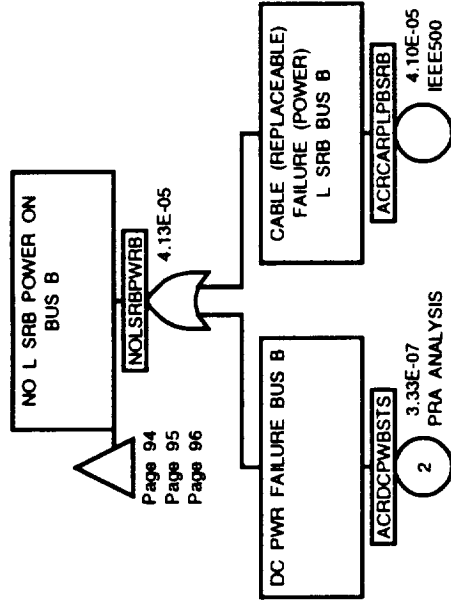


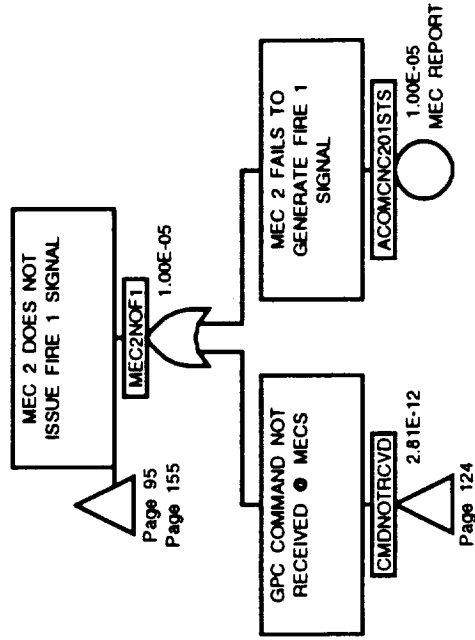


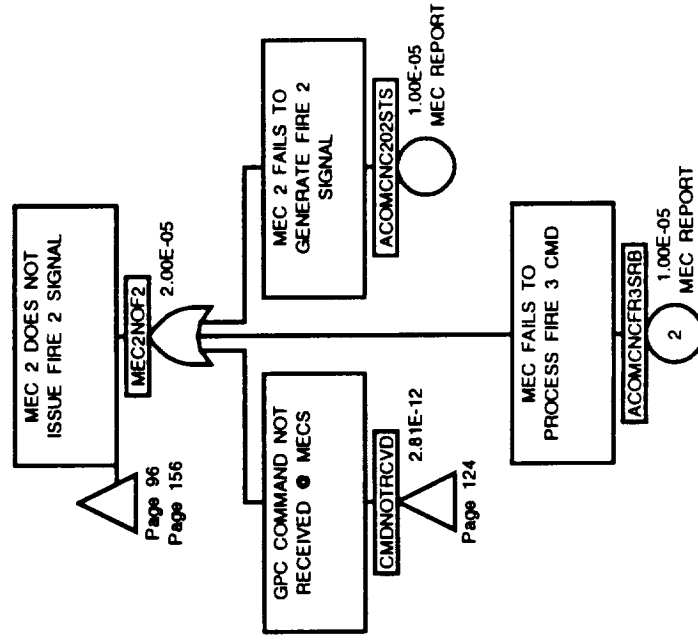


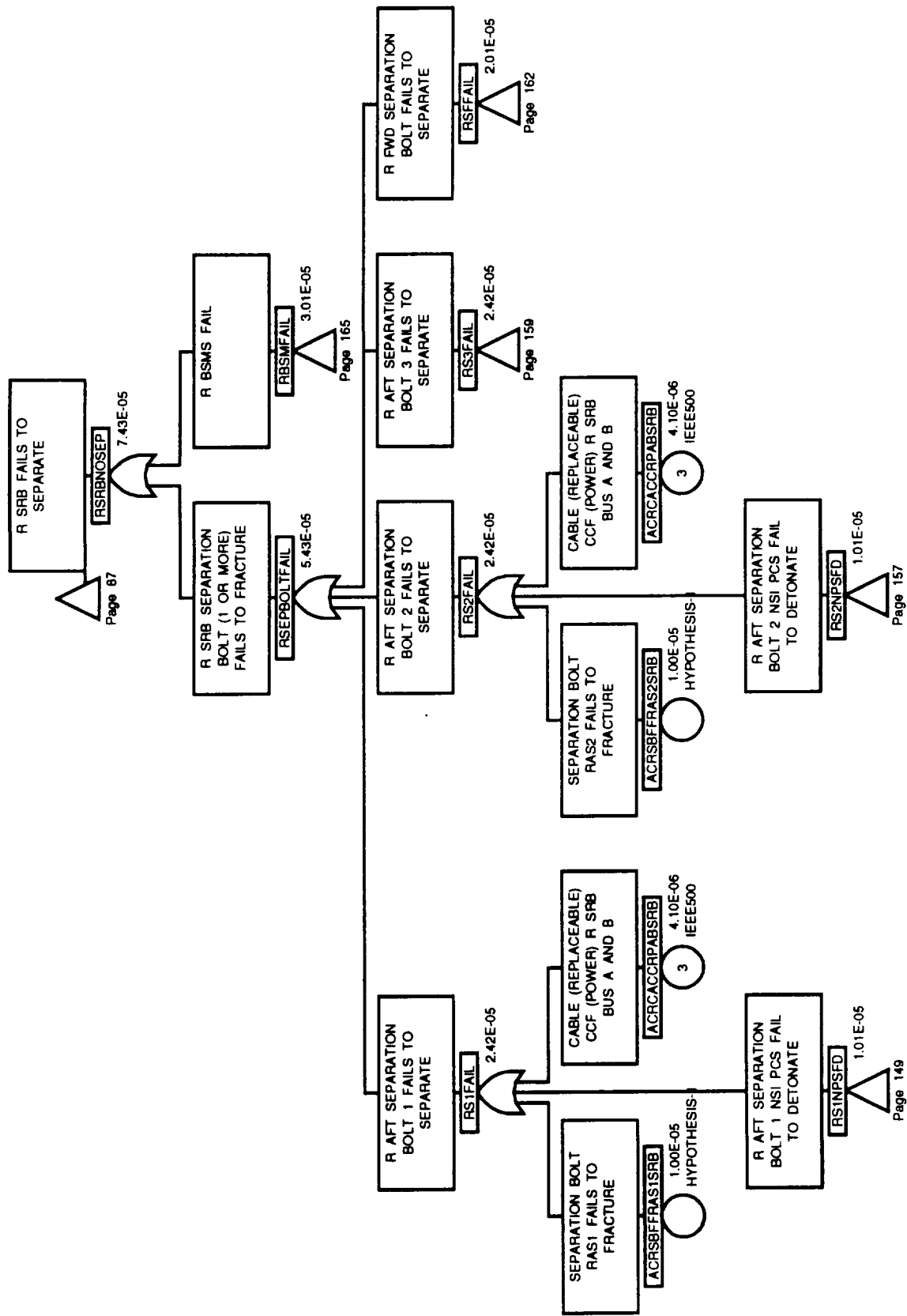


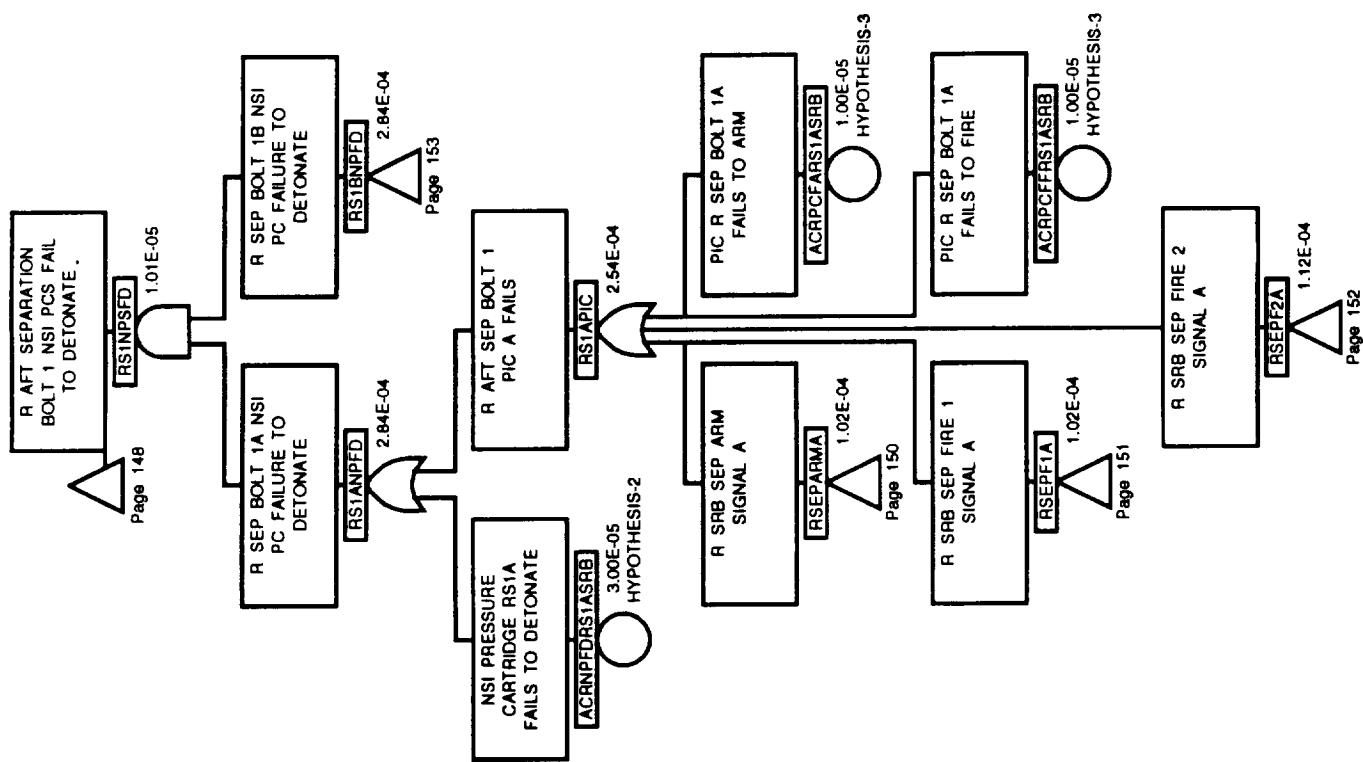


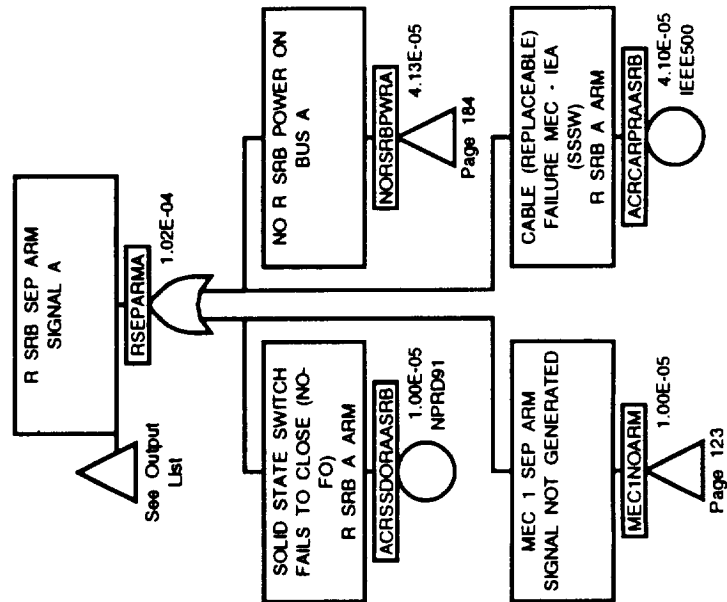




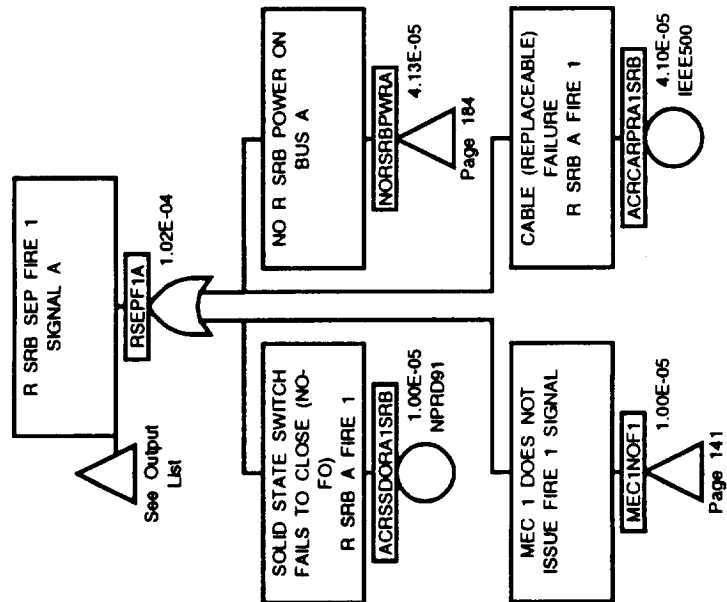


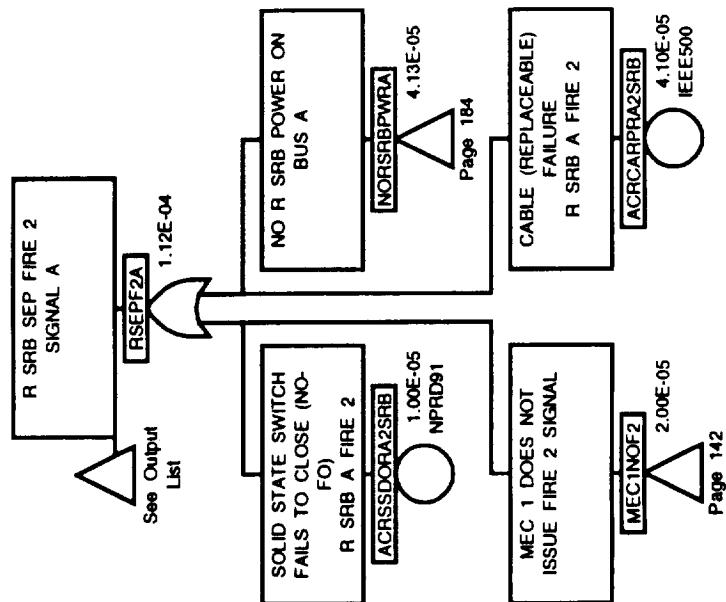


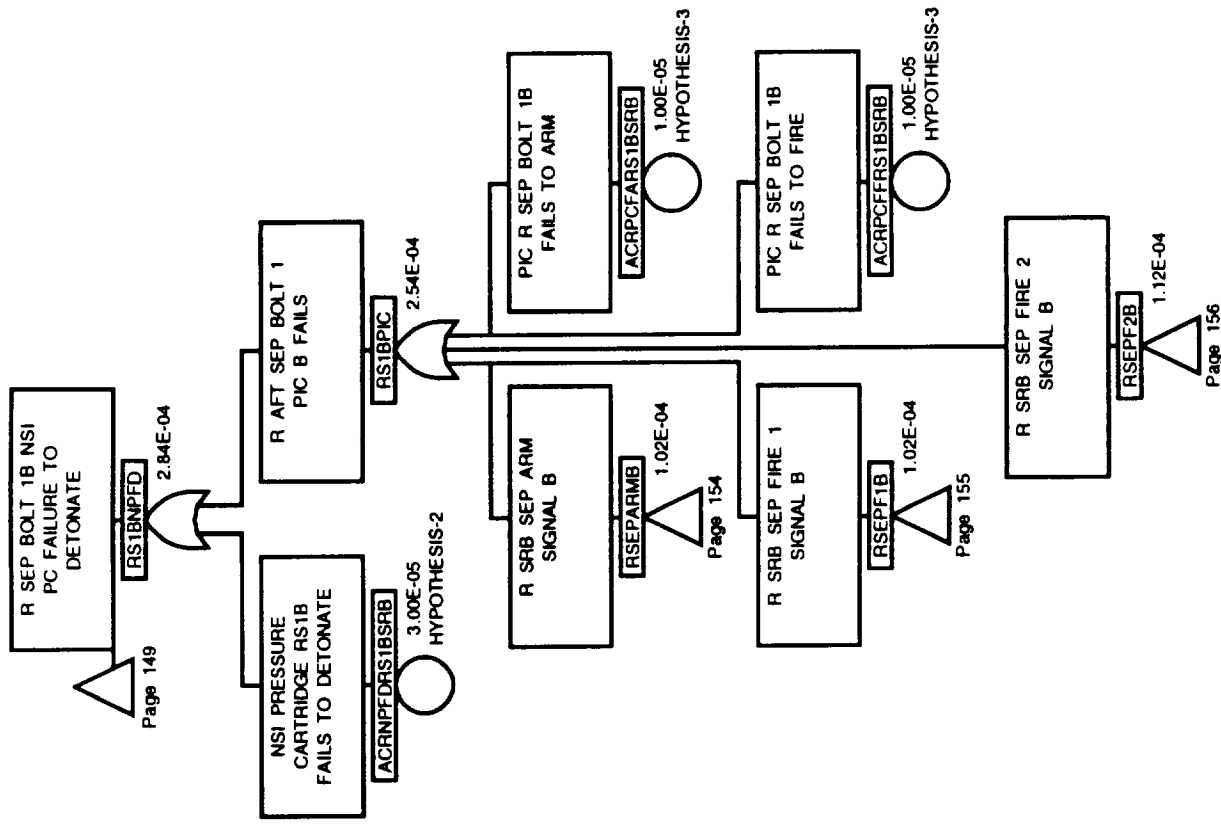


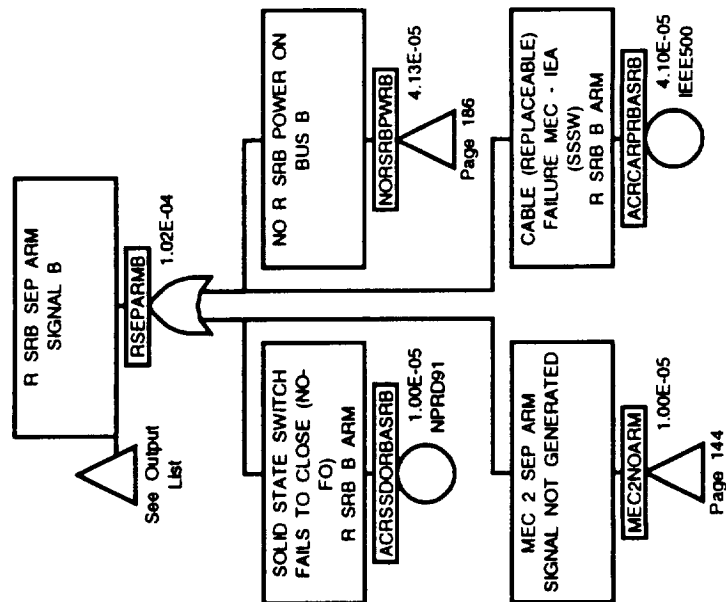


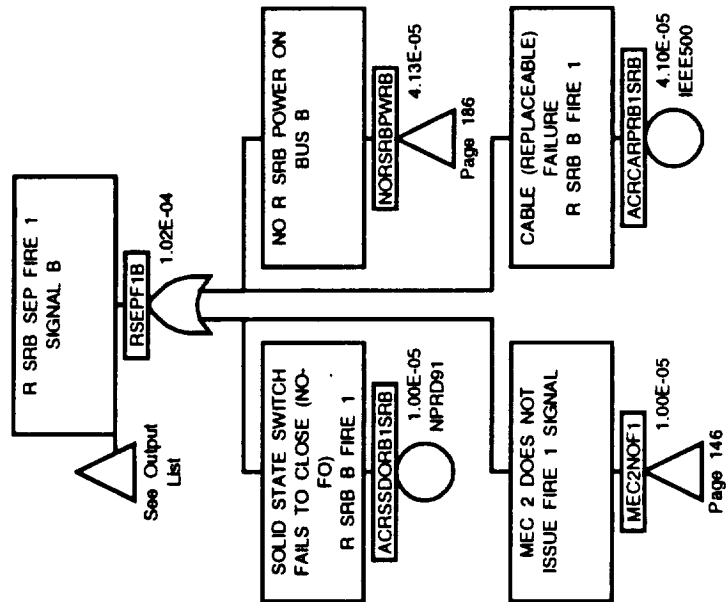


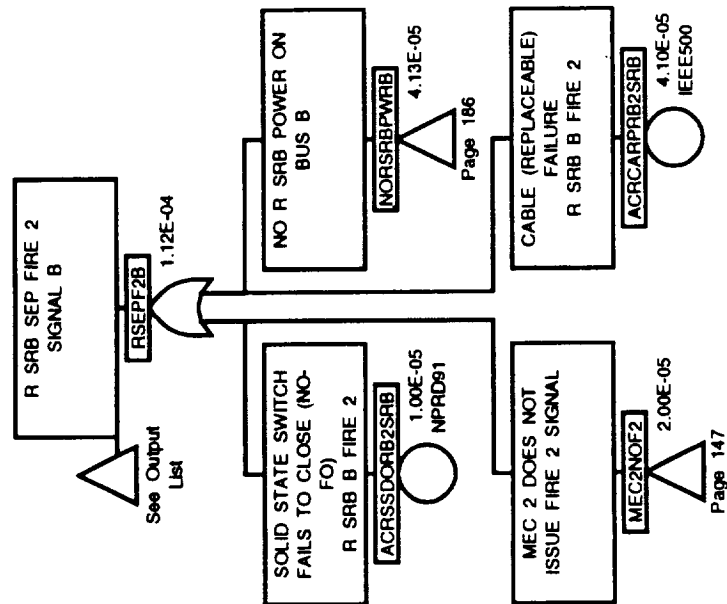


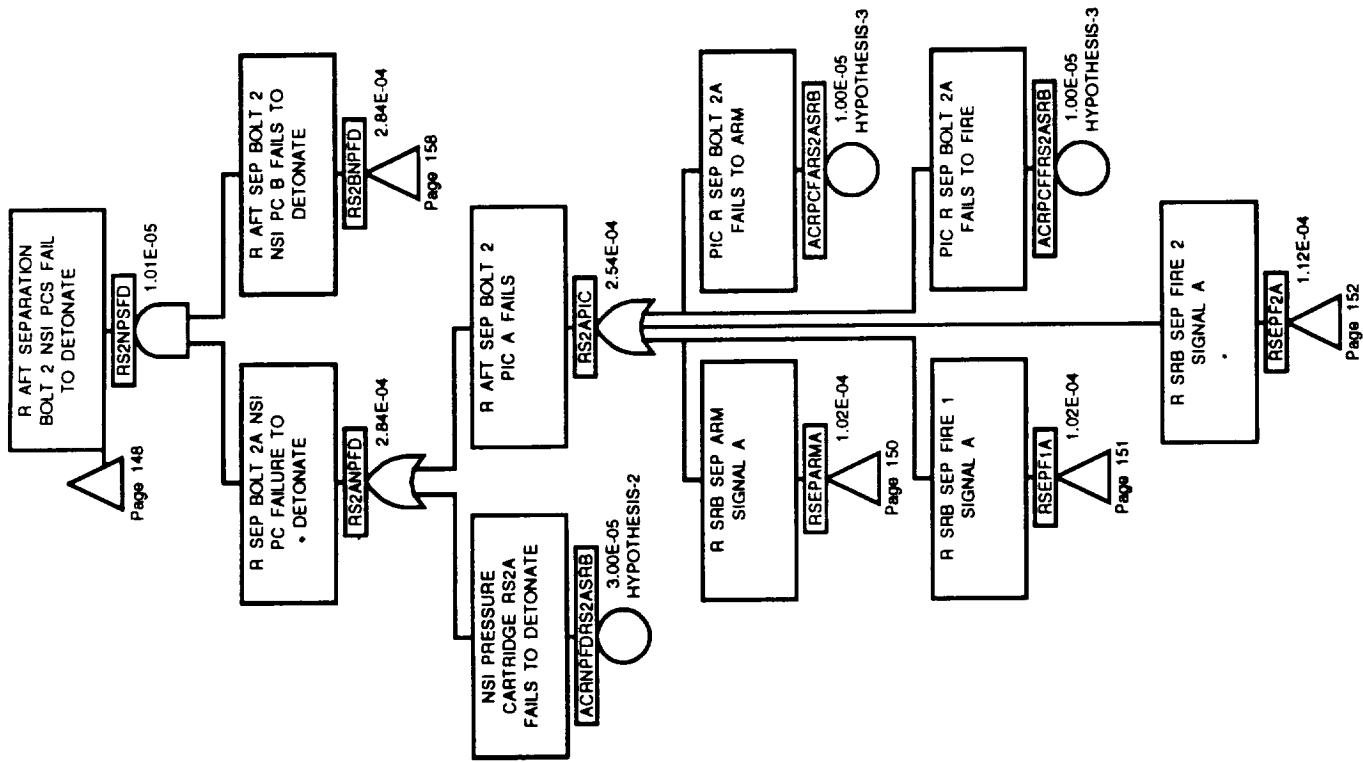


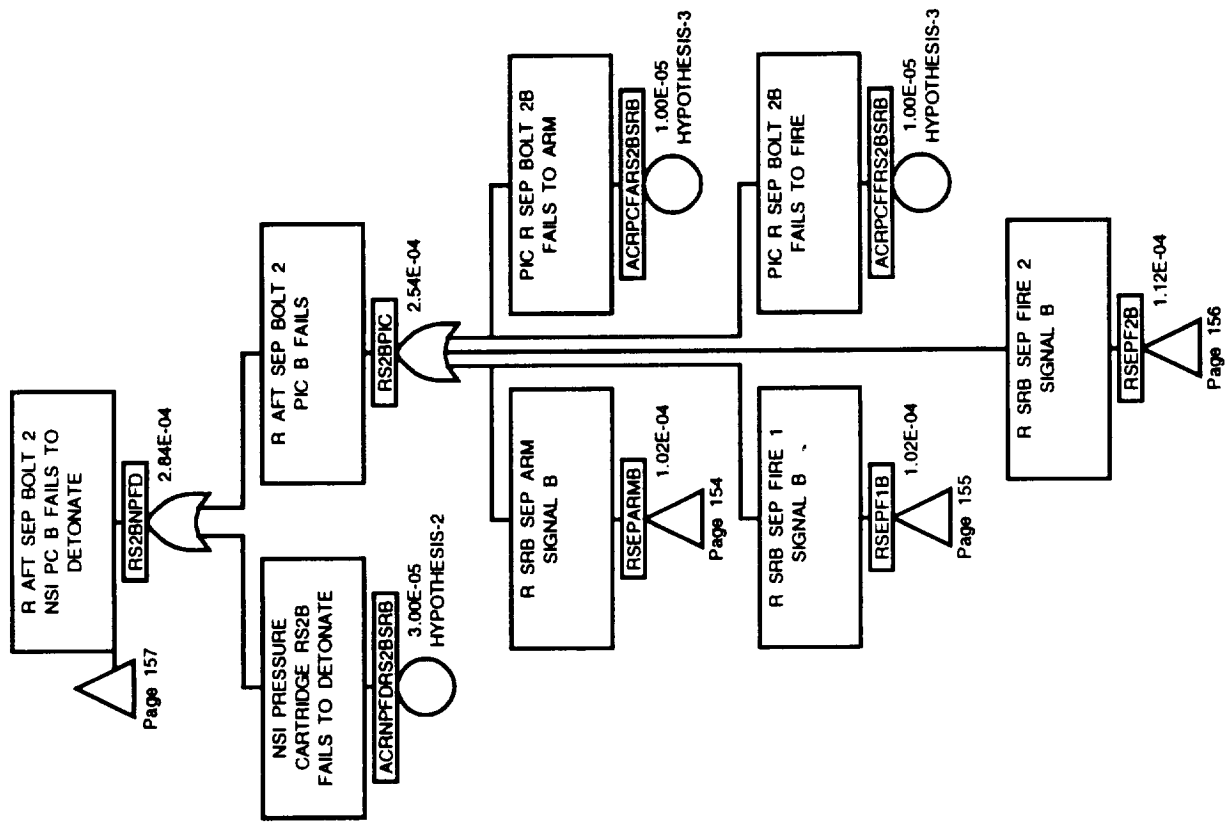




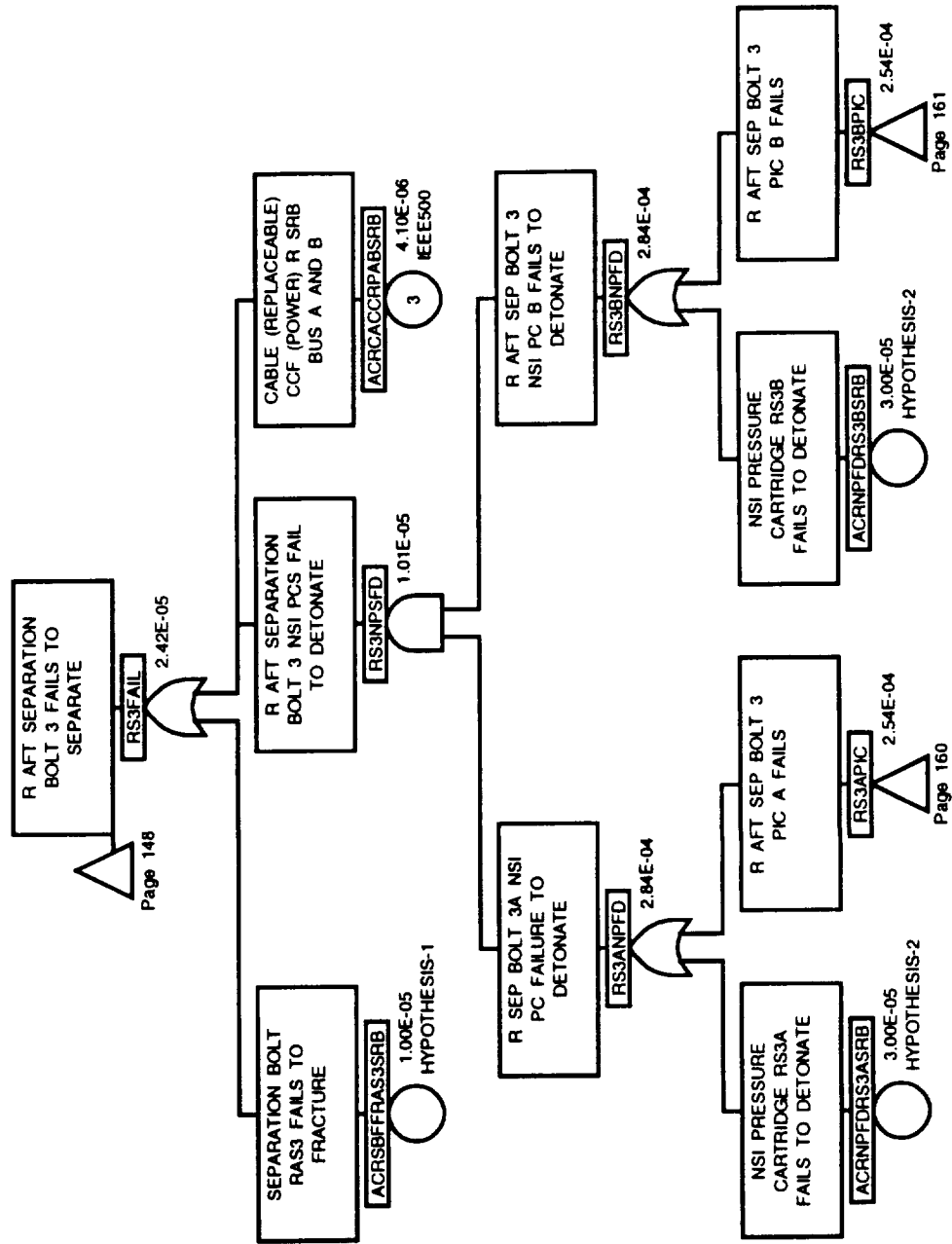








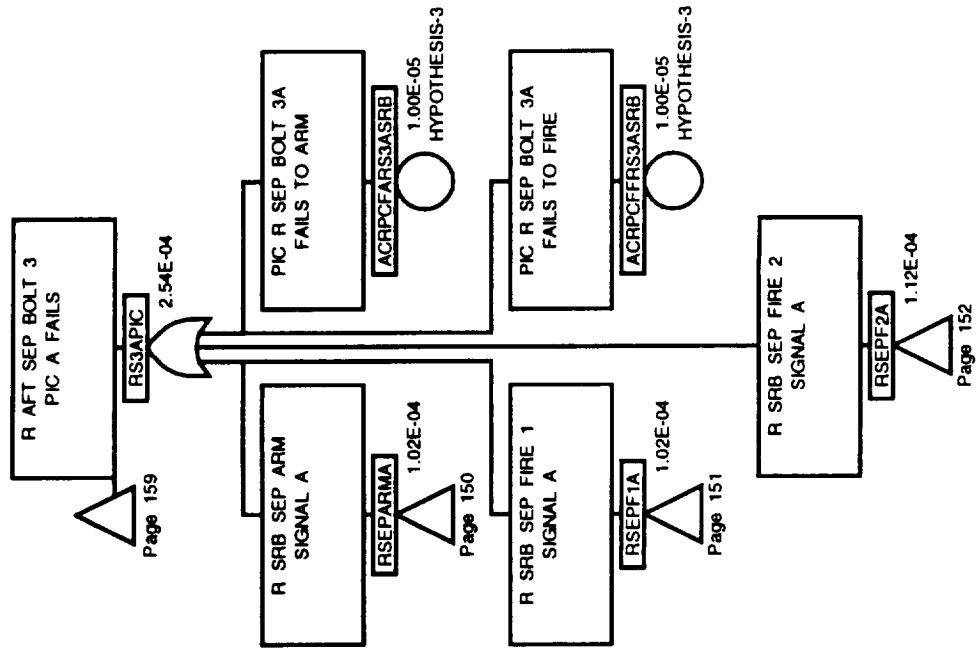


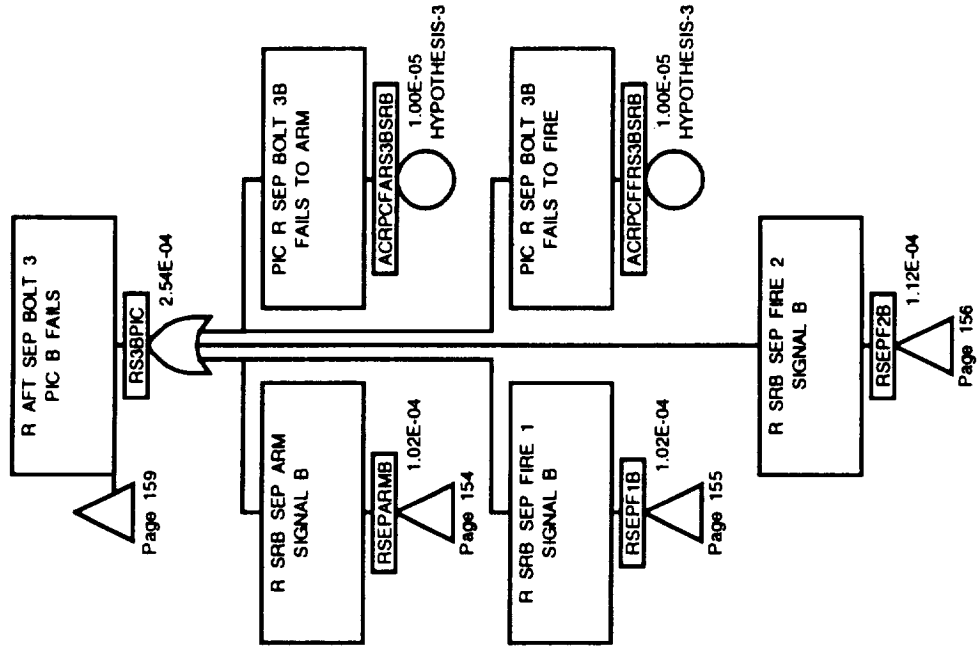


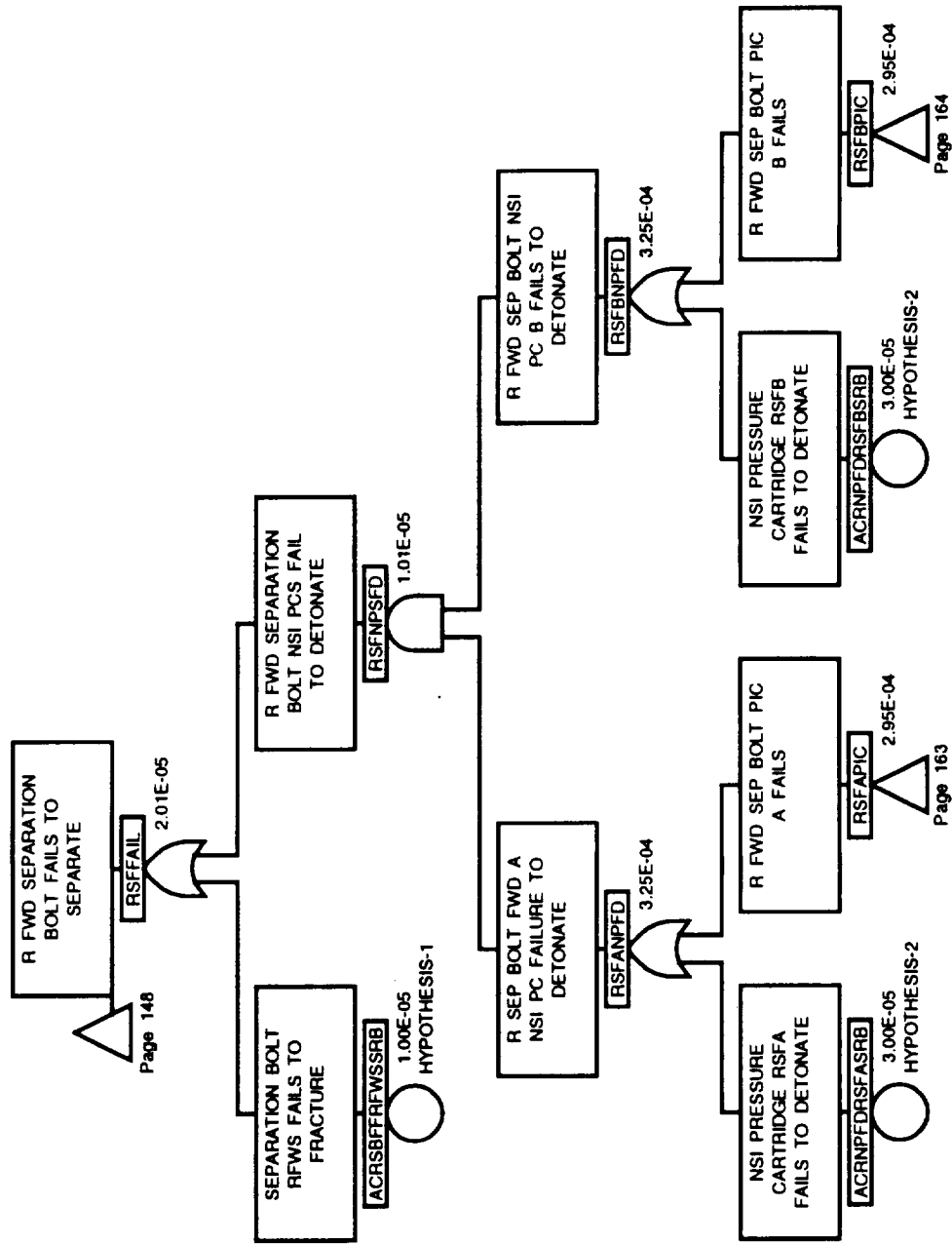
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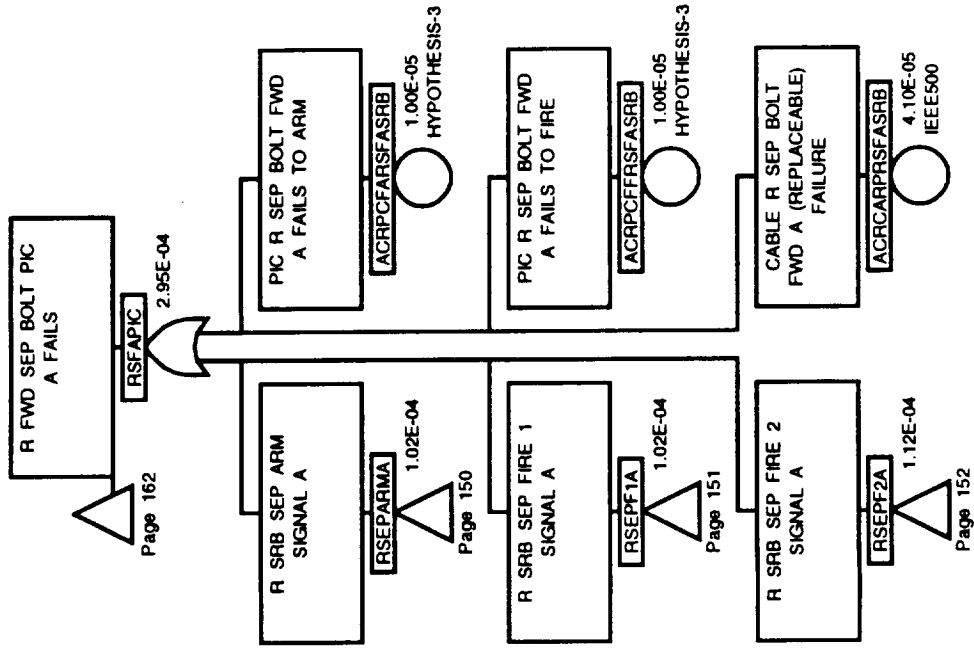
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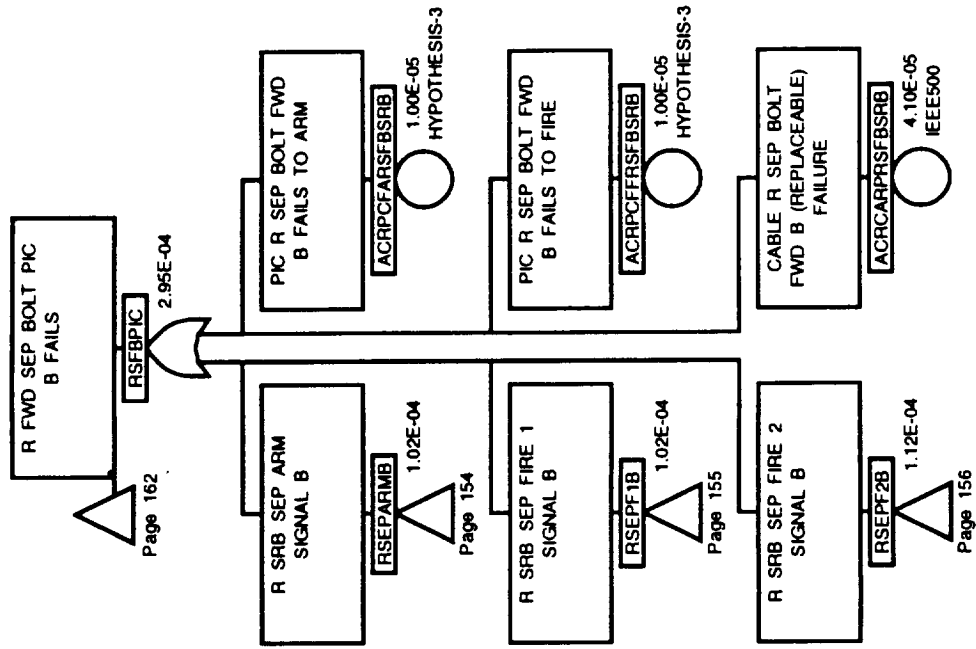
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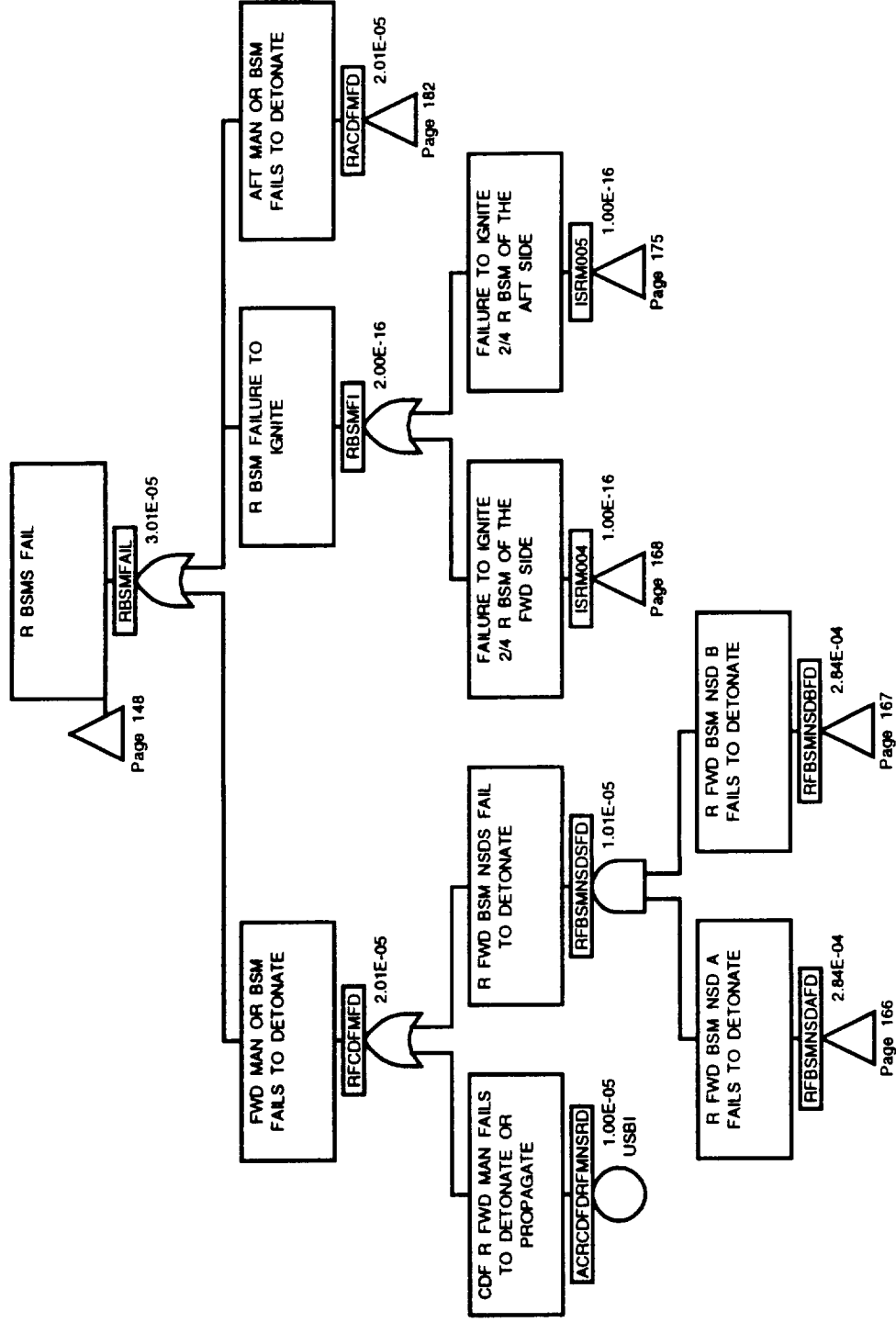


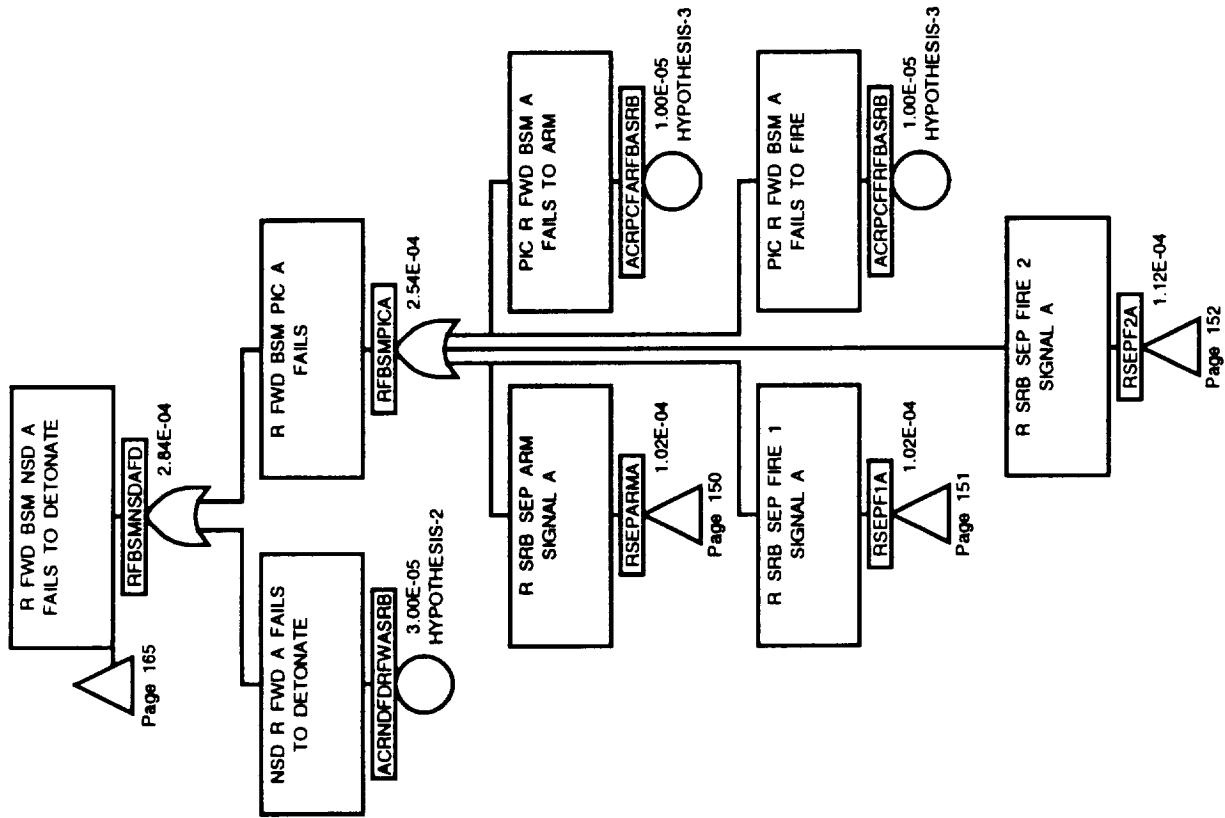




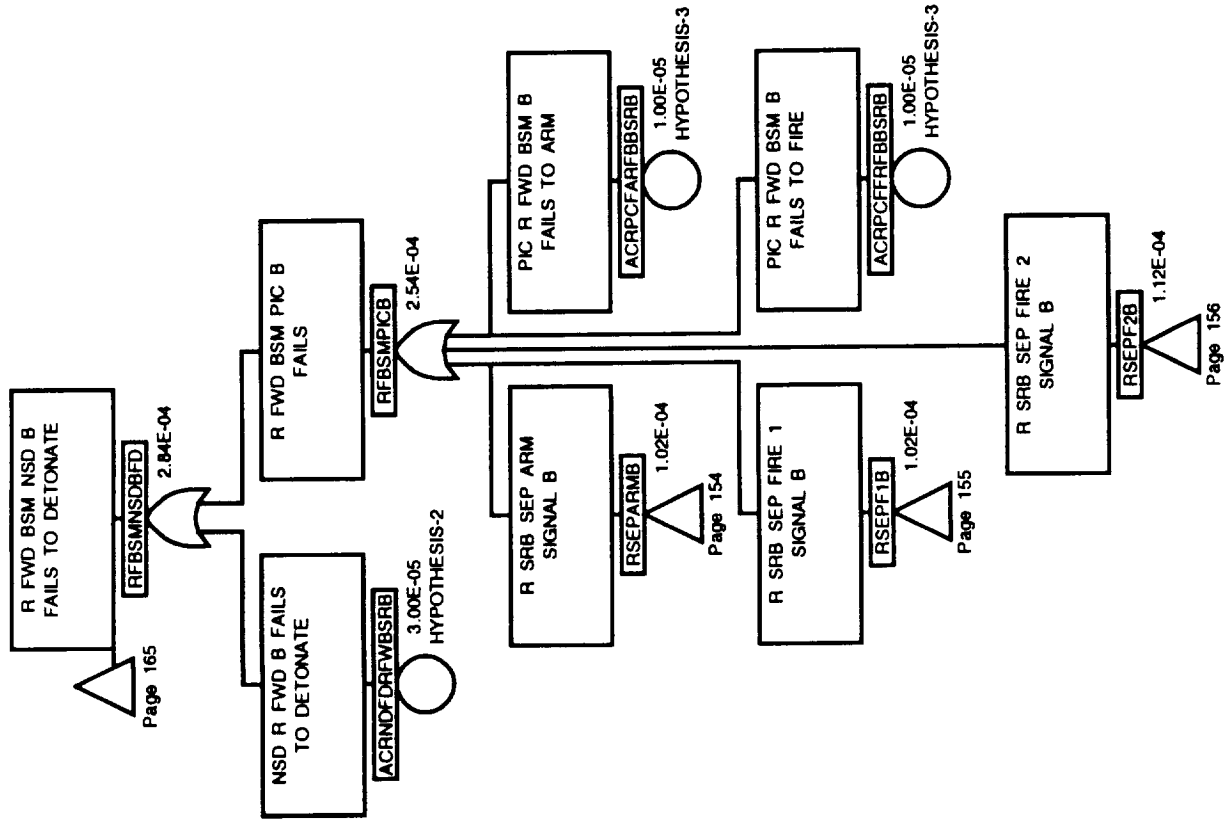


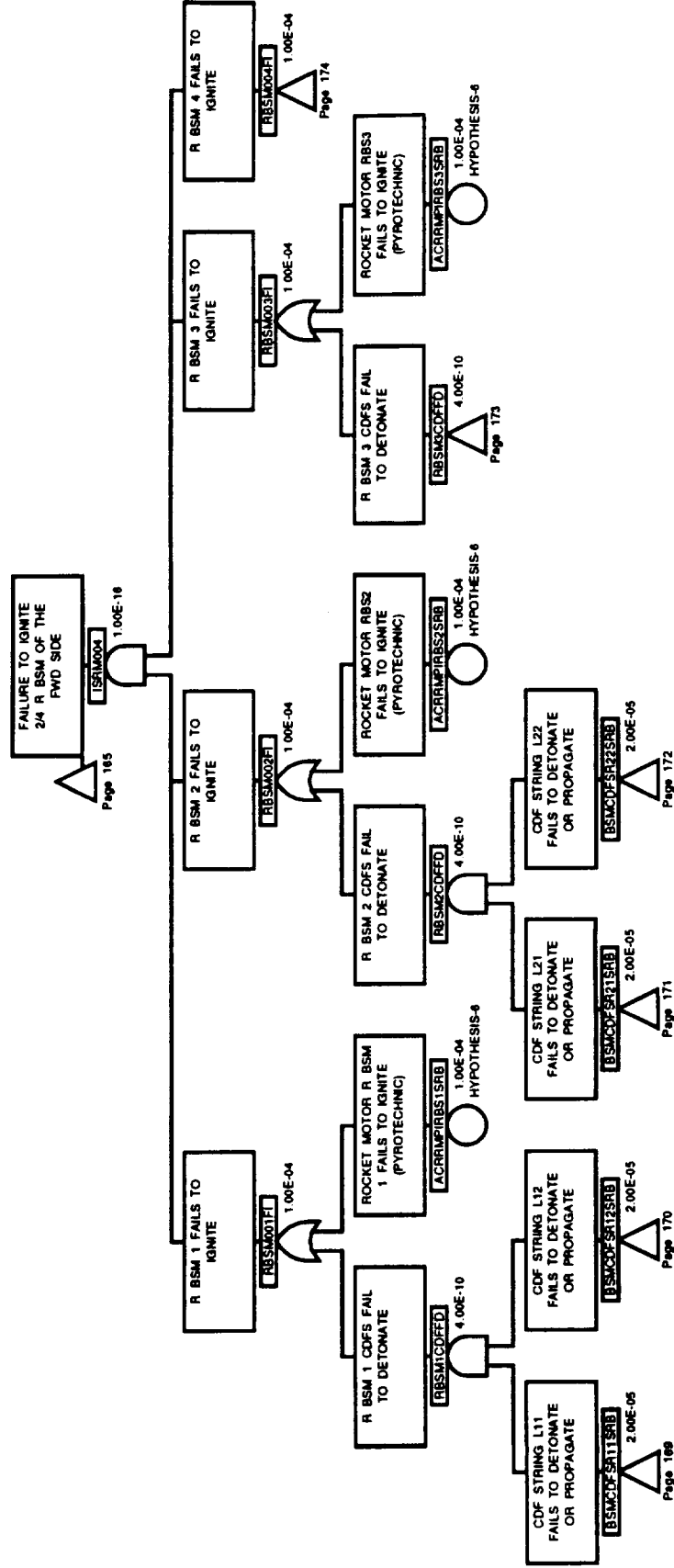


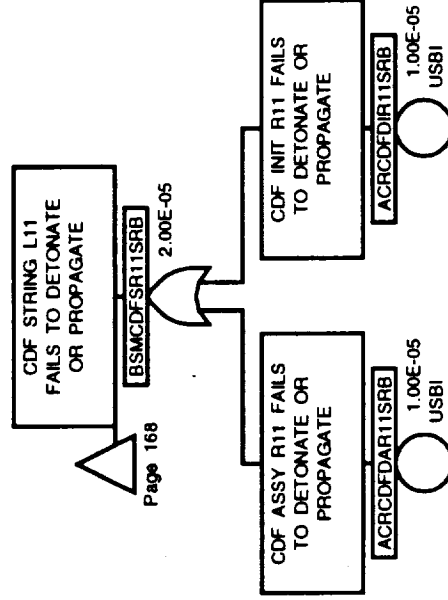




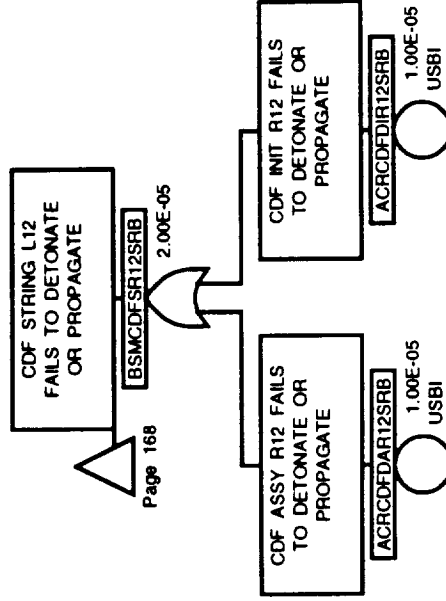




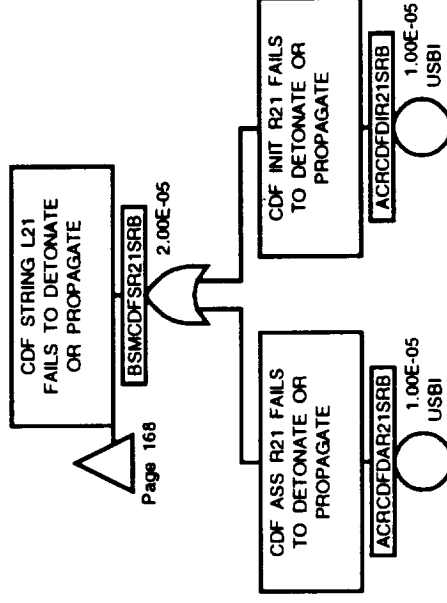




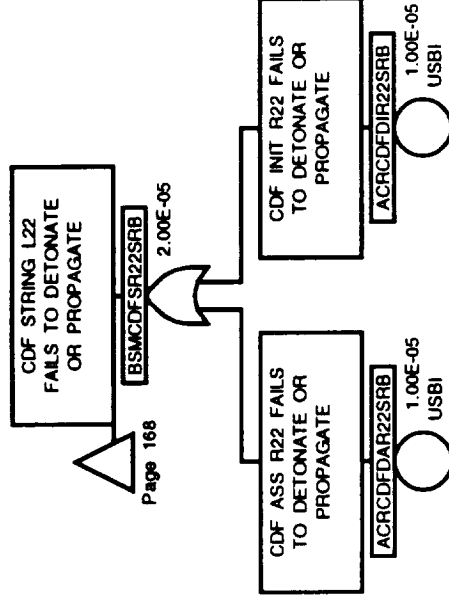
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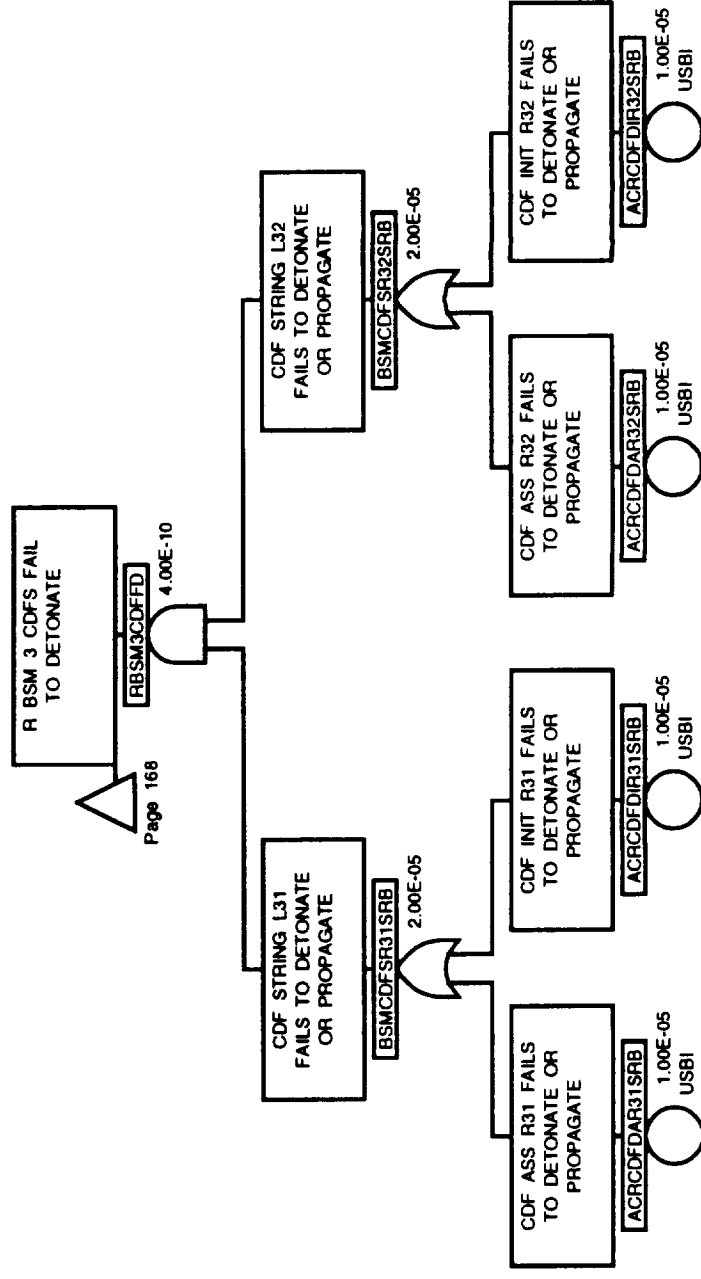
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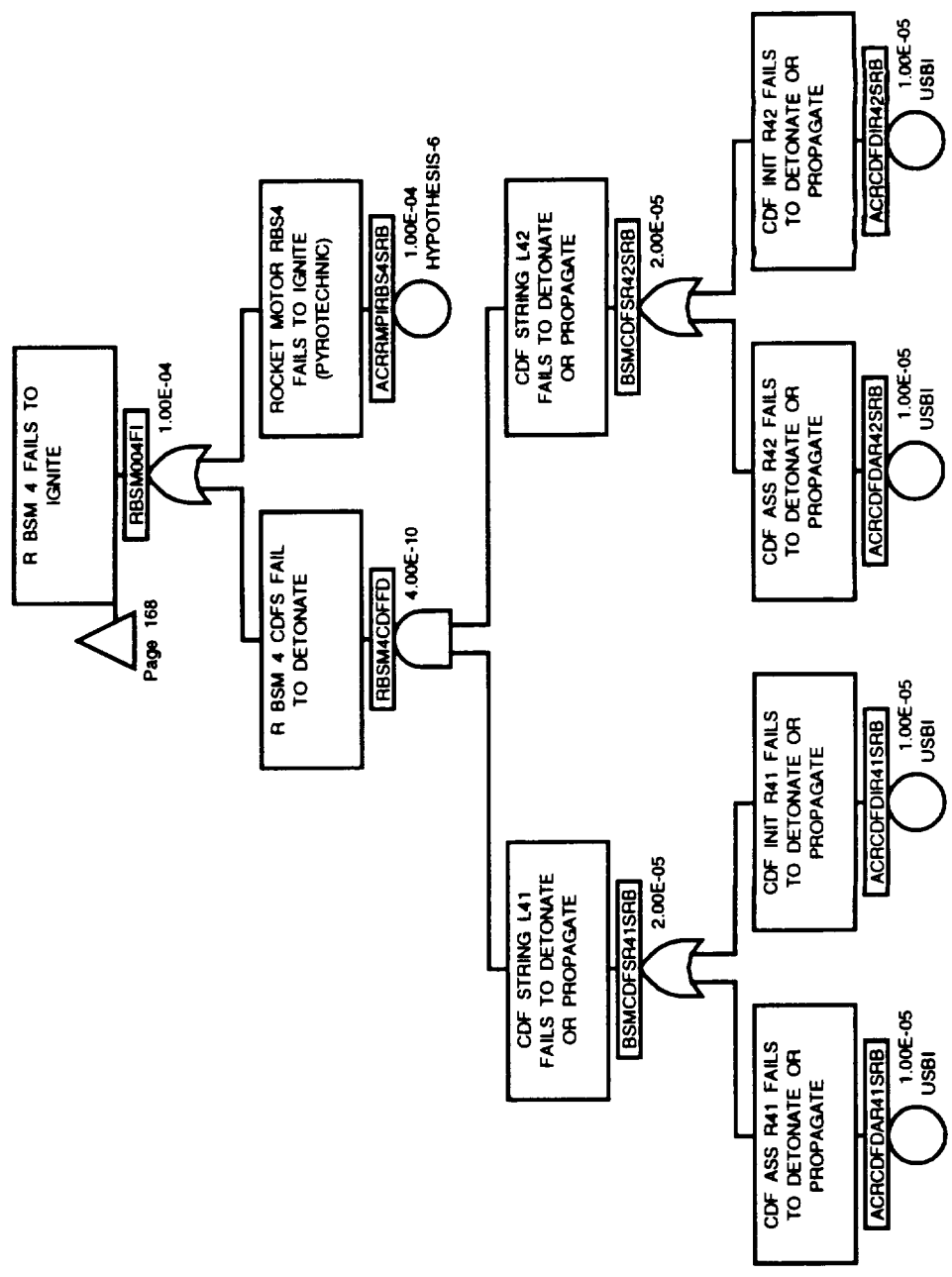
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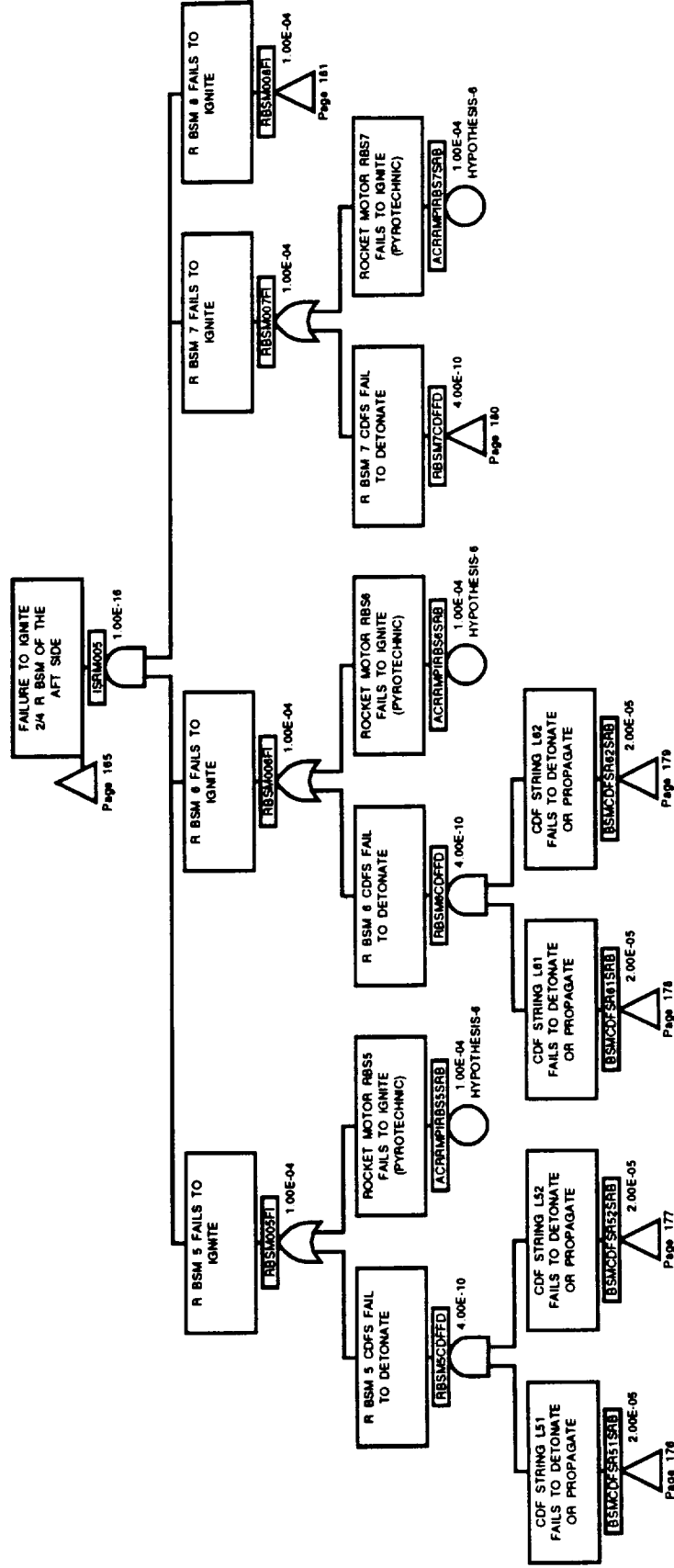


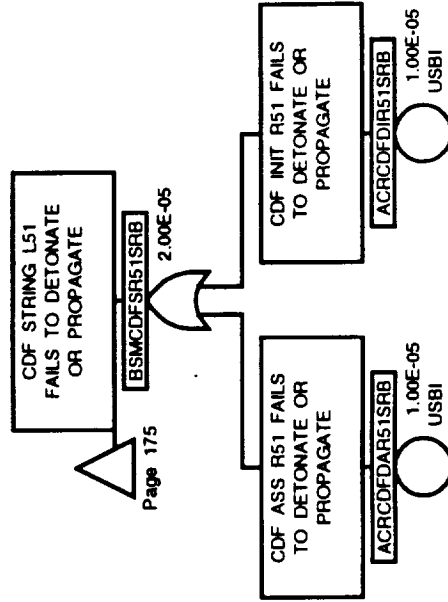
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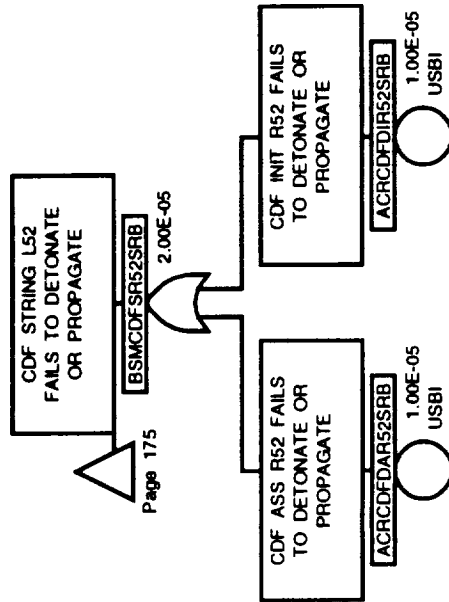
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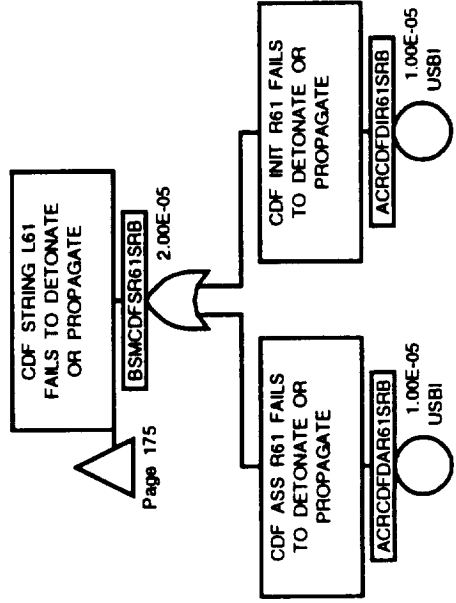




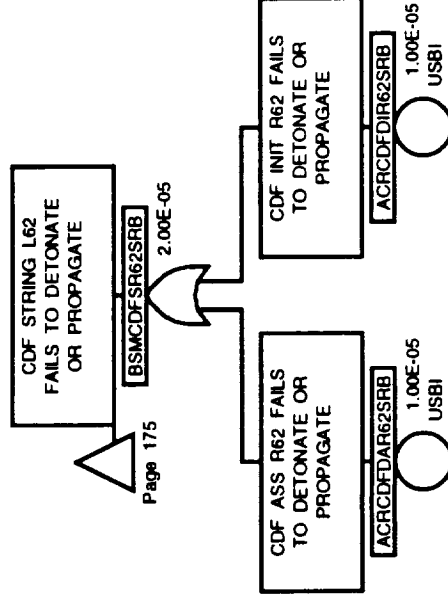
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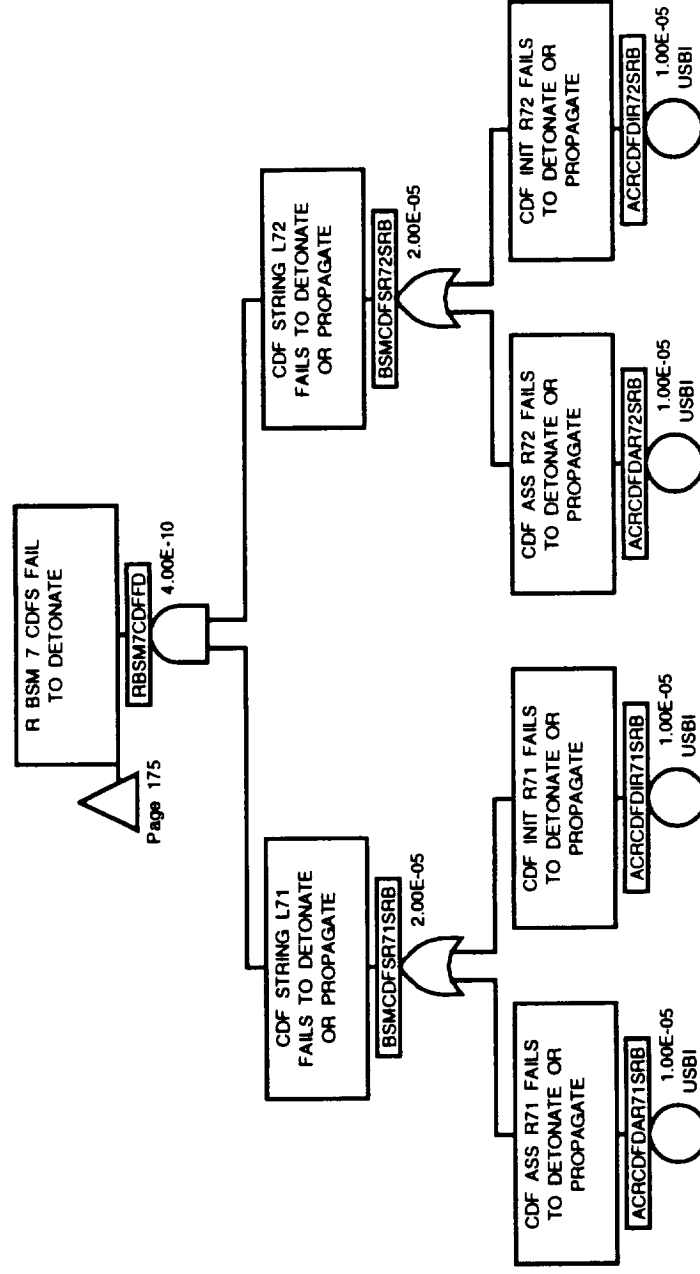
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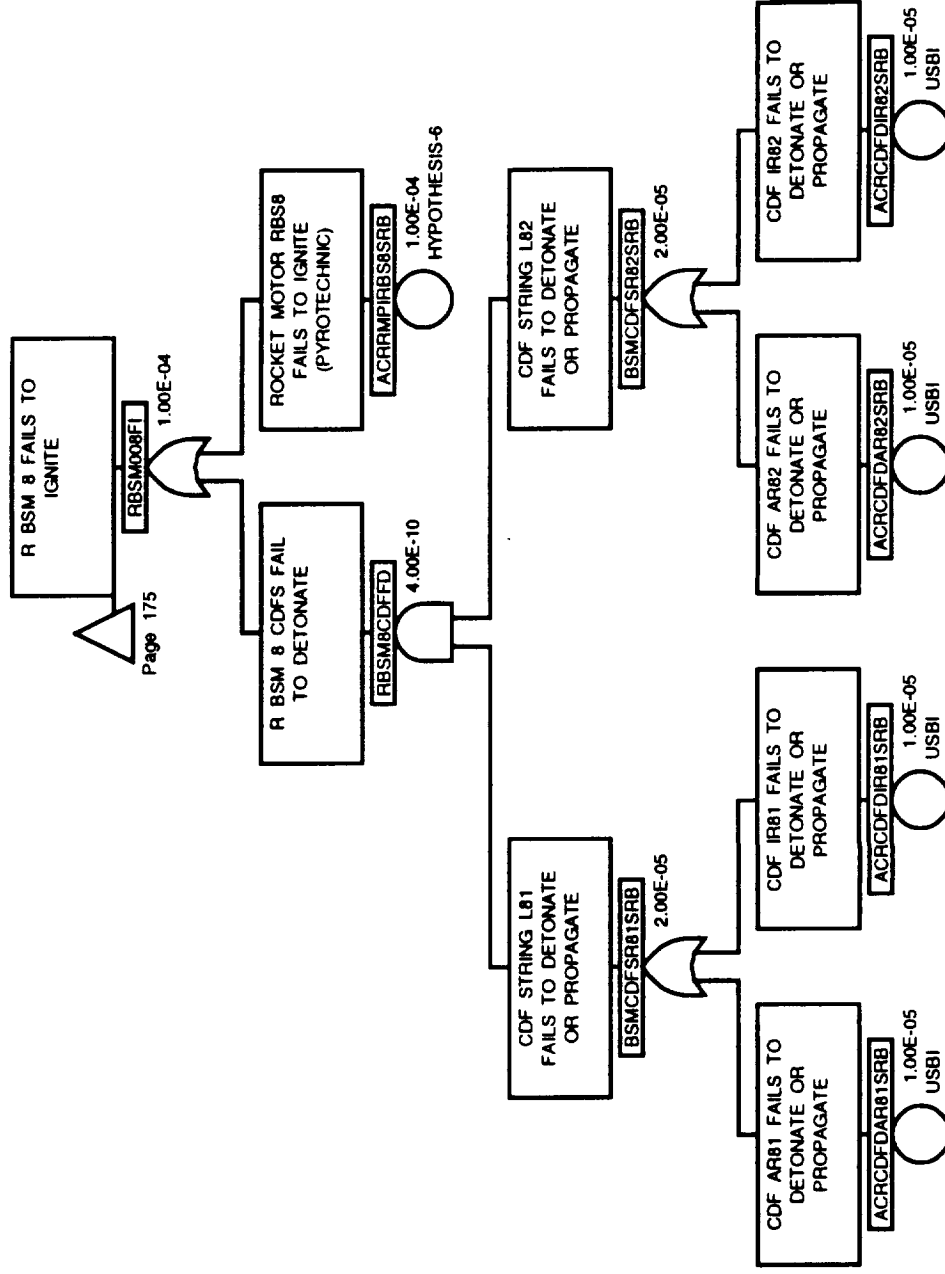


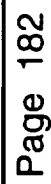
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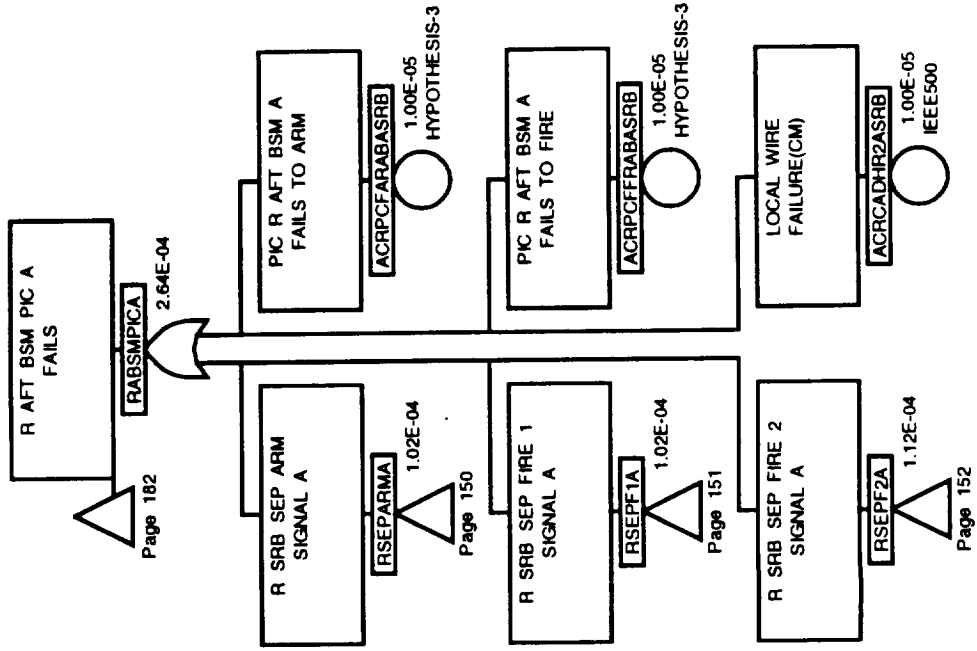
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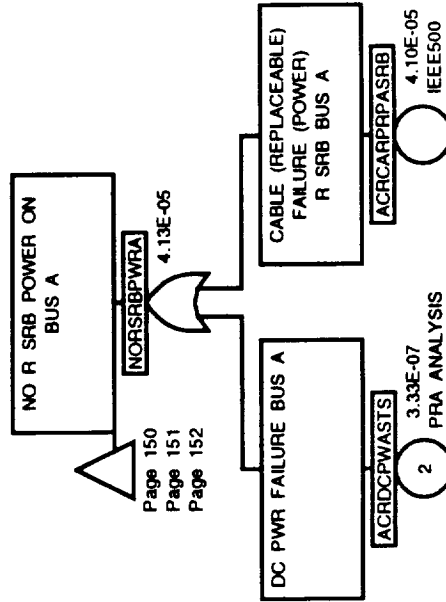




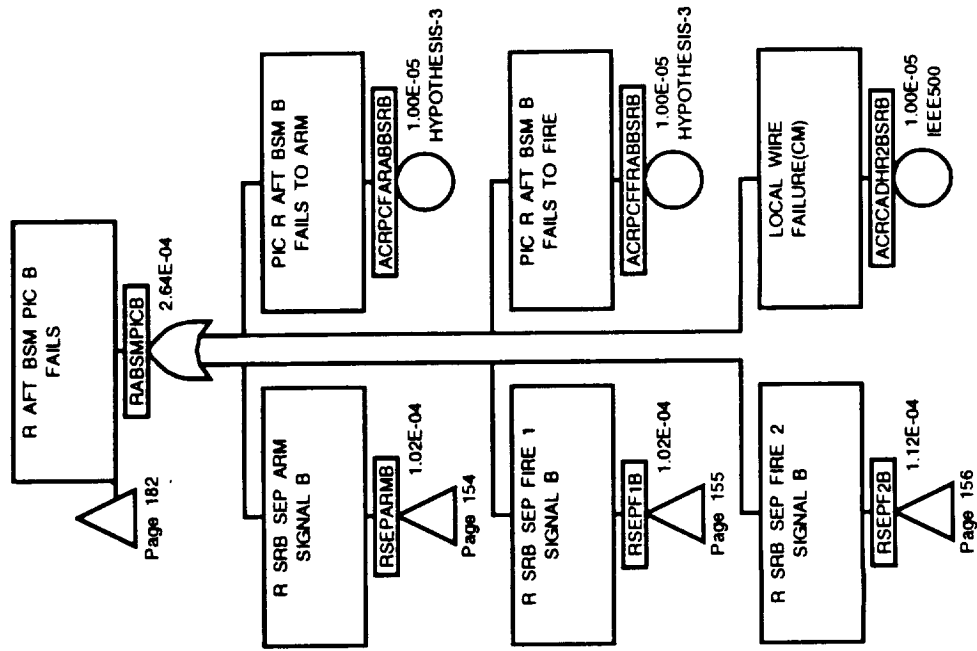


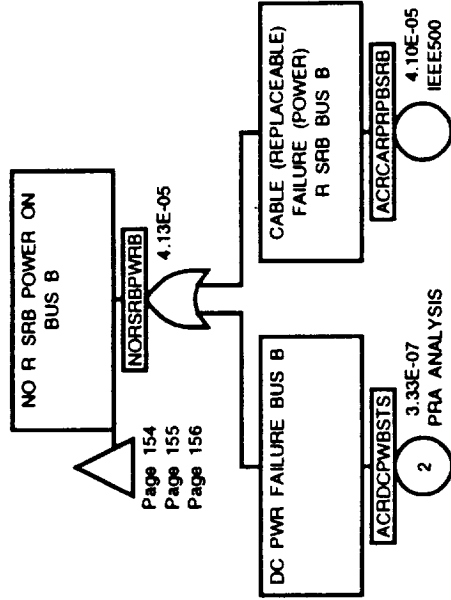


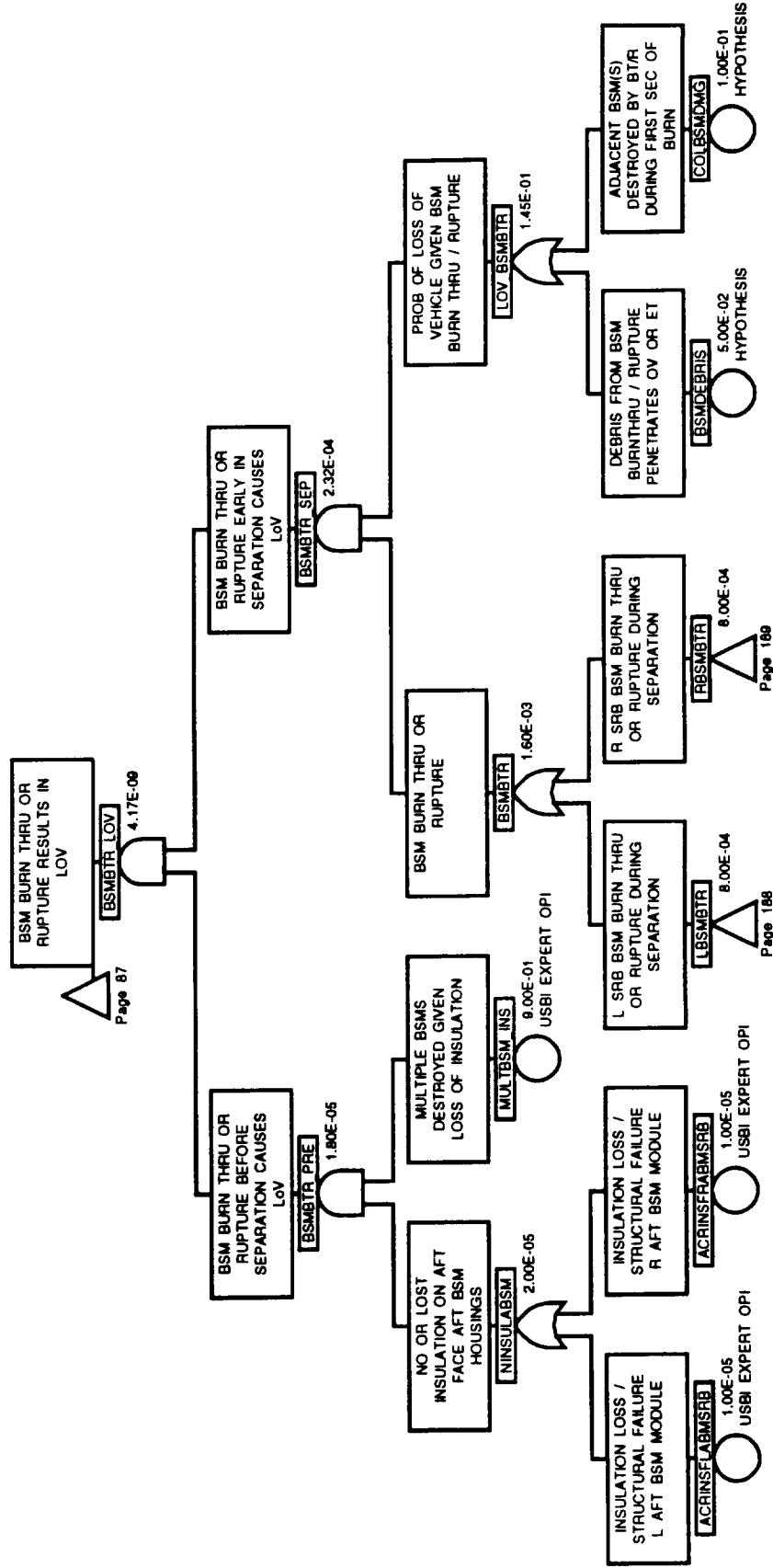


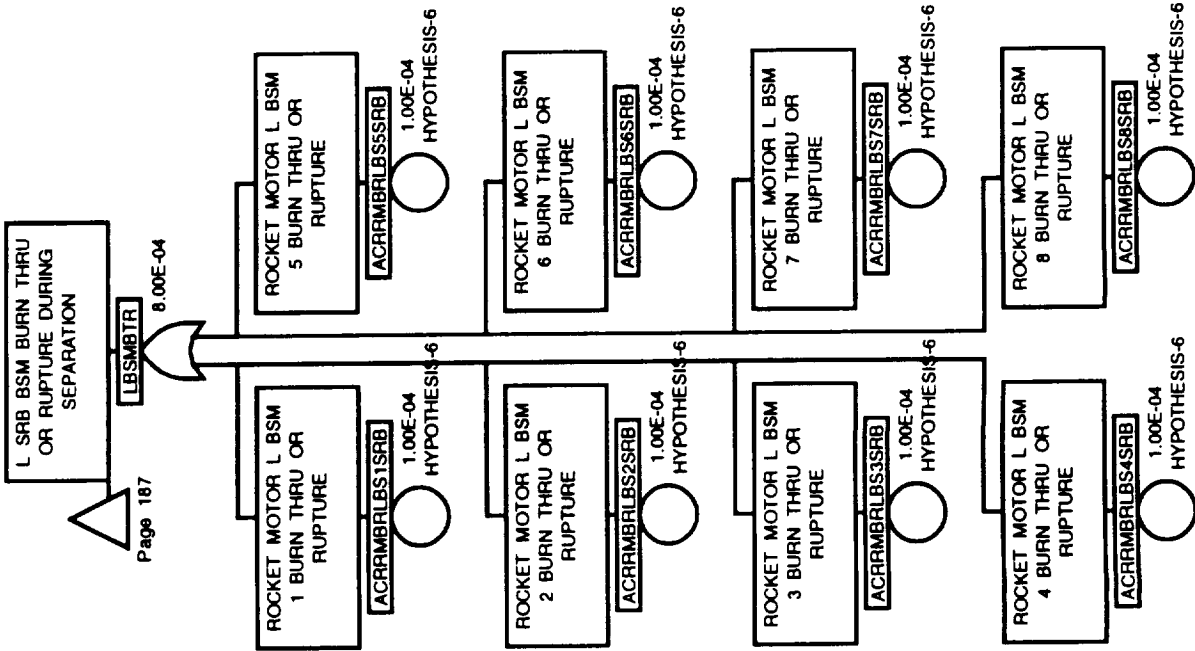


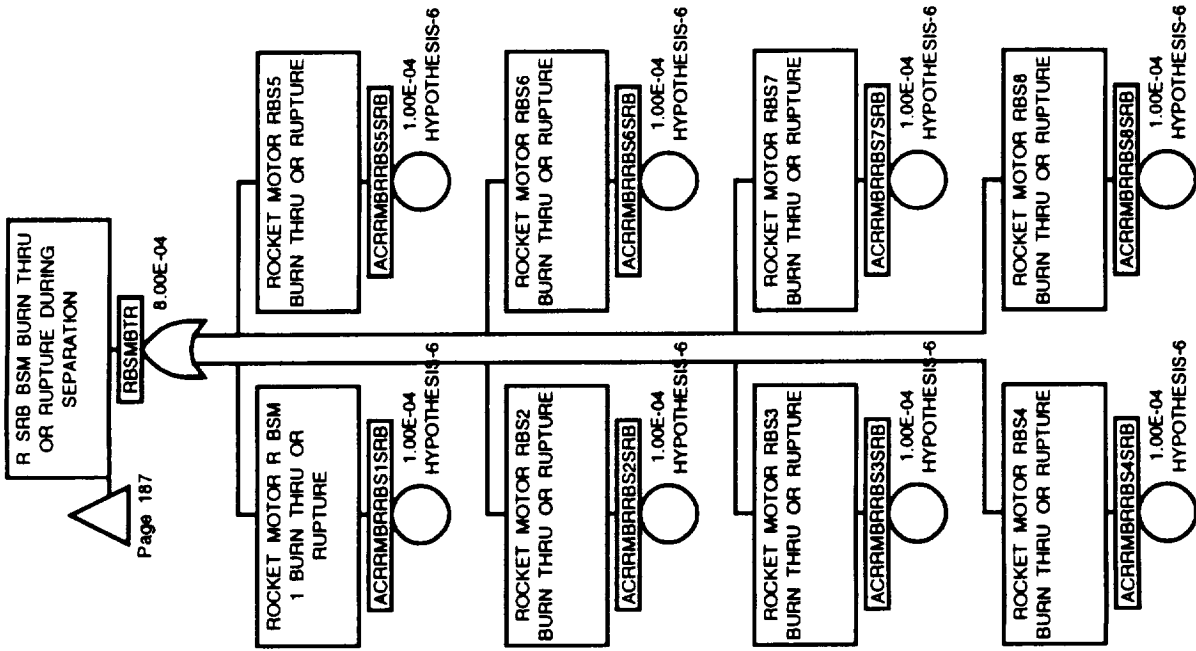
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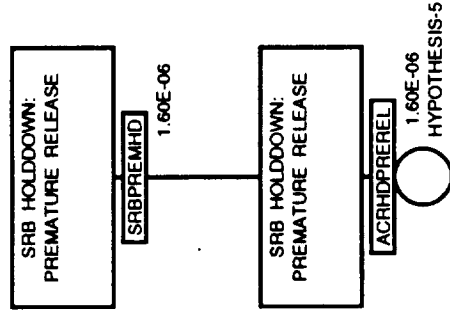




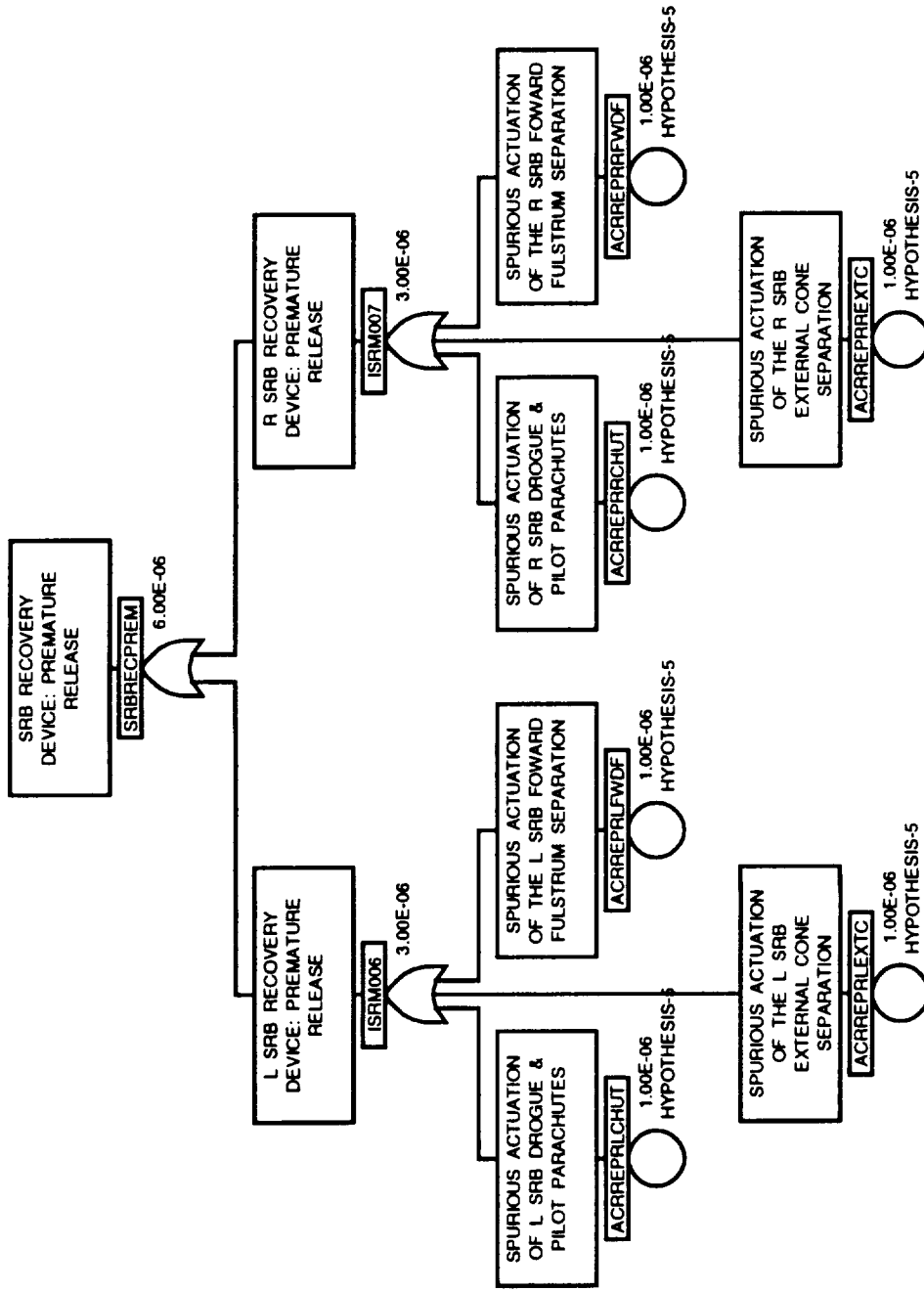


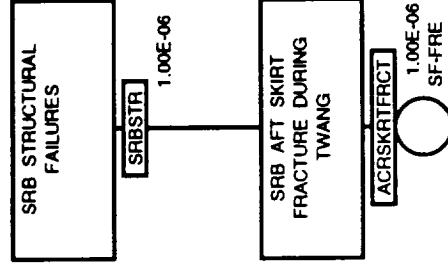


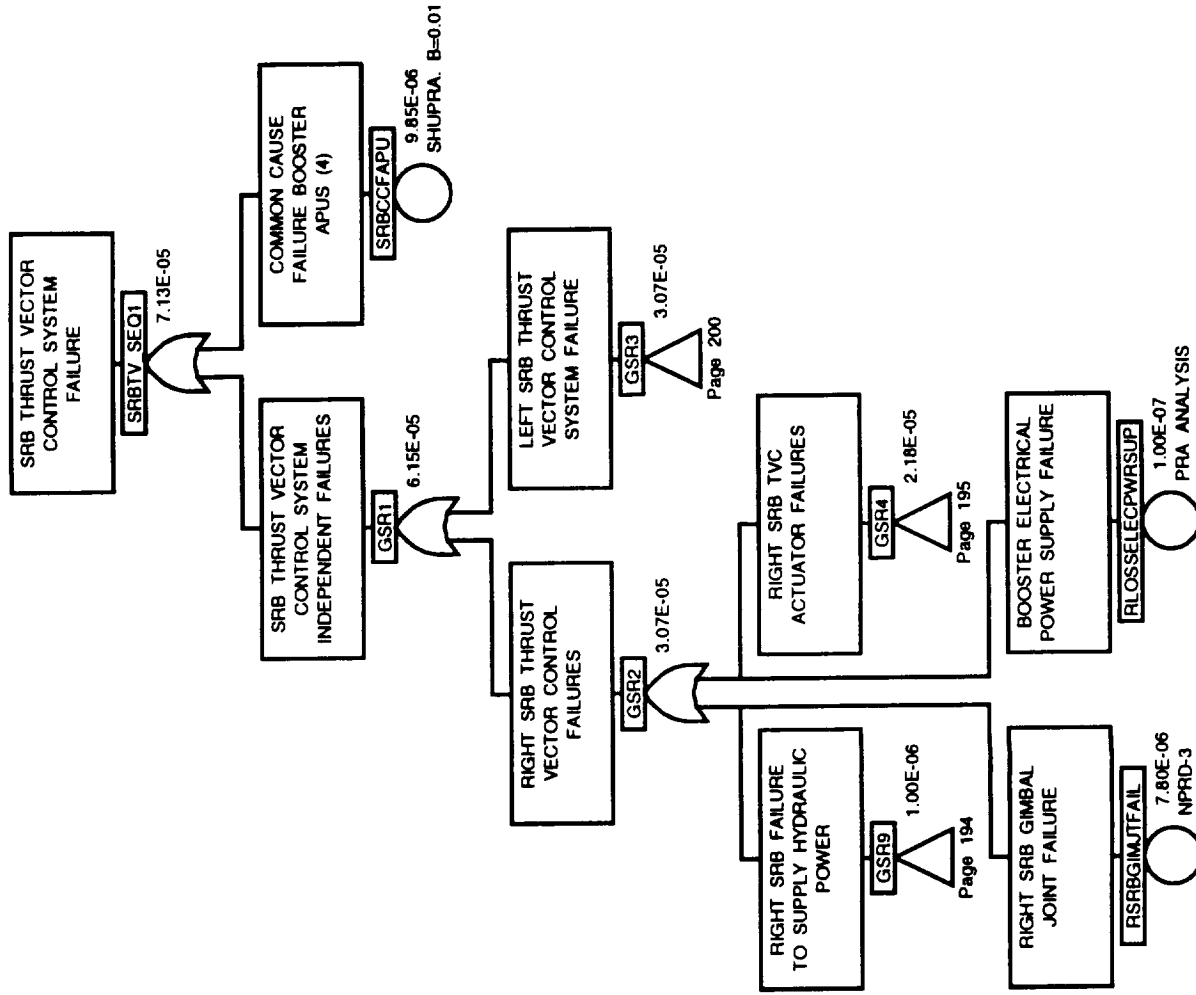


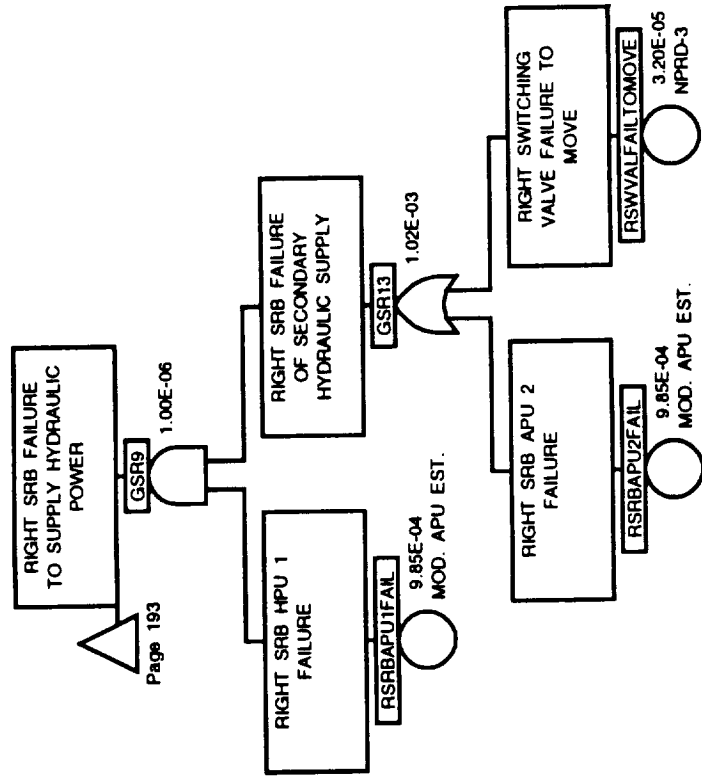




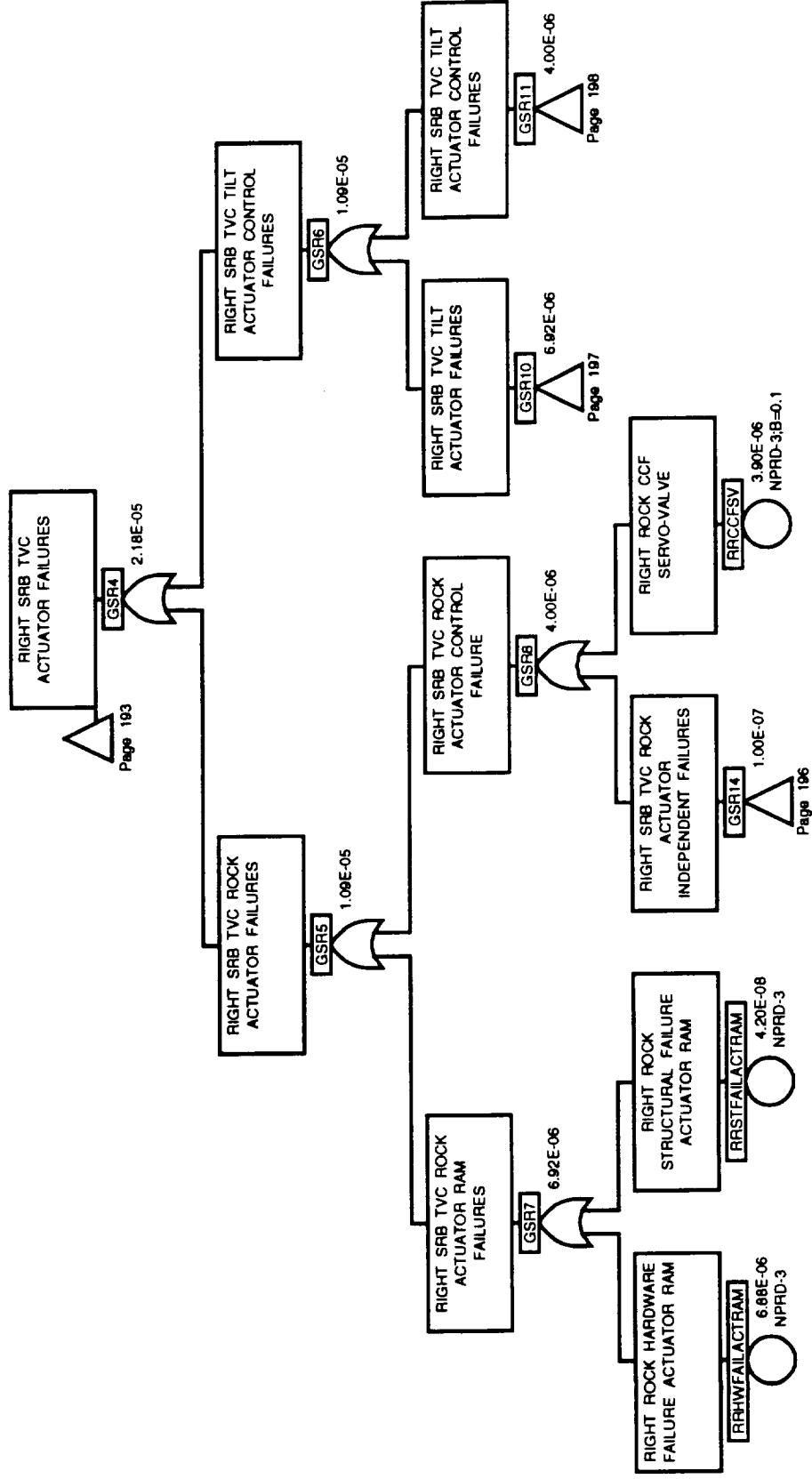


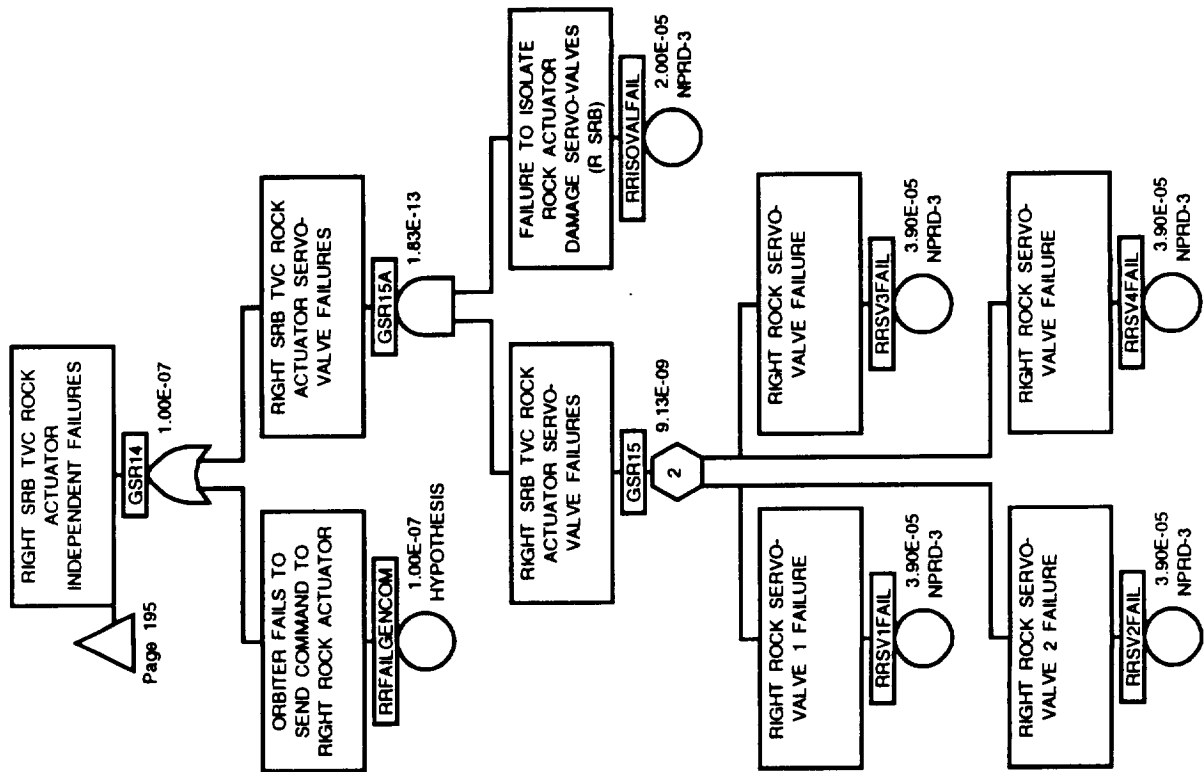




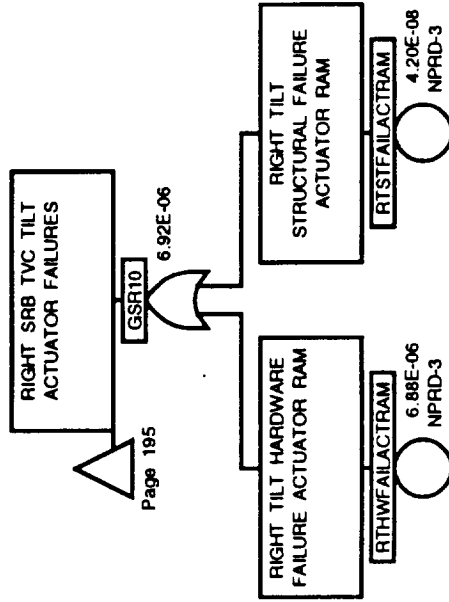


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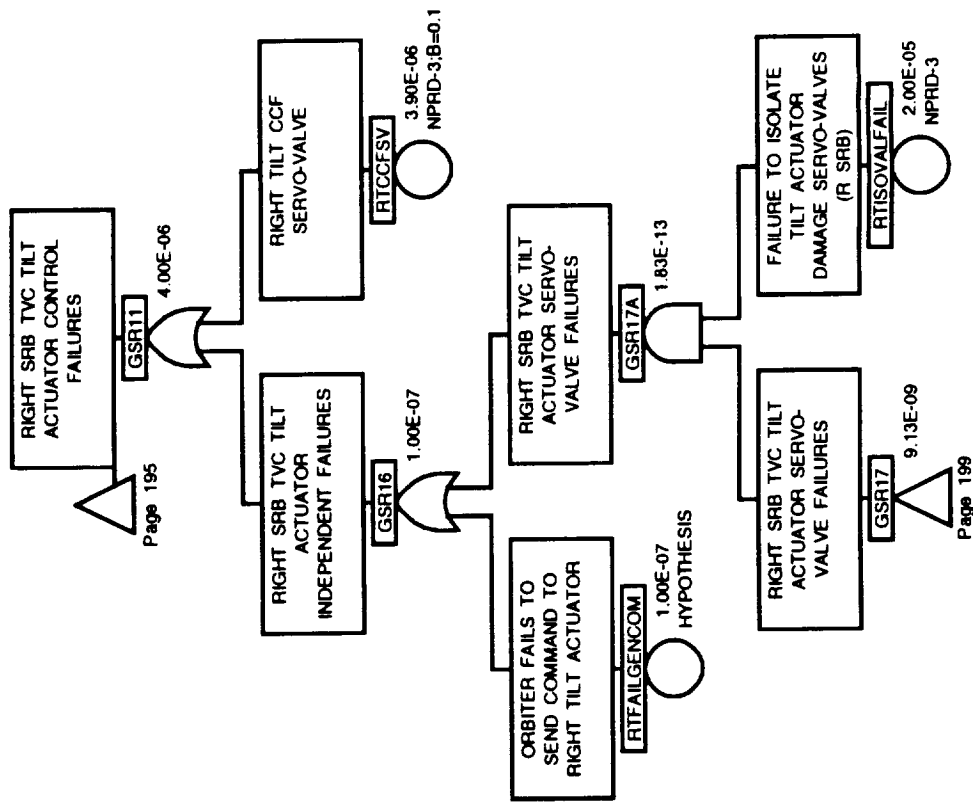




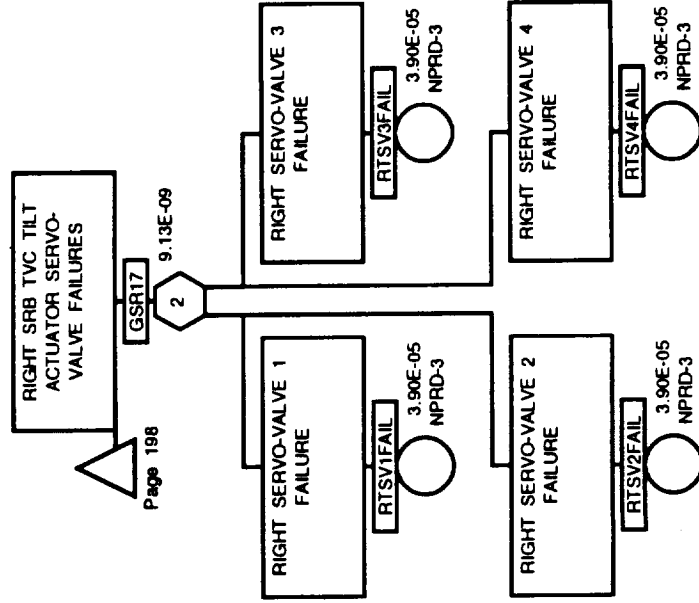
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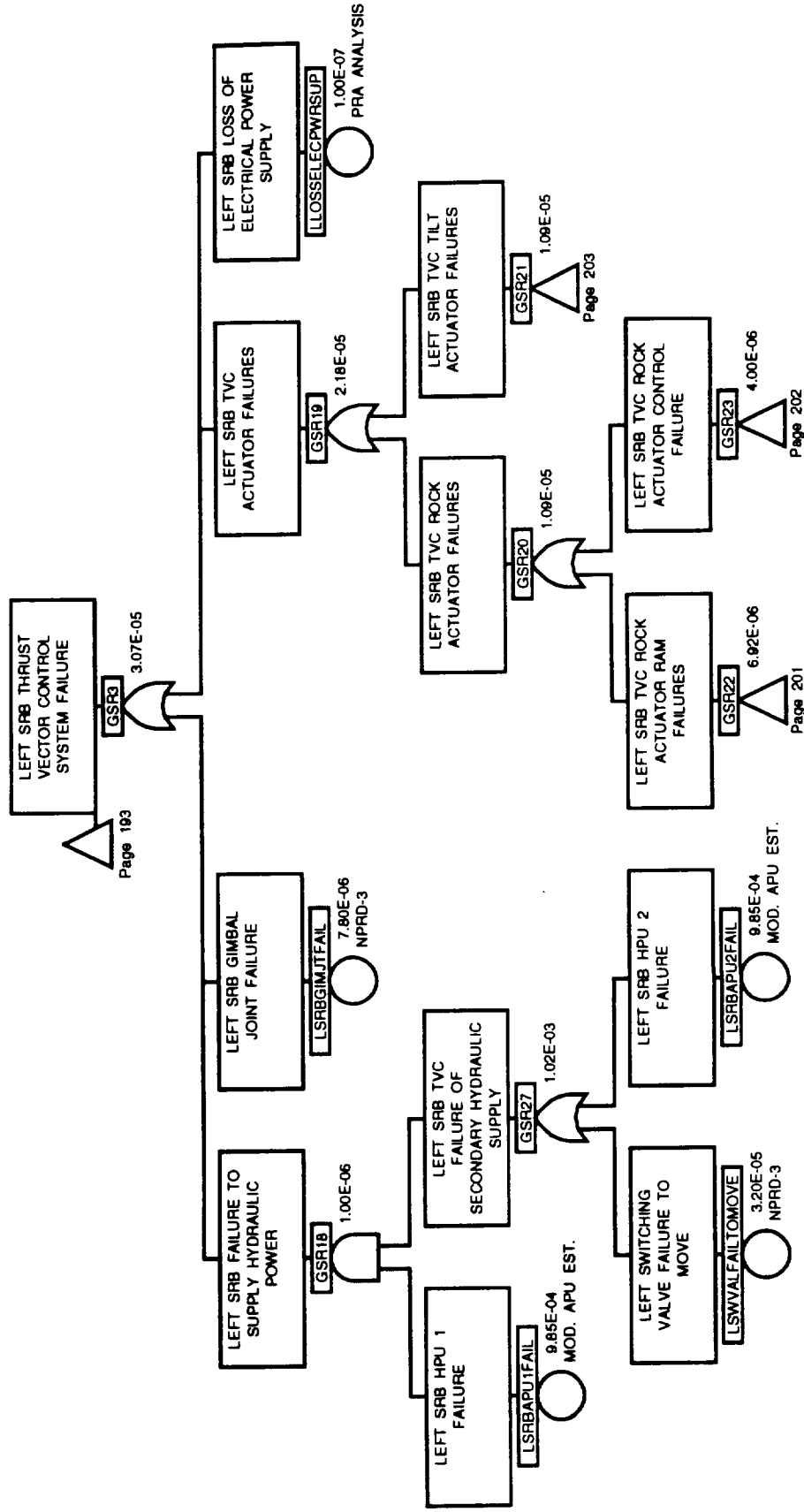
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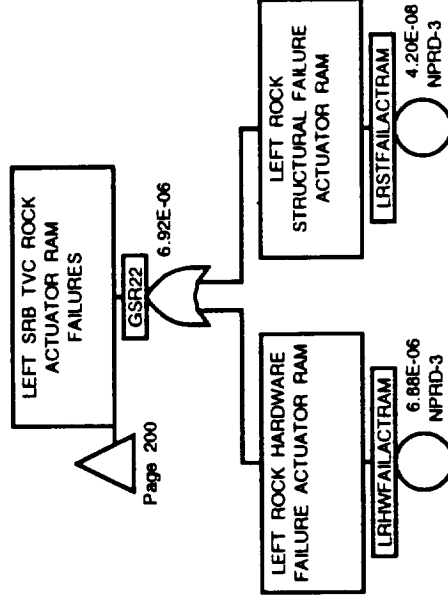




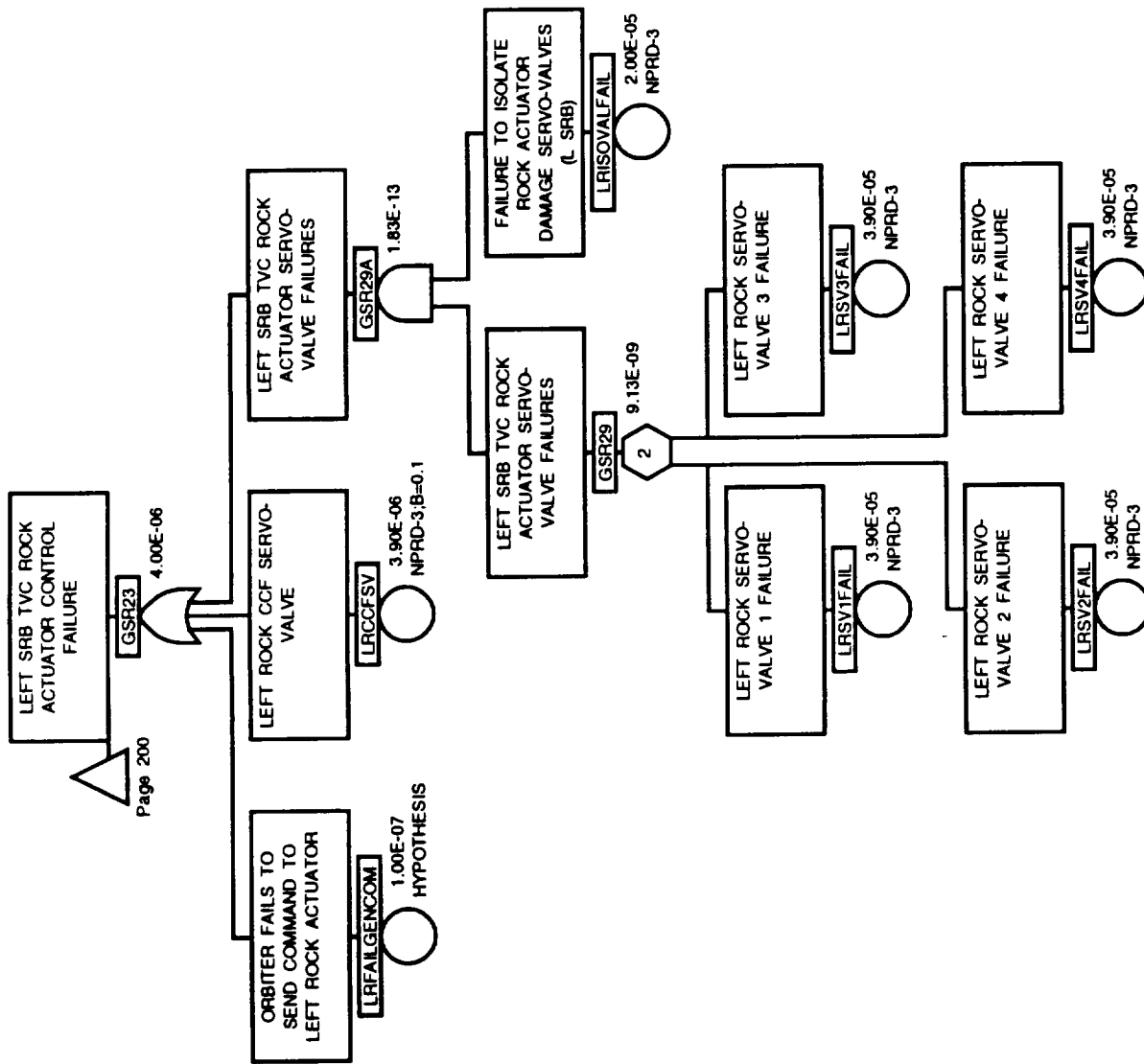


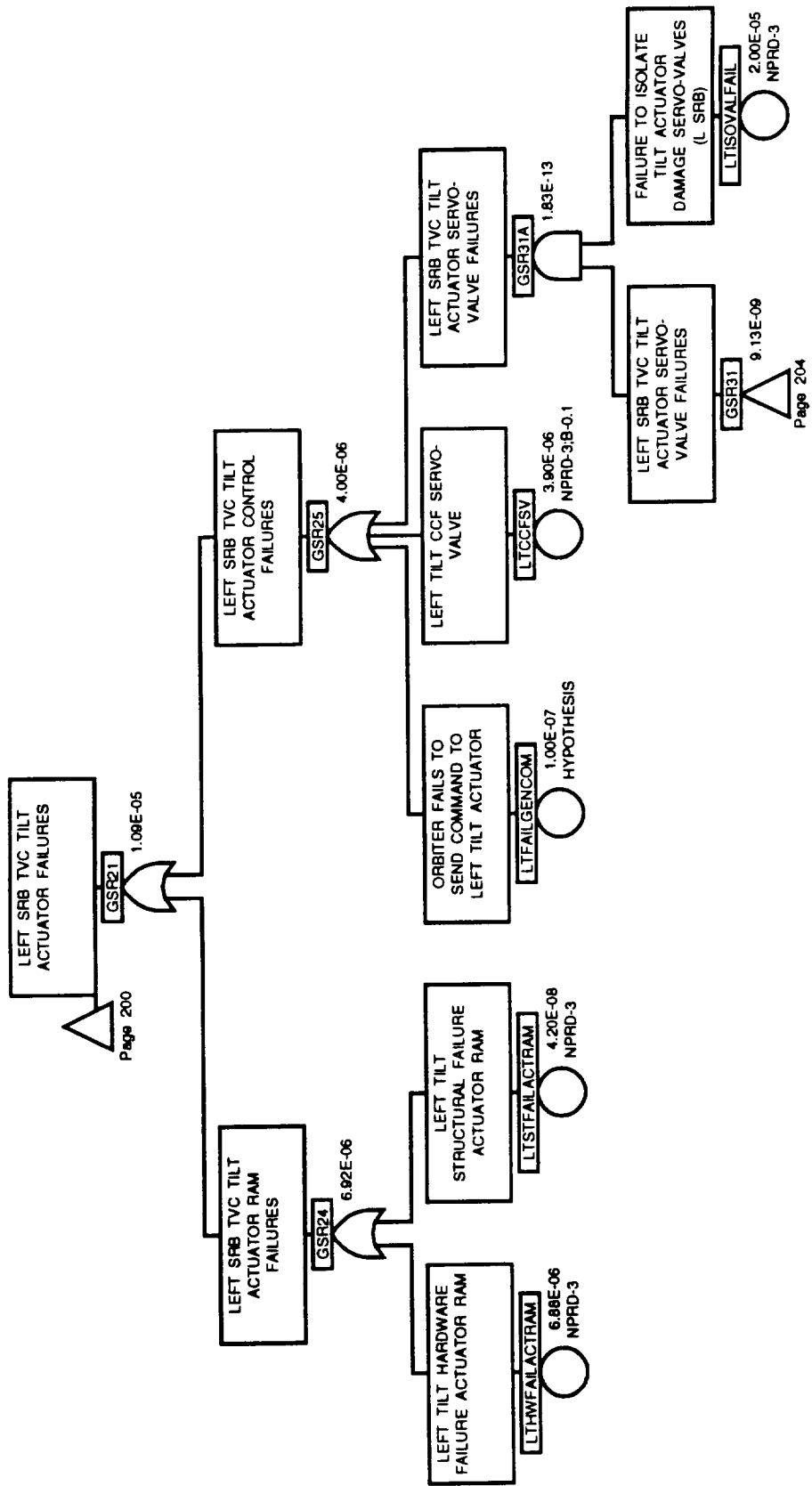
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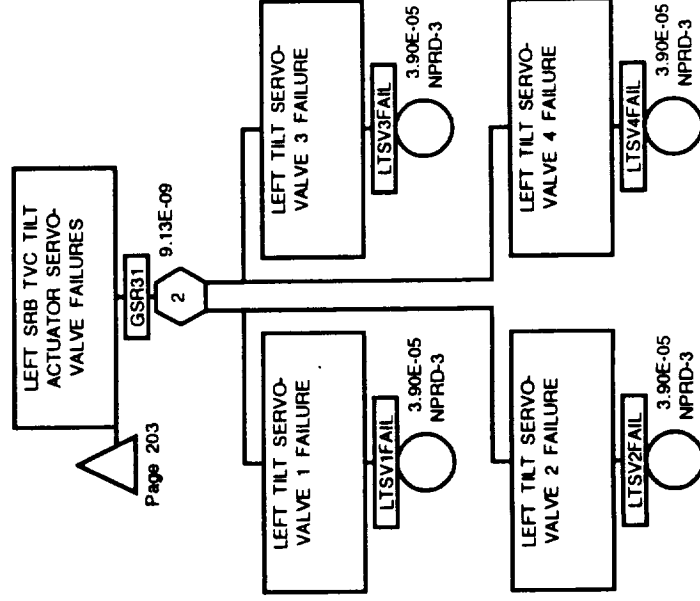




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SRB Component Data

COMPONENT	QTY/FLIGHT	# OF FLIGHTS	GROUND TESTS	TOTAL	FAILURES*
Frangible Nut	8	62	141	637	0
Booster Ctdg (Frangible Nut)	16	62	189	1181	0
NSI Pressure Cartridge	20	62	271	1511	0
CDF Manifold	18	62	292	1408	0
CDF Assembly**	56	62	838	4310	0
CDF Initiator	32	62	409	2393	***1
Booster Separation Bolt	16	62	104	1096	0
Forward Separation Bolt	2	62	77	201	0
Aft Separation Bolt	8	62	141	637	0
* Only failures which could lead to loss of vehicle are included.					
** Similar designs (at E.T., Inc.) have had over 75,000 successful firings with no failures					
*** Failure successfully screened by LAT, lot rejected at vendors's facility (not counted as flight failure)					
Additional CDF related information obtained from Explosive Technologies: 19,460 test firings with no failures					
CDF Failure Probability Estimate $> 1 / (3 * (19460 + 2 * (4310) + 1408 + 2393)) = 1.05E-5$					



# RSRM Joint Leak Data

## NOZZLE-TO-CASE JOINTS

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
Polysulfide	Flights 1-37,39,41	78			5
	Static Tests	9			1
	Totals:	87			6
Wiper O-Ring	Flights 1-37,39,41	6	78		
	Static Tests	1	9		
	NUES/TPTA,QM6	1			
	Totals:	8	87	0.2	1
Vent Port Plug Primary O-Ring (nozzle and case combined)  (47 motors counted as 23 tests)	Flights 1-37,39,41		234		
	Static Tests		30		
	TPTA 1.3,2.1,2.2	7			
	NUES/JES 3C	4			1
	SPC (70lb Motor)	23	23		
	Totals:	34	287	0.9	1
Vent Port Plug Second O-Ring (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1,2.2	3			
	NUES/JES 3C	3			
	Totals:	6	352	0.9	0
Closure Vent Port Plug (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1	2			
	NUES/JES 3C	2			
	Totals:	4	352	0.6	0
Primary O-Ring	Flights 1-37,39,41		78		
	Static Tests		9		
	TPTA 1.2,2.1	2			
	NUES 3A,PVM1	2			
	Totals:	4	87	0.6	0
Leak Check Port Plug (case/nozzle/igniter combined)	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0
Stat-O-Seal	Case	100	9000		
	Igniter		5040		
	Nozzle	100	6776		
	Totals:	200	20816	0.9	0
Secondary O-Ring	Flights 1-37,39,41		78		
	Static Tests		10		
	TPTA 1.3	1			
	NUES 3B	1			
	Totals:	2	88	0.9	0

# RSRM Joint Leak Data

## IGNITER INTERNAL JOINTS

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
S&A Primary Gasket	Static Tests	12	12		
	SRM, HPM, RSRM	128	128		
	Totals:	140	140	0.6	0
S&A Secondary Gasket	Static Test		12		
	SRM, HPM, RSRM		128		
	Totals:		140	0.9	0
COMMON CAUSE Leak Check Port Plug (case/nozzle/igniter)					
	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0
OPT Primary O-Ring (3/igniter)	Static Tests	36			
	SRM,HPM,RSRM	384			
	Minuteman	3300			
	Totals:	3720			0
OPT Secondary O-Ring (3/igniter)	TPTA-2.2	3	0		
	JES-3C	3	24		
	TPTA-1.3	3	256		
	Totals:	9	280	0.9	0
COMMON CAUSE Rotor Primary O-Rings	Static Tests	12	12		
	SRM,HPM,RSRM	128	128		
	Totals:	140	140	0.6	0
Rotor Secondary O-Rings	Static Tests	2	12		
	SRM,HPM,RSRM		128		
	Totals:	2	140	0.9	0
COMMON CAUSE SII Primary O-Ring					
	Static Tests	24	24		
	SRM,HPM,RSRM	256	256		
	Totals:	280	280	0.9	0
SII Secondary O-Ring	Static Tests	2	24		
	SRM,HPM,RSRM		256		
	Totals:	2	280	0.9	0

# RSRM Joint Leak Data

## IGNITER-TO-CASE JOINT

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
INNER J-LEG	FSM-3	1			
	RSRM 23,35-37,39,41	12			
	Totals:	13			0
Special Bolt O-Ring (4/igniter)	Static Test	48	48		
	SRM,HPM,RSRM	512	512		
	Totals:	560	560	0.6	0
Outer J-Leg	FSM-3	1			
	RSRM 23,35-37,39,41	12			
	Totals:	13			0
Inner Gasket/Inner Seal	blow-holes (RSRM)	60			
	Static Tests		12		
	SRM,HPM,RSRM		128		
	Totals:	60	140	0.6	0
Inner Gasket/Outer Seal	blow-hole (RSRM)	60			
	Static Tests		12		
	SRM,HPM,RSRM		128		
	Totals:	60	140	0.9	0
Outer Gasket/Inner Seal	blow-holes (RSRM)	60			
	Static Tests		12		
	SRM,HPM,RSRM		128		
	Totals:	60	140	0.6	0
Outer Gasket/Outer Seal	Static Tests				
	SRM,HPM,RSRM		12		
	Totals:		128		
Stat-O-Seals (36/igniter)	Case	100	9000		
	Igniter		5040		
	Nozzle	100	6776		
	Totals:	200	20816	0.9	0
Leak Check Port Plug (case/nozzle/igniter)	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0

RSRM Joint Leak Data

CASE FIELD JOINT

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
J-Seal	Flights 1-37,39,41	234			
	Static Tests	15			
	JES 3A	2			
	TPTA 1.1, 2.1	3			
	Totals:	254			0
Capture Feature O-Ring	Flights 1-37,39,41		234		
	Static Tests		24		
	JES 3B	1	0		
	QM-6	1	2		
	PVM-1	1	1		
	Totals:	3	261	0.6	0
Vent Port Plug Primary O-Ring (nozzle and case combined)  (47 motors counted as 23 tests)	Flights 1-37,39,41				
	Static Tests				
	TPTA 1.3,2.1,2.2	7			
	NUES/JES 3C	4			1
	SPC(70lb Motor)	23	23		
	Totals:	34	287	0.9	1
Vent Port Plug Second O-Ring (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1,2.2	3			
	NUES/JES 3C	3			
	Totals:	6	352	0.9	0
Closure Vent Port Plug (nozzle and case combined)	Flights 1-37,39,41		312		
	Static Tests		40		
	TPTA 1.3,2.1	2			
	NUES/JES 3C	2			
	Totals:	4	352	0.5	0
Primary O-Ring	Flights 1-37,39,41		234		
	Static Tests	1	27		
	TPTA 1.3,2.1,2.2	5			
	JES3B/3C	2			
	Totals:	8	261	0.9	0
Outer Gasket/Outer Seal	Static Tests				
	SRM,HPM,RSRM		12		
	Totals:		128		
Leak Check Prot Plug (case/nozzle/igniter combined)	Flights 1-37,39,41		780		
	static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.5	0
Secondary O-Ring	Flights 1-37,39,41		234		
	Static Tests		27		
	TPTA 2.2	2			
	JES 3C	1			
	Totals:	3	261	0.9	0

# RSRM Joint Leak Data

## NOZZLE JOINT

Joint Component	Source	Hot Firings	Leak Checks	Leak Potentiality Factor	Failures
RTV Backfill	Joint 1	90			5
	Joint 2	18			7
	Joint 3	88			10
	Joint 4	88			10
	Joint 5	88			6
	Totals:	372			38
Primary O-Ring	Flight	24	390		
	Static Tests	14	50		
	Totals:	38	440	0.6	0
Secondary O-Ring	Flight		390		
	Static Tests		50		
	Totals:	0	440	0.9	0
Stat-O-Seals	Case	100	9000		
	Igniter		5040		
	Nozzle	100	6776		
	Totals:	200	20816	0.9	0
Leak Check Port Plug	Flights 1-37,39,41		780		
	Static Tests		100		
	SRM01-51L (fld)	4			
	SRM01-51L (noz)	7			
	Totals:	11	880	0.6	0

B.3. Orbiter Auxiliary Power  
Unit/Hydraulics

## **9.0 DEVELOPMENT OF PROBABILITY DISTRIBUTIONS FOR FAULT TREES**

The development of probability distributions for the fault trees is done using Bayesian updating methods. Prior probability distributions for failure rates are taken from the 1987 APU/HPU study, NPRD-95, IREP, IEEE Std. 500, WASH 1400, Shuttle experience and expert judgment. System level priors for the entire APU/HYD/WSB system (failure to start and failure to run distributions) are developed using component data mostly from the 1987 study. Bayesian updating was done at the system level using data found in the in-flight anomaly list (IFAS), PRACA reports, and Post Flight Mission Safety Evaluation Reports.

Data obtained shows that there have been four APU shutdowns on ascent due to the water spray boiler failing to provide adequate cooling, and a near hydraulic system failure due to a massive hydraulic leak during descent.

Due to the fact that the APU/HYD/WSB systems have redundancy, i.e., they are a two-out-of-three or better system, common cause failures become a concern. The fault trees are evaluated using the Multiple Greek Letter (MGL) method to determine the common cause and independent failure rates.

Section 9.1 describes how the MGL method is used to determine the independent failure rates and common cause failure rates from the generic failure rate for each sequence.

Section 9.2 describes the prior distributions used in the study. Fault trees are included in this section to show how prior distributions are calculated for APU/HYD/WSB failure to start, APU/HYD/WSB failure to run, and APU turbine wheel runaway.

### **9.1 Models/Equations for Fault Tree Basic Events**

#### **9.1.1 List of Basic Events**

Table 9.1-1 is a complete list of the basic events found in the fault trees, and their two letter identification code used throughout the model.

#### **9.1.2 Assumptions**

Several assumptions have been made concerning data input probability distributions. The first is that given a common cause leak, all three APU units leak. The second assumption pertains to the detection/confirmation of the leaks. If all three units leak, and a leak is detected in one unit, then the leaks in all units are assumed to be found. A third assumption concerns the restarts of APU units. All units will have to go through a restart process sometime during the reentry process. Some scenarios have APU hydrazine leaks detected, in which case an APU unit is shutdown during the entry sequence. After an APU unit is shutdown, if another unit fails, then the shutdown unit is restarted. However, in the sequence, only one restart of the shutdown APU is considered. There are several reasons for this simplistic modeling. First, the reentry sequence will not begin until an APU unit is working to perform the flight controls check. Second, leaking APUs are shutdown only when a leak is detected and confirmed, and the probability of a leak being detected is only about one in twenty, so these scenario simplifications will not have a significant impact on the total risk.

Identification	Basic Event
CE	Flight critical equipment damaged given LL or TU
CF	Common cause failure to run
CL	Common cause leak
CO	No containment given turbine overspeed
CS	Common cause failure to start or run
HB	Hub breakup given turbine overspeed
ID	Independent/dependent failure to run (ascent)
IF	Independent failure to run (ascent)
IS	Independent failure to start or run (descent)
LA	Leak detected/confirmed given all three APU units leak
LD	Leak detected/confirmed given that one APU unit leaks
LF	Own leakage induced failure (ascent)
LK	Leak in one APU unit
LL	Large exhaust gas or hydrazine leak
LO	Leakage from another unit induced failure (ascent)
LS	Leakage from other unit induced failure to start or run (descent)
LU	Leak undetected given that one APU unit leaks
LZ	Leak undetected given that all three APU units leak
O1	APU unit okay given that one other APU unit leaks
O3	APU unit okay given that all three APU units leak
OK	APU unit okay
OL	APU unit okay given that it leaks
OS	Own leakage induced failure to start or run (descent)
SI	Structural integrity of aft compartment fails given LL or TU
SR	Successful restart of shutdown APU unit
TU	Turbine overspeed or hub failure at normal speed
UL	Unsuccessful single APU/HYD unit reentry, TAEM and landing

**Table 9.1-1: List of Basic Events and Descriptions**

### **9.1.3 Derivation of Common Cause Failure Equations**

As components fail, it is not always entirely clear which failures are truly independent and which are common cause. In order to estimate the frequency of common cause failures from the total estimated frequency, several methods, such as the Multiple Greek Letter (MGL) or beta factor



methods, are used. In this analysis, the MGL method was used. The labeling of the APU units is as follows: if a single APU unit is leaking hydrazine, then that unit is labeled as unit 1, or if all three APU units are leaking hydrazine, then the unit that is shutdown (if the leaks are detected/confirmed) is labeled as unit 1.

#### **9.1.3.1 One APU Unit Leaks Hydrazine During Reentry, TAEM and Landing (LO State)<sup>(1)</sup>**

##### **Sequence 4**

In this sequence, APU units 1 and 2, or 1 and 3, fail. This is basically a 1 out of 3 system, denoted  $Q(1/3)$ . There are two ways in which independent failures of this type can occur:  $Q_1Q_2$  and  $Q_1Q_3$ . For the common cause failures, there are also two ways that those may occur:  $Q_{12}$  and  $Q_{13}$ . Rewriting those terms in the MGL format using  $Q_1$  for independent failures and  $Q_2$  for common cause failure of two components yields the following equation for system failures:

$$Q(1/3) = 2Q_2 + 2Q_1^2$$

In this form of the MGL method where we are dealing both with common cause failures for two systems and common cause failures for three systems. The MGL method defines two parameters:  $\beta$  and  $\gamma$ . Beta is the ratio of two and three unit common cause failures of each unit to all failures for each unit. Gamma is the ratio of three unit common cause failures to two and three unit common cause failures. For each unit, beta is thus:

$$\beta = \frac{2Q_2 + Q_3}{Q_1 + 2Q_2 + Q_3}$$

and gamma is:

$$\gamma = \frac{Q_3}{2Q_2 + Q_3}$$

Omitting the algebra, the single system and common cause for two system failures can be written as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

Since  $Q$  represents the failures due to start or run failures, it should be rewritten as:

$$Q = q_s + \lambda t$$

<sup>(1)</sup> The LO descent initiating event state is equivalent to the IL0 ascent end state.

where  $q_s$  is the failure to start probability, and  $\lambda t$  is the probability of a failure during the run time.<sup>(2,3)</sup> If we substitute into  $Q(1/3)$  for  $Q_1$ ,  $Q_2$  and  $Q$ , then the equation for failures becomes:

$$Q(1/3) = [(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t] + 2[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

This is the total failure rate. We now need to relate the above equation to the fault tree basic events. The first term in the above equation is the common cause term, and does not need to be changed. The second term in the above equation needs to represent the independent failures as depicted in the fault tree. For example, if we examine the fault tree for the sequence 4 LOV with the initiating L0 state (one APU unit is leaking), then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(1, 2 \text{ or } 1, 3) = P(1 \text{ IF})P(2 \text{ IF}) + P(1 \text{ IF})P(3 \text{ IF}) + P(\text{CCF}) + P(1 \text{ IF})P(3 \text{ LO}) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the fourth and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(\text{CCF}) = [(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t]$$

$$2P(\text{IF})^2 = 2[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

If we reduce the independent failure rate probability, we get:

$$P(\text{IF}) = \sqrt{[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2}$$

which reduces to:

$$P(\text{IF}) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

## Sequence 6

In this sequence, both APU units 2 and 3 have failed. This is basically a 1 out of 3 system, denoted  $Q(1/3)$ . There is one way in which independent failures of this type can occur:  $Q_2 Q_3$ . For the common cause failures, there is also only one way that this may occur:  $Q_{23}$ . Rewriting those terms in the MGL format using  $Q_1$  for independent failures and  $Q_2$  for common cause failure of two components yields the following equation for system failures:

$$Q(1/3) = Q_1^2 + Q_2$$

As before, the single and common cause (for two systems) factors are defined as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

<sup>(2)</sup> In this analysis the  $\beta_s$  and  $\beta_r$  are given the same numerical value, and  $\gamma_s$  and  $\gamma_r$  are given the same numerical value.

<sup>(3)</sup> For ascent sequences,  $\lambda t$  is the probability of basic event ID (or IF) in Table 9.3-1. For descent sequences  $q_s + \lambda t$  is the probability of a basic event IS in Table 9.3-1.

Since  $Q$  represents the failures due to start or run failures, it should be rewritten as:

$$Q = q_s + \lambda t$$

where  $q_s$  is the failure to start probability, and  $\lambda t$  is the probability of a failure during the run time. If we substitute into  $Q(1/3)$  for  $Q_1$ ,  $Q_2$  and  $Q$ , then the equation for failures becomes:

$$Q(1/3) = \frac{1}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t] + [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

As before, we can see that the first term represents the common cause failure rate, and the second term represents the independent failure rate. If we examine the fault tree for the sequence 6 LOV with the initiating L0 state, then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(2, 3) = P(2 \text{ IF})P(3 \text{ IF}) + P(\text{CCF}) + P(2 \text{ IF})P(3 \text{ LO}) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the third and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(\text{CCF}) = \frac{1}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t]$$

$$P(\text{IF})^2 = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

If we reduce the independent failure rate probability, we get:

$$P(\text{IF}) = \sqrt{[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2}$$

which reduces to:

$$P(\text{IF}) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

This is the same expressions as determined in the Sequence 4 LOV.

### Sequence 7

In this sequence, since there is no leak detection, no distinction is made between which units fail and which do not. All three units fail, even though 1 out of 3 is needed for survival, so this is denoted  $Q(1/3)$ . There is one way in which independent failures of this type can occur:  $Q_1 Q_2 Q_3$ . For the common cause failures, there is also only one common cause for all three,  $Q_{123}$ . There are three combinations of pairs of common cause failures for two systems, i.e.,  $Q_{12}$  and  $Q_{23}$  is one pair, and three combinations of an independent failure and a common cause failure for two systems, i.e.,  $Q_1$  and  $Q_{23}$ , and one pair. Rewriting those terms in the MGL format using  $Q_1$  for independent failures,  $Q_2$  for common cause failures of two components and  $Q_3$  for common cause failures of three components yields the following equation for system failures:

$$Q(1/3) = Q_3 + 3Q_1 Q_2 + 3Q_2^2 + Q_1^3$$

Omitting the algebra, the failures can be written as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

$$Q_3 = \gamma\beta Q$$

Substituting for  $Q_1$ ,  $Q_2$  and  $Q_3$  into  $Q(1/3)$  yields:

$$Q(1/3) = \gamma\beta Q + \frac{3}{2}(1 - \beta)\beta(1 - \gamma)Q^2 + \frac{1}{2}\frac{(1 - \gamma)}{(1 - \beta)}\beta\left[\frac{3}{2}(1 - \beta)\beta(1 - \gamma)Q^2\right] + (1 - \beta)^3 Q^3$$

If we examine the above expression, we see that there are four terms, which from left to right we'll call one, two, three and four. The third term is negligible because

$$\frac{1}{2}\frac{(1 - \gamma)}{(1 - \beta)}\beta \ll 1$$

and is, furthermore, much less than the second term. As before:

$$Q = q_s + \lambda t$$

where  $q_s$  is the failure to start probability, and  $\lambda t$  is the probability of a failure during the run time. Substitute  $Q$  into  $Q(1/3)$  with the simplifying assumption yields:

$$Q(1/3) = (\gamma_s\beta_s q_s + \gamma_r\beta_r \lambda t) + \frac{3}{2}\{[(1 - \beta_s)\beta_s(1 - \gamma_s)q_s^2] + [(1 - \beta_s)\beta_r(1 - \gamma_r)q_s \lambda t] + [(1 - \beta_r)\beta_s(1 - \gamma_s)q_s \lambda t] + [(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2]\} + [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^3$$

As before, we can see that the first term represents the common cause failure rate, and the second term represents the independent failure rate. If we examine the fault tree for the sequence 7 LOV with the initiating LO state, then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(1, 2, 3) = P(1 \text{ IF})P(2 \text{ IF})P(3 \text{ IF}) + P(\text{CCF}) + P(1 \text{ LO})P(2 \text{ IF})P(3 \text{ IF}) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the third and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(\text{CCF}) = \gamma_s\beta_s q_s + \gamma_r\beta_r \lambda t + \frac{3}{2}\{[(1 - \beta_s)\beta_s(1 - \gamma_s)q_s^2] + [(1 - \beta_s)\beta_r(1 - \gamma_r)q_s \lambda t] + [(1 - \beta_r)\beta_s(1 - \gamma_s)q_s \lambda t] + [(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2]\}$$

$$P(\text{IF}) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

### Sequence 11

In this sequence, two APU units fail, and since the event is undetected, no distinction is made as to which two have failed. System failures are thus defined as:

$$Q(1/3) = 3Q_2 + 3Q_1^2$$

As before, the failures are defined as:

$$Q_1 = (1 - \beta)Q$$

$$Q_2 = \frac{1}{2}(1 - \gamma)\beta Q$$

Since Q represents the failures due to start and run failures, it should be rewritten as:

$$Q = q_s + \lambda t$$

where  $q_s$  is the failure to start probability, and  $\lambda t$  is the probability of a failure during the run time. If we substitute into  $Q(1/3)$  for  $Q_1$ ,  $Q_2$  and  $Q$ , then the equation for failures becomes:

$$Q(1/3) = \frac{3}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t] + 3[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

As before, we can see that the first term represents the common cause failure rate, and the second term represents the independent failure rate. If we examine the fault tree for the sequence 11 LOV with the initiating L0 state, then by analysis at the basic event level, the probability of the component failures in the sequence can be expressed as:

$$P(2 \text{ fail}) = P(1 \text{ IF})P(2 \text{ IF}) + P(1 \text{ IF})P(3 \text{ IF}) + P(2 \text{ IF})P(3 \text{ IF}) + P(\text{CCF}) + P(2 \text{ IF})P(3 \text{ LO}) + \dots$$

where IF, CCF and LO were defined previously as independent failures, common cause failure, and own leak induced failure. Since we are only concerned about independent and common cause failures, we will ignore the fifth and remaining terms as being inapplicable to the determination of the common cause failure rate and the independent failure rate. If the independent failure rates are the same for all APU units, then the previous two expressions can be combined as:

$$P(\text{CCF}) = \frac{3}{2}[(1 - \gamma_s)\beta_s q_s + (1 - \gamma_r)\beta_r \lambda t]$$

$$3P(\text{IF})^2 = 3[(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]^2$$

If we reduce the independent failure rate probability, we get:

$$P(\text{IF}) = [(1 - \beta_s)q_s + (1 - \beta_r)\lambda t]$$

### Sequence 12

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for IL0 sequence 7.

### Sequence 16

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

This sequence also models the remaining two APU units developing a common cause leak, given the initial leak in one unit.<sup>(1)</sup> As described for OK sequence 21, the formula for common cause leakage is given by:

$$P(CCF) = \gamma_L \beta_L \lambda_{L,t} + \frac{3}{2}(1 - \beta_L) \beta_L (1 - \gamma_L) \lambda_L^2 t^2$$

Here,  $\lambda_{L,t}$  is the probability of the initial state, L0. So, since the conditional probability of developing the common cause leak is multiplied against the initial state probability, and given that the first term in the equation is by far the dominant factor, the common cause conditional probability should be entered as:

$$P(CCF) = \gamma_L \beta_L$$

### **Sequence 18**

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6. The equation for a common cause leak is the same as that described for L0 sequence 16.

### **Sequence 19**

This sequence occurs when all APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for a common cause leak is the same as that described for L0 sequence 16.

### **Sequence 23**

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11. The equation for a common cause leak is the same as that described for L0 sequence 16.

### **Sequence 24**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for a common cause leak is the same as that described for L0 sequence 16.

## **9.1.3.2 All Three APU Units Leak Hydrazine During Reentry, TAEM and Landing (LT State)**

### **Sequence 4**

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

<sup>(1)</sup>  $\lambda_L$  is the frequency of event LK in Table 9.3-1.

### **Sequence 6**

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6.

### **Sequence 7**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7.

### **Sequence 11**

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11.

### **Sequence 12**

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 12.

### **9.1.3.3 All Three APU Units are OK During Reentry, TAEM and Landing (OK State)**

### **Sequence 4**

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11.

### **Sequence 5**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7.

### **Sequence 9**

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

This sequence also involves a common cause treatment of APU leaks. Here, we are modeling any one of the three APUs develops a leak, which is basically a 1 out of 3 system, denoted as  $Q(1/3)$ . There are three ways in which independent failures of this type can occur:  $Q_1$ ,  $Q_2$ , or  $Q_3$ . Rewriting those terms in the MGL format using  $Q_1$  for the independent failures yields the following equation for system failures:

$$Q(1/3) = 3Q_1$$

As before, the failures are identified as:

$$Q_1 = (1 - \beta)Q$$

Since  $Q$  in this case represents leakage failures over the exposure time,  $Q$  is replaced by:

$$Q = \lambda_L t$$

where  $\lambda_L$  is the leakage failure rate and  $t$  is the exposure time of the system. If we substitute into  $Q(1/3)$  for  $Q1$ , then the equation for failures becomes:

$$Q(1/3) = 3(1 - \beta_L)\lambda_L t$$

Since independent failures are the only contributors in this equation, we get:

$$P(IF) = 3(1 - \beta_L)\lambda_L t$$

### **Sequence 11**

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6. The equation for independent leaks is the same as that described for OK sequence 9.

### **Sequence 12**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for independent leaks is the same as that described for OK sequence 9.

### **Sequence 16**

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11. The equation for independent leaks is the same as that described for OK sequence 9.

### **Sequence 17**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equation for independent leaks is the same as that described for OK sequence 9.

### **Sequence 21**

This sequence occurs when APU/HYD systems 1 and 2 or 1 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 4.

This sequence also involves a common cause treatment of APU leaks. Here, we are modeling all three APUs develop leaks. The equations for independent and common cause failures are similar to those described for L0 sequence 7, but with  $Q$  defined differently as in OK sequence 9. Omitting the algebra, the new independent and common cause failure rates can be determined by the following equations:

$$P(CCF) = \gamma_L \beta_L \lambda_L t + \frac{3}{2}(1 - \beta_L)\beta_L(1 - \gamma_L)\lambda_L^2 t^2$$

$$P(IF) = (1 - \beta_L)\lambda_L t$$



### **Sequence 23**

This sequence occurs when APU/HYD systems 2 and 3 fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 6. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

### **Sequence 24**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

### **Sequence 28**

This sequence occurs when any two out of the three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 11. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

### **Sequence 29**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for L0 sequence 7. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

#### **9.1.3.4 All Three APU Units are OK During Ascent (OK State)**

For the ascent phase, it is assumed that all APU units are already started, otherwise the launch sequence would not have been completed. Hence,  $Q$  is now defined as:

$$Q = \lambda t$$

### **Sequence 4**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are similar to those described for L0 sequence 7, but with  $Q$  defined differently. Omitting the algebra, the new independent and common cause failure rates can be determined by the following equations:

$$P(IF) = (1 - \beta_r)\lambda t$$

$$P(CCF) = \gamma_r \beta_r \lambda t + \frac{3}{2}(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2$$

#### **9.1.3.5 At Least One APU Unit is Leaking Hydrazine During Ascent (LK State)**

### **Sequence 6**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equation for independent leaks is the same as that described for OK sequence 9.

### **Sequence 7**

This sequence occurs when one APU unit has an undetected leaks. The equation for independent leaks is the same as that described for OK sequence 9.

### **Sequence 12**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equation for independent leaks is the same as that described for OK sequence 9.

### **Sequence 16**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

### **Sequence 17**

This sequence occurs when all three APU units have undetected leaks. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

### **Sequence 20**

This sequence occurs when all three APU/HYD systems fail. The equations for independent system failures and common cause failures are the same as those described for OK sequence 4. The equations for independent and common cause leaks are the same as those described for OK sequence 21.

#### **9.1.3.6 MGL Parameters**

The following point estimates are generic over all components and all failure modes. They were developed as part of a recent effort funded by EPRI to completely automate the process of analyzing common cause failures in PRAs. The software is available through Boyer Chu at EPRI. This recent effort was based on previous data development and MGL method development found in EPRI INP 3967 (1985), NUREG/CR-4780 (1988), and NUREG/CR-5801 (1993).

For information on methods and procedures for common cause failure you can refer to NUREG/CR-4780 (1988) and NUREG/CR-5801 (1993).

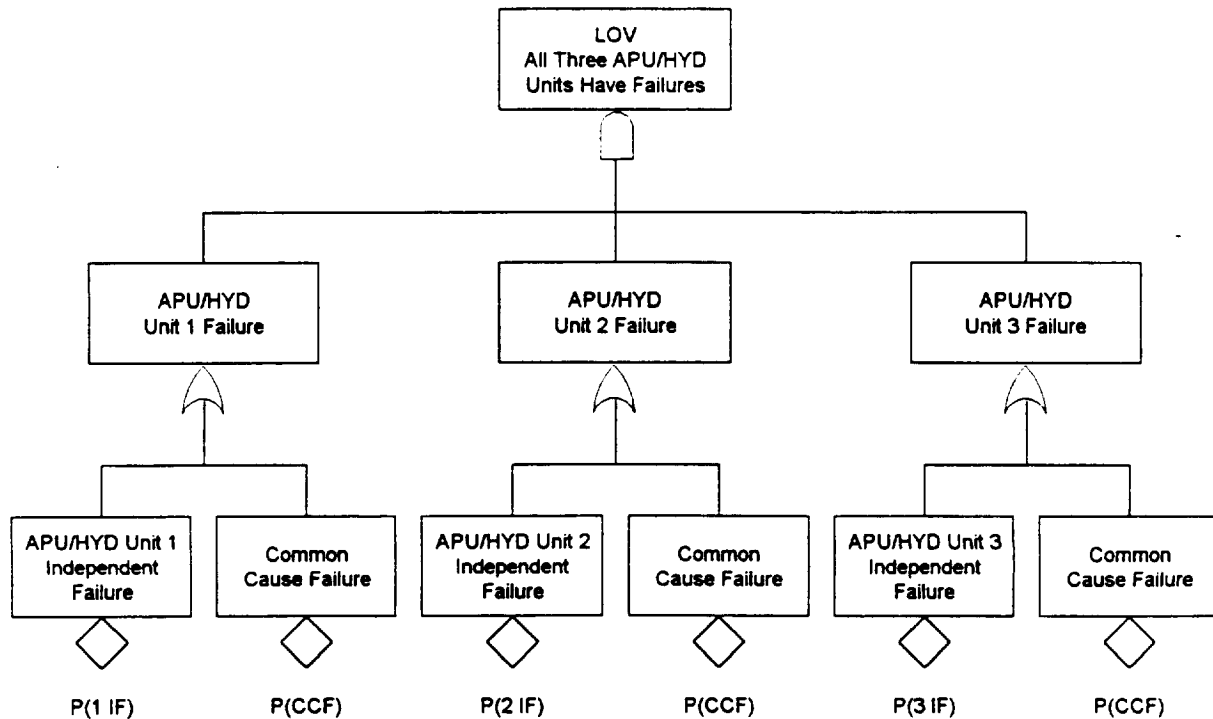
APU component failure rates are generally within the variability range of the generic database from which the Beta and Gamma factors are derived. We believe, therefore, that these are an indication of future failure rates of the APU, and the generic factors apply to the APUs.

We also used the generic data for common cause hydrazine leakage. We have found six leaks (see Section 9.2.2.6). Two of the leaks happened in the same mission (STS-9) for a common cause (carbonization and stress cracking of the injector). The Beta factor could be estimated as 1/3 (3 of 6). However, we know that the manufacturing process has been altered to reduce the likelihood of this cause. There has also been an effort to reduce the exposure of the nozzles to hydrazine between missions. We have used, therefore, a generic Beta factor of 0.1 instead of the

data driven Beta factor of 1/3. We see no justification to apply a Beta factor less than indicated by the generic level.

#### 9.1.4 Equations Graphed in Fault Tree for Illustration

As an example of how the independent failure rate and common cause failure rate equations developed in the previous section are applied, see Figure 9.1-1. In the figure is a simple fault tree that shows the sequence 4 LOV for the ascent phase in which no hydrazine leaks have occurred.



**Figure 9.1-1: Fault Tree for LOV Sequence 4 for an OK State During Ascent**

For the LOV to occur, all three APU/HYD systems must fail. System failures can occur independently, or as common cause failures. These failure rates were determined from the total failure rate using the Multiple Greek Letter method previously described, and are shown under the basic events to which they pertain.

From before, we defined  $P(CCF)$  and  $P(IF)$  as:

$$P(IF) = (1 - \beta_r)\lambda t$$

$$P(CCF) = \gamma_r \beta_r \lambda t + \frac{3}{2}(1 - \beta_r)\beta_r(1 - \gamma_r)\lambda^2 t^2$$

## **9.2 Prior Distribution for Model**

The priors used in the assessment of  $P(IF)$  came from a previous study (McDonnell Douglas Astronautics Company Engineering Services, Space Shuttle Probabilistic Risk Assessment Proof-of-Concept Study Volume III: Auxiliary Power Unit and Hydraulic Power Unit Analysis Report, paper WP-VA88004-03, 1987). As described previously, the priors were updated at the system level with observed Shuttle in flight failures.

### **9.2.1 Inputs Needed to Develop Priors**

The study performed in 1987 was done at a component level; i.e., the failure rates of the components in the system were calculated, and no quantification was done on the system level. This study has defined basic events on the system level in order to have such information for future decision-making. Two prior distributions, the failure to start on demand and the run failure rate, were estimated using the component level data.

The fault tree in Figure 9.2-1 depicts the component failures that most contribute to a system failure to run. These components failure rates were agglomerated to obtain a prior distribution for APU system failure to run (events, ID, IF and IS).

Similarly, Figure 9.2-2 depicts a fault tree in which any of the component failures may cause a failure to start condition. These component failure rates were agglomerated for the start contribution of event IS.

The 1987 study performed a detailed fault tree for turbine overspeed. Quantification of that tree showed that four events dominated the failure probability. These are shown in a simplified fault tree in Figure 9.2-3.

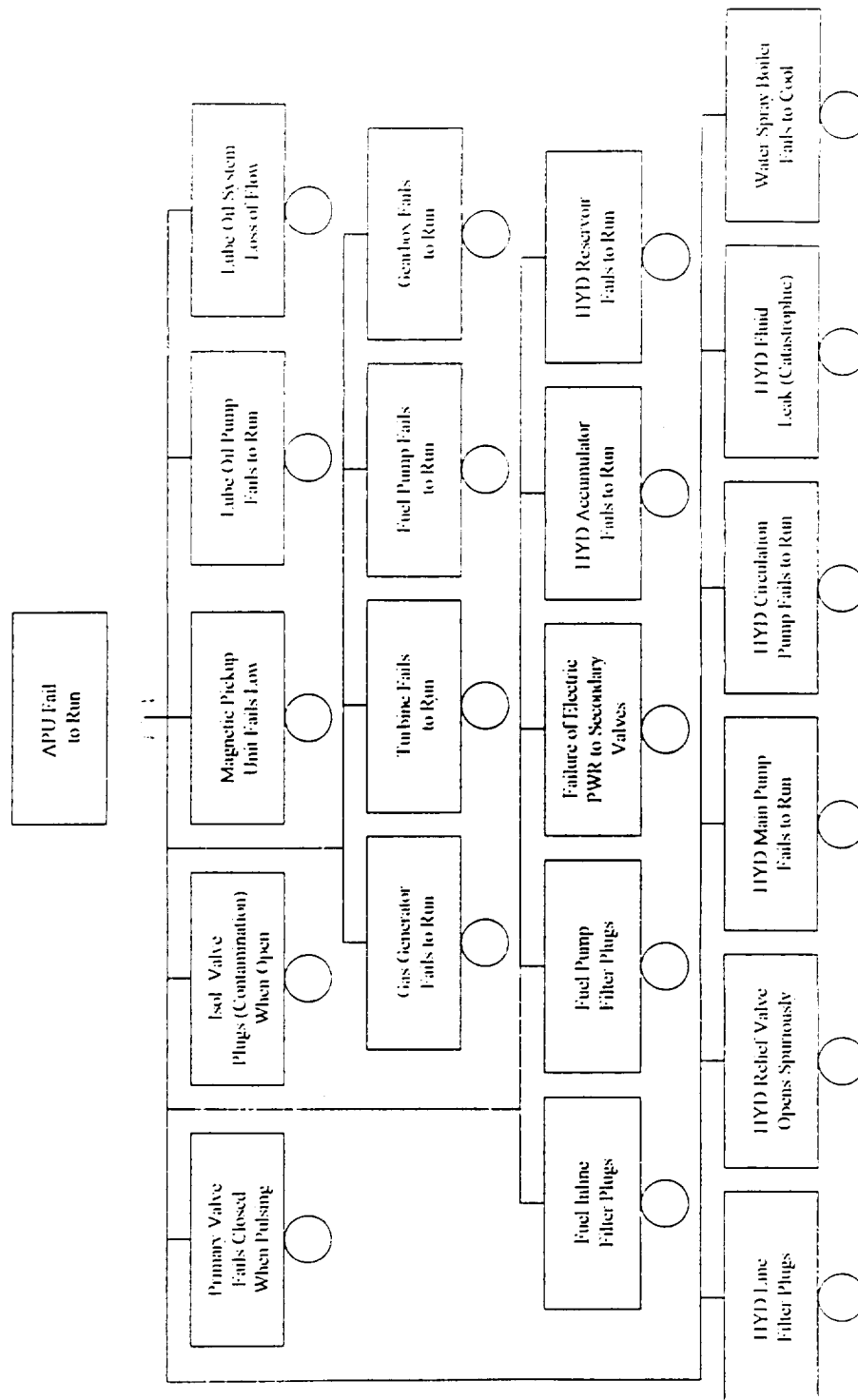


Figure 9.2-1: Fault Tree for APU/HYD/WSB Run Failures

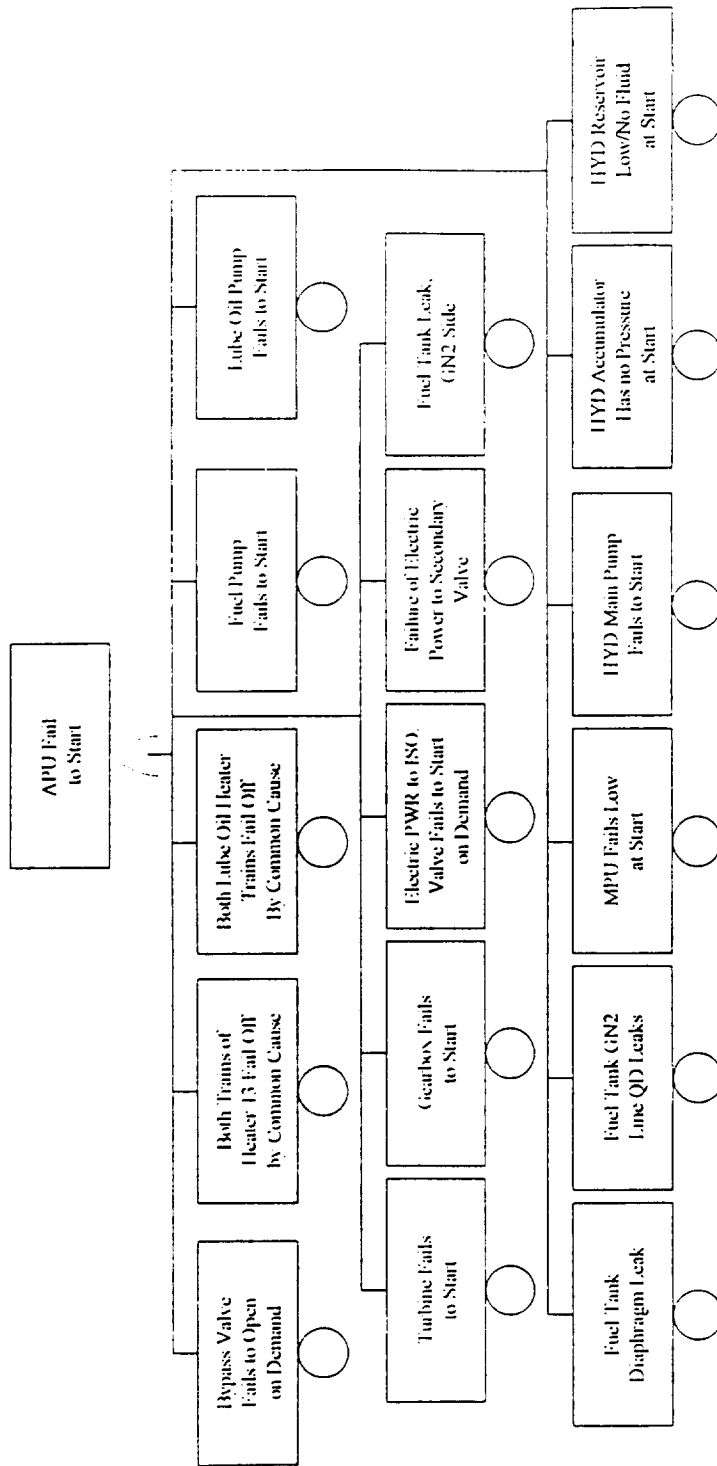
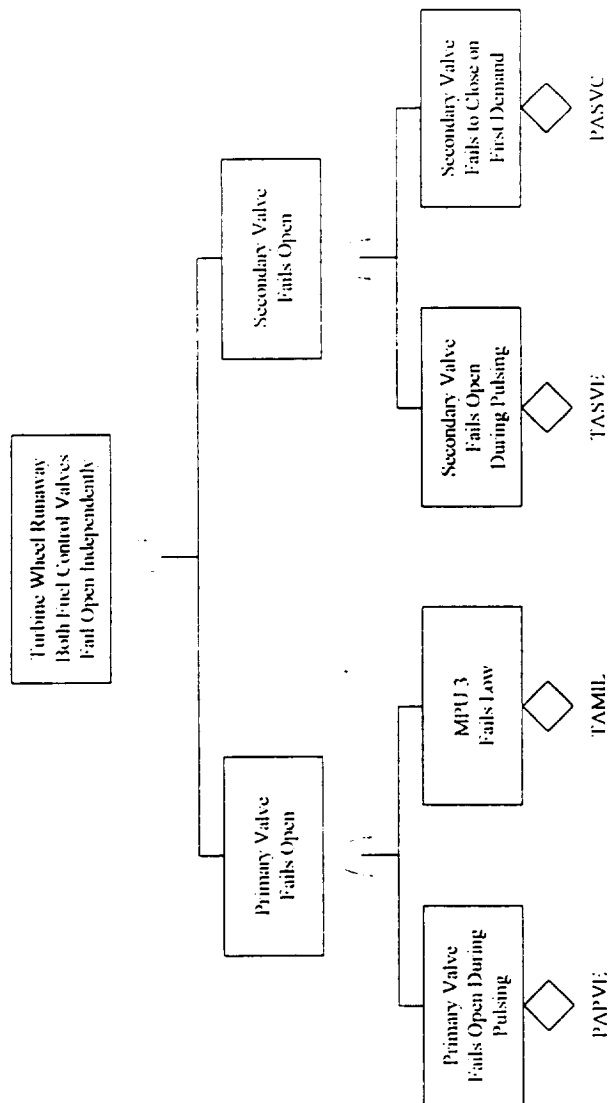


Figure 9.2-2: Fault Tree for APU/HYD/WSB Start Failures



**Figure 9.2-3: Fault Tree for Turbine Overspeed Failures**

## 9.2.2 Output Distributions for Priors

### 9.2.2.1 APU Failure to Run

The first prior calculated is that for an APU to fail to run. Table 9.2-1 lists the component failures frequency distributions that were in the model for APU subsystem run failures.

Failure	Mean-Dist	5th percentile	Median	95th percentile	Ref. (1)
Primary Valve Fails Closed When Pulsing	4.481E-03	3.494E-04	2.404E-03	1.225E-02	1
Isol. Valve Plugs (Contamination) When Open	1.086E-06	4.681E-08	4.343E-07	3.875E-06	1
Magnetic Pickup Unit Fails Low	2.240E-03	1.747E-04	1.202E-03	6.127E-03	1
Fuel Pump Fails To Run	7.685E-05	2.791E-06	2.887E-05	2.797E-04	1
Lube Oil Pump Fails To Run	7.685E-05	2.791E-06	2.887E-05	2.797E-04	1
Lube Oil System Loss Of Flow	2.664E-03	9.334E-05	9.698E-04	9.681E-03	1
Gas Generator Fails To Run	1.436E-04	9.020E-07	2.467E-05	4.429E-04	1
Turbine Fails To Run	6.041E-04	2.722E-05	2.350E-04	1.837E-03	1
Gearbox Fails To Run	2.628E-05	9.323E-07	9.672E-06	9.651E-05	1
Fuel Inline Filter Plugs	7.959E-06	2.799E-07	2.907E-06	2.894E-05	1
Fuel Pump Filter Plugs	2.040E-04	2.722E-06	5.002E-05	6.507E-04	1
Failure Of Electric Pwr To Secondary Valves	4.926E-05	9.231E-07	1.357E-05	1.866E-04	1
HYD Accumulator Fails To Run	2.664E-05	1.0E-06	1.0E-05	1.0E-04	2
HYD Reservoir Fails To Run	2.664E-05	1.0E-06	1.0E-05	1.0E-04	2
HYD Line Filter Plugs	7.840E-06	6.0E-06	7.746E-06	1.0E-05	3
HYD Relief Valve Opens Spuriously	1.212E-05	3.0E-06	9.487E-06	3.0E-05	5
HYD Main Pump Fails To Run	4.040E-05	1.0E-05	3.162E-05	1.0E-04	2,5
HYD Circulation Pump Fails To Run	1.127E-04	7.0E-06	5.292E-05	4.0E-04	2,3
HYD Fluid Leak (Catastrophic)	4.332E-04	5.0E-06	5.0E-05	5.0E-04	1,3,4
Water Spray Boiler Fails To Cool	3.385E-05	1.0E-04	2.236E-05	5.0E-06	2,5
Total Fail To Run/Hr	9.150E-03	3.059E-03	6.956E-03	2.174E-02	

(1)

- |                   |              |   |
|-------------------|--------------|---|
| 1. 1987 APU Study | 4. OREDA     | 6. Shuttle history of 0 failures is 882 demands in a maximum                      |
| 2. NPRD-95        | 5. WASH-1400 | entropy log normal: $882 = (6 \text{ APU Starts/Missions} + 4 \text{ HPU starts}$ |
| 3. IEEE-STD-500   |              | $+ 4 \text{ HPU Hot Fire Tests}) \times 63$                                       |

**Table 9.2-1: Component Failures Leading to APU System Run Failure (Failures/hour)**

In order to calculate the distribution of the sum of these failures, an @Risk Monte Carlo simulation (20,000 trials) in a Lotus 1-2-3 spreadsheet was used. A graphical representation of this distribution can be seen in Figure 9.2-4.



### 9.2.2.2 APU Failure to Start

In Table 9.2-2, various component failures are listed that will lead to a failed-start condition. Once again, to calculate the failed-start distribution based on the sum of the various component failures, an @Risk Monte Carlo simulation (20,000 trials) in a Lotus 1-2-3 spreadsheet was used.

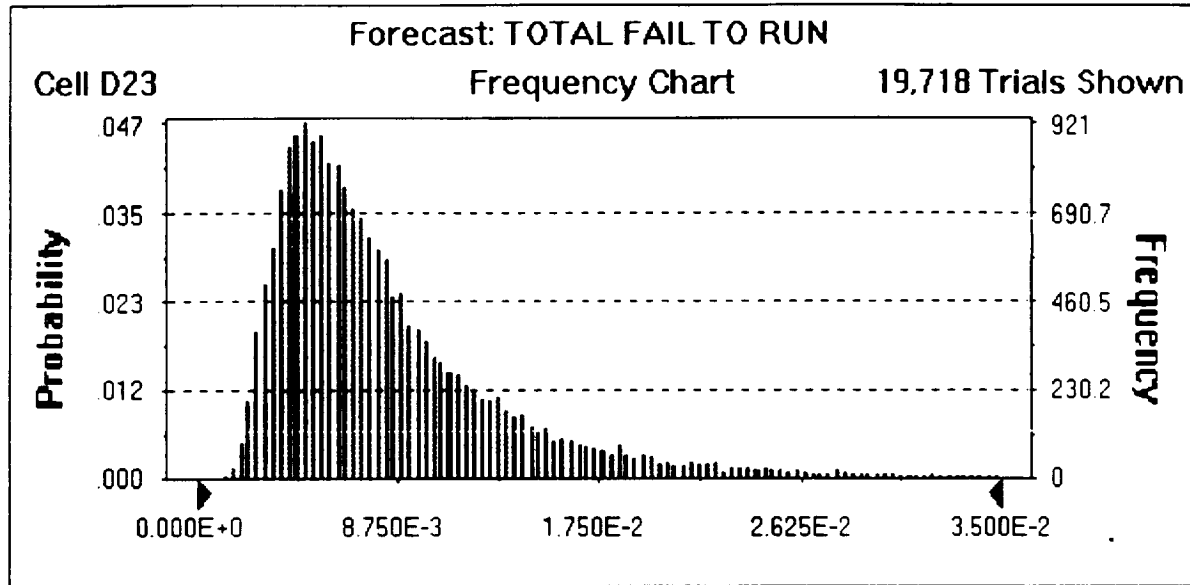


Figure 9.2-4: @Risk Simulation Results for Failure to Run Frequency

Failure	Mean-Dist	5th percentile	Median	95th percentile	Reference
Bypass Valve Fails To Open On Demand	4.689E-04	1.690E-05	1.730E-04	1.276E-03	1
Common Cause Heater Train 13 Failure	6.5E-05	4.6E-006	3.6E-05	1.5E-04	1
Common Cause Lube Oil Heater Train Failure	2.1E-05	5.3E-07	7.8E-06	5.7E-05	1
Fuel Pump Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Lube Oil Pump Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Turbine Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Gearbox Fails To Start	1.278E-05	9.139E-08	2.138E-06	4.702E-05	1
Electric Pwr To Primary Valve Fails	6.2E-04	1.3E-05	2.0E-04	1.9E-03	1
Electric Power To Secondary Valve Fails	6.207E-04	1.329E-05	2.045E-04	1.879E-03	1
MPU Fails Low	7.409E-04	3.447E-05	3.260E-04	2.032E-03	1
HYD Main Pump Fails To Start	4.0E-04	4.683E-05	2.426E-04	1.257E-05	6
HYD Accumulator Has No Pressure At Start	4.475E-03	1.68E-04	1.680E-03	1.68E-02	2 <sup>(1)</sup>
HYD Reservoir Low/No Fluid At Start	4.475E-03	1.68E-04	1.680E-03	1.68E-02	2 <sup>(1)</sup>
Total Failures To Start	1.205E-02	3.322E-03	7.949E-03	3.342E-02	

<sup>(1)</sup> Converted hourly failure rate to a start failure by multiplication by exposure time (168 hours)

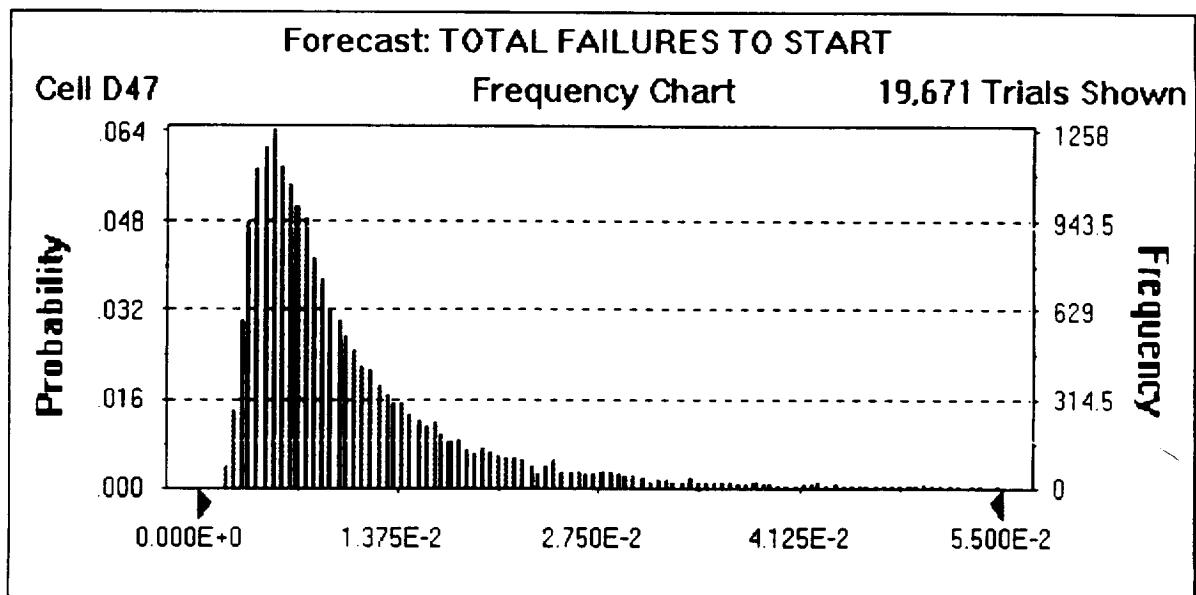
1. 1987 APU Study
2. NPRD-95
3. IEEE-STD-500

4. OREDA
5. WASH-1400

6. Shuttle history of 0 failures is 882 demands in a maximum entropy log normal:  $882 = (6 \text{ APU Starts/Missions} + 4 \text{ HPU Starts} + \text{HPU Hot Fire Tests}) \times 63$

**Table 9.2-2: Component Failures Leading to APU System Start Failure (Failures/Demand to Start)**

The @Risk Monte Carlo simulation (20,000 trials) for the failure to start probability distribution can be seen in Figure 9.2-5.



**Figure 9.2-5: @Risk Simulation Results for Failure to Start Frequency**

### 9.2.2.3 Turbine Overspeed and Hub Failure at Normal Speed

Figure 9.2-3 depicted the fault tree for a turbine overspeed condition which is an initiating event (TU). Prior distributions were obtained from the 1987 APU study. The following Table 9.2-3 provides the priors and the in-flight shuttle data used for the likelihood function. The posterior failure rates of these various components are listed in Table 9.2-5. To calculate the turbine overspeed frequency distribution based on fault tree logic, @Risk Monte Carlo simulation (20,000 trials) in a Lotus 1-2-3 spreadsheet was used.

Event	Prior (Log Normal) 5 Percentile	Prior (Log Normal) 95 Percentile	Shuttle Specific Data
PASVC	$8 \times 10^{-5}/D$	$7 \times 10^{-3}/D$	1/378 Demands <sup>(1)</sup>
TASVE	$1 \times 10^{-4}/hr$	$1 \times 10^{-2}/hr$	0/0 <sup>(2)</sup>
TAMIL	$5 \times 10^{-5}/hr$	$5 \times 10^{-3}/hr$	1/796 hrs <sup>(3)</sup>
PAPVE	$1 \times 10^{-4}/hr$	$1 \times 10^{-2}/hr$	1/292 hrs <sup>(4)</sup>

<sup>(1)</sup> 2 Demand/APU x 63 millions x 3 APUs/Missions = 378 Demands

<sup>(2)</sup> Failure of primary valve in mission SB-31 generated a demand on the secondary valve for a few minutes before the launch was scrubbed. The secondary valve did not fail.

<sup>(3)</sup> 1.33 hours/APU x 3 APUs/Missions x 3 HPU/APUs x 63 Missions = 796 hours

<sup>(4)</sup> 1.33 hours/APU x 3 APUs/Missions x 63 Missions = 292

**Table 9.2-3: Priors and In-Flight Shuttle Data Used for the Likelihood Function**

Shuttle in-flight failures used in the above table are described below in Table 9.2-4:

Car No.	Date	Flight No.	APU No.	Basic Event	Description
AC8511-01	08/06/84	41B	3	PASVC	GGVM Shut off valve leaking at a rate of 248 scim due to a broken poppet valve seat
AC0055-01	07/24/81	1	2	TAMIL	MPU #2 was inopr.; MPU resistance measured open
IFA STS-31-01	04/24/91	STS-31	1	PAPVE	Primary pulse control valve chipped (valve sent failure) allowing hydrazine to continue flowing. Secondary valve took over. Launch scrubbed.

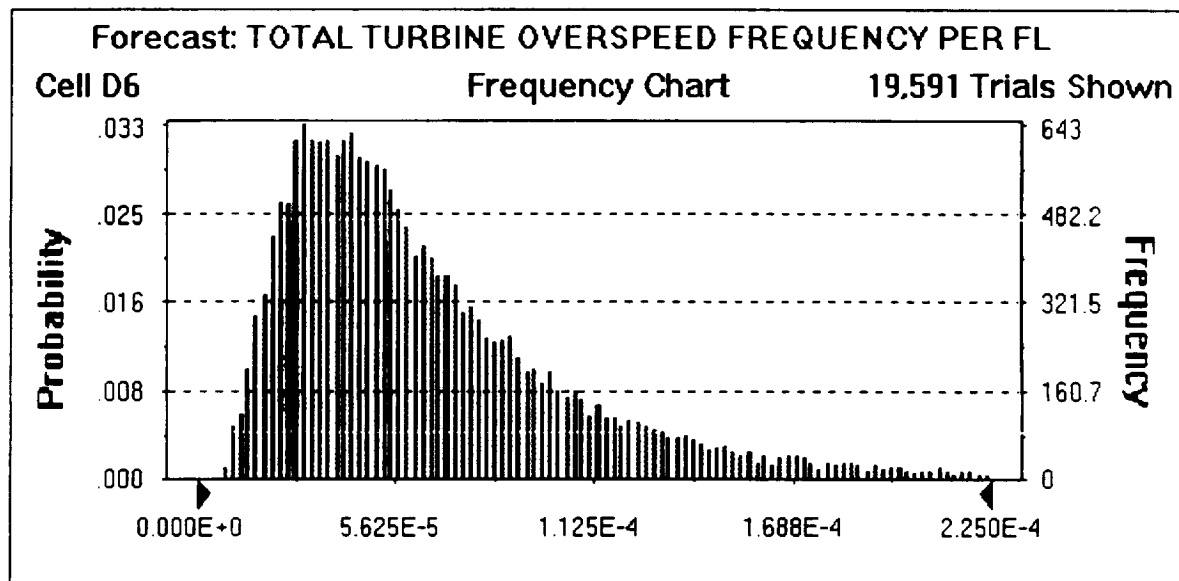
**Table 9.2-4: APU Turbine Component Failure Descriptions**

The @Risk Monte Carlo simulation (20,000 trials) for the failure to start probability distribution can be seen in Figure 9.2-6.

Failure	Mean-Dist	5th percentile	Median	95th percentile
Primary Valve Fails Open During Pulsing	1.477E-03	6.852E-05	6.500E-04	4.054E-03
Magnetic Pickup Unit Fails Low	2.240E-03	1.747E-04	1.202E-03	6.127E-03
Secondary Valve Fails Open During Pulsing	9.602E-04	5.032E-05	4.484E-04	2.685E-03
Secondary Valve Fails To Close On Demand	2.631E-03	2.305E-04	1.504E-03	7.500E-03
Total Probability For Turbine Overspeed/Flight <sup>(1)</sup>	2.518E-04	6.733E-06	7.530E-05	9.403E-04

(1) All APUs included

**Table 9.2-5: Posterior Failure Rate Data for Component Failures Leading to Turbine Overspeed**



**Figure 9.2-6: @Risk Simulation Results for Turbine Overspeed Frequency**

Turbine hub failure at normal speed is not a significant contributor to the probability of this event. APU hub cracking is mapped and it has been shown by analysis (at JSC) that the likelihood of blade cracking propagating to a hub crack is very small. Furthermore, experiments on hub breakup show that even a notched or drilled hub requires a speed significantly above nominal to induce hub failure. NPRD-95 has a value of turbine failure of about  $10^{-5}$ /hr. for all modes combined, not just hub failure. Therefore, hub failure at normal speed is at least an order of magnitude less in probability than turbine overspeed.

#### **9.2.2.4 Other Prior Distributions**

The remaining prior distributions were taken directly from the 1987 study, were defined by MGL analysis, or were a result of our assessment. All of the prior distributions are in Table 9.2-8. The two letter descriptions were discussed previously in Table 9.1-1.

Some events, such as an APU OK state, are not in this table since they are not incorporated into the quantification of the scenarios. For some inputs only a mean value was estimated.

#### **9.2.2.5 Large Exhaust Gas or Hydrazine Leak (LL)**

This prior distribution was generated by breaking the event down into its three major contributors: tank/pipe rupture; hot gas leak; and isolation valve leak/rupture. For both the tank/pipe rupture and hot gas leak modes, a failure rate range based on variability was defined from Nonelectronic Parts Reliability Data 1995 (NPRD-95). The median value from this range was multiplied by the 1.5 hour total APU run time for ascent and descent, and times 3 for the number of APUs, to get a point estimate failure probability for the system per flight.

A failure rate range was also defined for the isolation valve leak from NPRD-95. In this case, the range was treated as defining the 5th and 95th percentiles of a lognormal distribution which was used as the prior in a Bayesian update. The evidence data consisted of two incidents in which cracks were found in APU and HPU isolation valves which did not propagate to a through crack of the valve casing that separates the flow path from the solenoid cavity. The concern here is that when hydrazine comes in contract with the solenoid it could decompose and rupture the isolation valve causing an unisolatable leak. These were not "hard" failures, but are valid evidence of failure potential. They were treated, therefore, by a near miss methodology as follows.

The solution was to treat the data according to the probability that these incidents might propagate into "hard" failures on other flights, where the circumstances might be different. This is a matter of judgment on the part of the analyst. In this case, since these incidents were determined to have a low probability of propagating to "hard" failures, the evidence was treated as having a 5% probability of representing 1 failure in 72000 hours (a lower bounding estimate of the total exposure time for APU and HPU isolation valves), and a 95% chance of representing zero failures in 72000 hours. The overall posterior distribution was then generated by taking a weighted average (according to the previously determined weights) of the two possible posterior distributions.

The following Table 9.2-6 shows the prior distributions.

	5 Percentile	95 Percentile	Exposure Time
Tank/Pipe Replace (prior only)	10 <sup>-9</sup> /hr.	10 <sup>-7</sup> /hr.	63 x 3 x 1.5 hrs.
Hot Gas Leak (prior only)	same	same	same
Isolation Valve (prior)	1 x 10 <sup>-7</sup> /hr.	10 <sup>-7</sup> /hr.	72000 hrs.
Isolation Valve (updated)	1.2 x 10 <sup>-9</sup> /hr.	8 x 10 <sup>-8</sup> /hr.	

**Table 9.2-6: Distributions for Large Hydrazine or Exhaust Gas Leak**

The data used in the isolation valve analysis is anecdotal. We are aware of a crack discovered in an APU isolation valve before STS-1. We are also aware of a recent crack found in an HPU, that when tested post-flight, leaked hydrazine into the solenoid cavity.

#### **9.2.2.6 Leak in One APU Unit (LK)**

A Bayesian analysis was not performed for hydrazine leaks. Shuttle in-flight experience was used to generate a point estimate of the rate at which hydrazine leaks develop. This rate was based on the data in Table 9.2-7, showing 6 leaks in 31752 hours of exposure time (63 flights x 3 APU's x assumed average flight duration of 7 days x 24 hours/day). To generate a probability distribution, the point estimate was assumed to be the mean value of a maximum entropy ( $\sigma = 1.0$ ) lognormal distribution.

This assessment was based on a number of assumptions. We assume that the APU's are leak checked and only launched if found acceptable. Hydrazine leaks may occur at any time during the mission. Exposure to hydrazine may cause leaks even without the system operating. However, the leaks may only be revealed when the system is operating.

CAR	IFAS	Flight	Date	APU #	Description
**		1CR	04/12/81	1	Hyd. leak from fuel pump cover
**		1CR	04/12/81	2	Hyd. leak at fuel pump inlet fitting
09F012-01		STS-9	11/28/83	1	Hyd. leak from cracked fuel injector tube *
09F013-01		STS-9	11/28/83	2	Hyd. leak from cracked fuel injector tube *
	X	STS-51F	07/29/85	1	Hyd. leak into gearbox ***
	X	STS-45	03/24/92	1	Hyd. leak into gearbox ****
<p>* APU failed due to the hydrazine leak</p> <p>** Data from APU subsystem manager database</p> <p>*** This leak was detected by increased pressure in the gearbox and the start of APU2 was delayed until Vrel=10k</p> <p>**** On this same mission APU2 leaked oil / GN2 from the gearbox to the aft compartment</p>					
	X	STS-45	03/24/92	2	Lube oil / GN2 leak from gearbox through turbine seal

**Table 9.2-7: Hydrazine Leakage History on STS**

The APUs contain many potential leakage sites. The data simply indicates that some have already occurred. Others have yet to become active. Because of this, we do not necessarily view corrective actions to individual leakage sites as reducing the predicted frequency of leaks. Rather, we treat past leaks as indicative of future rates.

#### **9.2.2.7 Leak Detected Confirmed (LD and LA)**

The first four leaks above were not detected during the mission. The last two leaks were detected by increased pressure in the gearbox. We assess the probability of leak detection, and APU delayed start, as 1 in 6 based on this data. Since no action has ever been taken on leaks during ascent, this indicated zero probability of leak detection on ascent. The use of zero detected and confirmed leaks during ascent avoids the paradox associated with a groundrule of this study. The groundrule is that aborts are assumed to be successful. Therefore, a failure that leads to an APU induced abort actually reduces the calculated risk. Flight rules call for an APU shutdown and an MDF abort if a single hydrazine leak is detected and confirmed. Two such leaks lead to a PLS abort. To avoid having to treat leaks as successes, we assume no detection on ascent.

#### **9.2.2.8 Own Leakage/Other Leakage Induced Failures (LF and LO)**

These prior distributions were defined through a data based assessment utilizing the 1987 study, PRACA records, hazards analyses and an understanding of the phenomenology of the failure modes. Specifically, the mean value for own leakage induced failure during descent was defined from the data shown in Table 9.2-7, indicating 2 APU failures in 6 leaks. The mean values for the other three conditional probabilities were then derived by maintaining the ratios between the values from the 1987 study and scaling them to the 0.3 defined for LF (des). This produced values of 0.2 for LO (des), 0.1 for LF (asc) and 0.008 for LO (asc).

An assessment of the applicable distributions was then made for the four probabilities. In the case of LF (des), an upper  $4\sigma$  bound of 0.5 was defined for the distribution, assuming a normal distribution. For LF (asc), an upper  $4\sigma$  bound of 0.2 was defined, again assuming a normal distribution. And for LO (asc), given the small value of the mean (0.008), a lognormal distribution was judged to be more applicable, as greater uncertainty is expected for small defined values. For this distribution, an Error Factor of 5 was assumed. For the normal distributions, values below zero should be truncated when using the defined distributions.

In the case of LO (des), data is available for a Bayesian update of the assessed value, so the distribution needs to be defined much broader than for the other cases (where the posterior was being defined directly), in order to overlap the likelihood function of the evidence. The prior distribution was defined using 0.2 as the mean value for a maximum entropy ( $\sigma = 1.0$ ) lognormal distribution. This was updated with evidence of 0 APU failures in 12 APUs exposed to other units leaking. Note the following for each leak: There are 2 opportunities for another APU to fail owing to the leak and 1 opportunity for itself to fail. For 6 leaks, there are  $6 \times 2 = 12$  opportunities for failure of another APU owing to the leak. None has occurred. The mean value of LO (des) drops to 0.07 given this evidence. The result of the Bayesian analysis is shown graphically in Figure 9.2-7.

#### 9.2.2.8.1 Sensitivity Treatment of APU 3 Failures

The previous section described the baseline treatment of these conditional probabilities. In the case of APU failure due to another units leakage (LO), it could be argued that APU 3 needs to be treated differently. APU 3 is physically located about 6' (on the starboard side) from the other two units, which are only a few inches apart. Thus, we believe that there is a lesser chance of APU 3 failing due to leakage in unit 1 than an APU 2 failure.

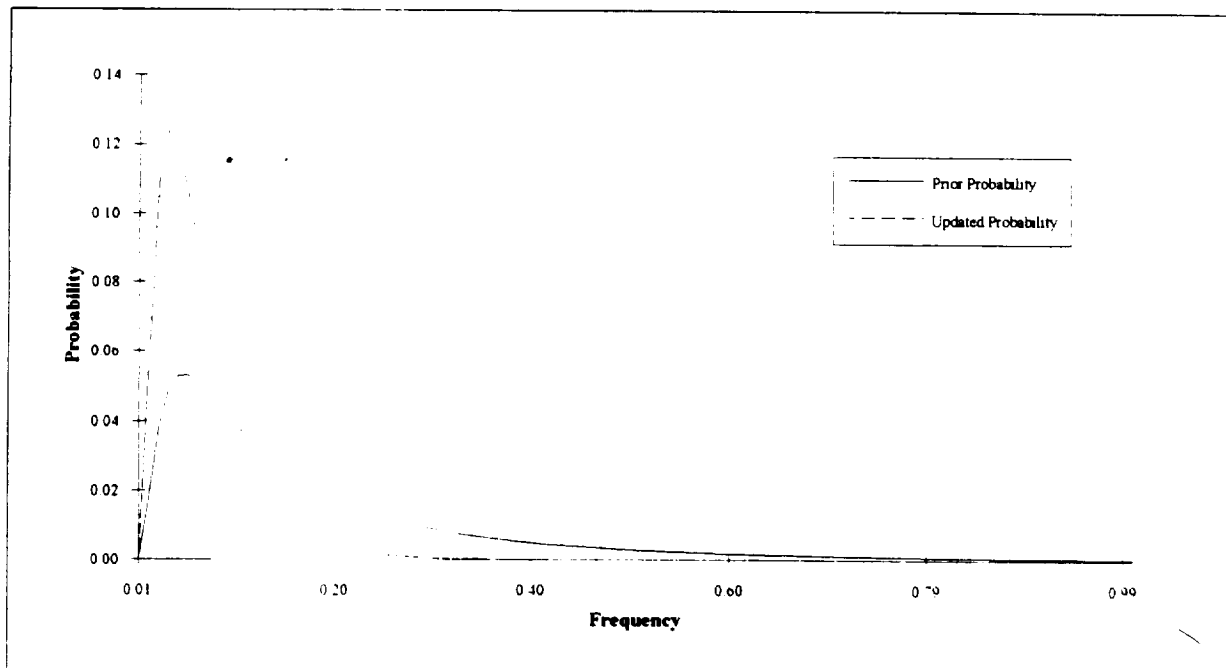
Our fault tree treatment is conservative in that each APU is considered "identical". It does not capture "full credit" for cases in which the actual APU 3 is leaking, which would lead to reduced LO conditional probabilities for both of the other units.

One way of capturing this logic would be to drop the LO conditional probability to a lower value for all of the APU 3 terms. In order to illustrate the affect this would have on the results, two of the most significant leakage fault trees have been quantified, at the mean value, for these two cases. For the baseline case:

- OK Initial State on Entry, Seq. 16      4.159E-04
- OK Initial State on Entry, Seq. 17      1.700E-04

For the sensitivity case, using as an example 0.01 as the unit 3 LO (des) probability:

- OK Initial State on Entry, Seq. 16      2.479E-04
- OK Initial State on Entry, Seq. 17      6.214E-05



**Figure 9.2-7: Bayesian Analysis Result for LO (Des)**



#### **9.2.2.9 Unsuccessful Single APU/HYD Unit Reentry, TAEM and Landing (UL)**

This prior distribution was generated according to judgment weighted by several factors. First, such landings are regularly simulated successfully in training. To the extent that the simulator is successful in characterizing the vehicle response given a single APU/HYD unit, this gives credence to a very high probability of success. However, this is tempered by the fact that a single APU/HYD unit landing is not certified by the program. Unfavorable weather conditions coupled with slower control rates could potentially indicate a much higher probability of a failed landing. The assessment team has translated this into a range of 80% to 100% for a successful landing. It was also determined that the lack of a strong conviction for any values within this range warranted a uniform distribution for this range.

ID	$\beta\delta$ -factor	PRIOR (/hr or /demand)			
		Mean	Median	5th	95th
CE	N/A	0.5 (LL) 0.88 (TU)			
CF	Calculated	using applicable	MGL method	formulas	
CL	Calculated	using applicable	MGL method	formulas	
CO	N/A	1			
CS	Calculated	using applicable	MGL method	formulas	
HB	N/A	0.9			
ID	N/A	9.150E-03/hr	6.956E-03/hr	3.059E-03/hr	2.174E-02/hr
IF	N/A	9.150E-03/hr	6.956E-03/hr	3.059E-03/hr	2.174E-02/hr
IS	N/A	1.205E-02/start 9.150E-03/hr	7.949E-03/start 6.956E-03/hr	3.322E-03/start 3.059E-03/hr	3.342E-02/start 2.174E-02/hr
LA	N/A	0.0 (asc) 0.1667 (des)			
LD	N/A	0.0 (asc) 0.1667 (des)			
LF OS	N/A see posterior	1.0E-01 (asc)	1.0E-01 (asc)	6.0E-02 (asc)	1.4E-01 (asc)
LK	N/A	1.890E-04/hr	1.152E-04/hr	2.224E-05/hr	5.971E-04/hr
LL	N/A	2.8E-05			
LO LS	N/A	8.0E-03 (asc) 2.0E-1 (des)	5.0E-03 (asc) 1.2E -01	9.9E-04 (asc) 2.3E-02	2.5E-02 (asc) 6.36-01
LU	N/A	1.0 (asc) 0.8333 (des)			
LZ	N/A	1.0 (asc) 0.8333 (des)			
SI	N/A	1.0 (LL) 0.88 (TU)			
SR	N/A	0.98795/start	0.99205/start	0.99668/start	.96658/start
TU	N/A	2.518E-04	7.530E-05	6.733E-06	9.403E-04
UL	N/A	0.1	0.1	0.01	0.19

**Table 9.2-8: Prior Probability Distributions**

### **9.3 Posterior Distributions for APU/HYD/WSB Failure to Run and Start (Ascent and Descent)**

Posterior distributions were determined by updating the prior distributions with available data using Bayes' Theorem. Data points not only include failures of the APU and HYD systems, but also the Water Spray Boiler (WSB). WSB failures, which lead to an APU shutdown and subsequent hydraulic loss, were not examined in the previous 1987 study, so data was extracted for these failures from all Shuttle flights. Other data points pertaining to these failures were taken from post-Challenger flights (1988) to STS-65 (flight 63, 7/8/94).

#### **9.3.1 Water Spray Boiler Failures Used in the Analysis**

##### **9.3.1.1 03-23-1982 STS-3**

WSB 3 freeze-up during ascent. APU temperature message at lift-off plus 4 minutes 23 seconds reported lube oil temperature climbing. Controller B was then selected, but the temperature continued to rise. APU 3 shutdown at liftoff plus 8 minutes, and the right main engine went into hydraulic lock-up. After ascent, at lift-off plus one hour, controller A was then selected; both controllers appeared to be working properly. The maximum APU 3 lube oil temperature was 330°F, and the maximum bearing temperature was between 355 and 360°F. FCS checkout tested both controllers, and both were 100% nominal. This situation was also seen on STS-1 and 2.

##### **9.3.1.2 08-02-1991 STS-43**

WSB 2 failed to provide cooling to the auxiliary power unit 2 lube oil throughout the mission. APU 2 (serial number 208) has been involved in lube oil over temperatures during seven of its eight flights. The WSB did not cool the lube oil on controller A following ascent. The crew switched to controller B when the lube oil return temperature reached approximately 297°F. The APU was operated an additional 1.5 minutes on the B controller, and still no cooling was observed. The APU was shutdown when the lube oil return temperature reached 323°F. The WSB is designed to control the lube oil temperature to 250±2°F.

An extended flight control system check-out using APU 2 was performed and the WSB was not cooling on either controller. The APU ran for 11 minutes during check-out, then was shutdown and declared lost. During descent, APU 2 was activated at terminal area energy management due to the lack of cooling. The lube oil reached 259°F before shutdown after wheel stop with no evidence of cooling. The spray boiler may not have had the chance to function, however, as this temperature is close to the 250°F control limit.

##### **9.3.1.3 09-12-1992 STS-47**

During ascent, WSB 3 (serial number 15) exhibited no cooling until just prior to the early shutdown of APU 3. The lube oil temperature reached approximately 292°F when the controller was switched from A to B. The lube oil temperature continued to rise to 311°F when the decision was made to shut down APU 3 early. Prior to APU 3 deactivation, the WSB GN2 regulator outlet pressure indicated that spraying had begun. WSB 3 continued to spray until the spray logic was turned off (1 minute 43 seconds). Steady-state cooling was never achieved on either controller since the lube oil temperature was not allowed to drop to 250°F prior to boiler spray logic shutdown.

APU 3 was selected to perform FCS checkout. The checkout time frame was extended to verify WSB 3 cooling performance. The extended run time demonstrated satisfactory cooling on both controllers (3 minutes 42 seconds for B, then 1 minute 47 seconds for A). WSB lube oil and hydraulic cooling performance during entry was nominal.

Spray bar freeze up remains the most likely cause of the WSB failure, although it could have resulted from spray valve or controller failures.

#### **9.3.1.4 01-13-1993 STS-54**

During ascent, WSB 3 (serial number 15) exhibited no cooling until just after the early shutdown of APU 3. The lube oil return temperature reached approximately 295°F when the WSB was switched from controller A to B. The lube oil return temperature reached 315°F when the decision was made to shut down APU 3 early. After deactivation, the WSB 3 GN2 regulator pressure indicated that spraying had started. WSB 3 continued to spray until the spray logic was turned off (approximately 35 seconds). Steady-state cooling was never achieved on controller A or B.

APU 3 was selected to perform the FCS check-out. The FCS checkout time frame was extended to verify WSB cooling performance. The extended APU 3 run-time demonstrated satisfactory cooling on both controllers, with a minor overcool observed on controller A. APU performance using controller B during entry was nominal.

Spray bar freeze-up remains the most probable cause of this cooling problem. However, data analysis also indicated that the local pressure at the vent nozzle of system 3 during ascent was somewhat higher than the other two systems. This high pressure is due to the location of the system 3 vent nozzle outlet (it is farther forward than the system 1 and 2 vent nozzle outlets). System 3's pressure remains higher than the other systems for the first 80 seconds of ascent, which is believed to be a contributing factor toward the repeated freeze-up anomalies observed in system 3.

Spray bar freeze-up conditions occur when the water triple point condition is met inside the heat exchanger. In the worst case freeze-ups, it is postulated the water triple point was reached prior to MECO. By increasing the water preload, the duration of heat exchanger tube bundle/water preload contact can be increased, which will reduce the likelihood/severity of spray bar freeze-up by maintaining pressure above the water triple point past MECO. The ongoing spray bar freeze-up test analysis indicates that the severity of the bar freeze-up at water triple point conditions may inversely correlate to the amount of water in the boiler. Therefore, KSC has been requested to preload WSB 3 to 5 +/-0.1 lbs. of water (normal is 3.75 +/-0.24 lbs.).

#### **9.3.2 Possible Water Spray Boiler Failure**

It is unknown whether or not this reported problem is an actual failure or not. For this analysis, it has not been considered as an actual data point.

##### **9.3.2.1 04-29-1985 STS-51B**

Shortly after MECO, the backup flight system indicated an APU 3 lube oil over temperature condition. The crew switched from controller A to B at a lube oil temperature of 320°F. The temperature continued to rise for an additional 20 seconds and reached a peak of 337°F. The crew was instructed to shutdown APU 3 to avoid reaching the lube oil temperature limit of 355°F. The

APU 3 lube oil temperature had decreased to approximately 320°F at shutdown, indicating that water spray boiler controller 3B was properly controlling lube oil cooling. Post flight testing has been unsuccessful in duplicating this problem. The A controller was replaced.

### **9.3.3 Possible Hydraulic System Failure**

#### **9.3.3.1 02-28-1990 STS-36**

Appendix C contains descriptions from PRACA records and hazards analyses of a "near-miss" failure involving a flex hose rupture in the hydraulic system.

### **9.3.4 Updated Posterior Distribution**

The four WSB failures in Section 9.3.1 were counted as APU shutdowns. All three of these failures occurred during the ascent phase. One of these failures was permanent and caused a late re-start of the APU during the entry phase, but was not counted as a failure during the reentry phase because it successfully completed its mission. For reentry, the hydraulic system rupture is counted as a possible APU/HYD unit failure in the update. The methodology for this type of update is described in section 9.2.2.5, where in this case the weighting uses 50% for 1 failure and 50% for zero failures. In the data column, if no data is available (i.e., no "trials"), an N/A for not applicable is placed in the box.

The common cause failure calculations for the MGL formulas used the ID and IS values, assuming 20 minutes for ascent and 1 hour for descent. The MGL calculations also used generic  $\beta$  and  $\gamma$  values of 0.1 and 0.27, respectively.

Table 9.3-1 lists the data and corresponding posterior probability distributions for the basic events. The means from these data distributions are used as basic event probability distribution inputs for use in SAIC's CAFTA model.

ID	Data	POSTERIOR (/hr or /demand)			
		Mean	Median	5th	95th
CE	N/A	0.5 (LL) 0.88 (TU)			
CF	Calculated	using applicable	MGL method	formulas	
CL	Calculated	using applicable	MGL method	formulas	
CO	N/A	1			
CS	Calculated	using applicable	MGL method	formulas	
HB	N/A	0.9			
ID	4/63 hrs	2.078E-02/hr	1.931E-02/hr	1.030E-02/hr	3.622E-02/hr
IF	4/63 hrs	2.078E-02/hr	1.931E-02/hr	1.030E-02/hr	3.622E-02/hr
IS	0/189 starts 0 to 1/252 hrs	5.677E-03/start 6.479E-03/hr	4.448E-03/start 5.614E-03/hr	1.433E-03/start 2.369E-03/hr	1.194E-02/start 1.219E-02/hr
LA	N/A	0.0 (asc) 0.1667 (des)			
LD	N/A	0.0 (asc) 0.1667 (des)			
LF	N/A	1.0E-01 (asc)	1.0E-01 (asc)	6.0E-02 (asc)	1.4E-01 (asc)
OS	2/6 Leaks	3.0E-01 (des)	3.0E-01 (des)	2.2E-01 (des)	3.8E-01 (des)
LK	N/A	1.890E-04/hr	1.152E-04/hr	2.224E-05/hr	5.971E-04/hr
LL	N/A	2.8E-05			
LO	N/A	8.0E-03 (asc)	5.0E-03 (asc)	9.9E-04 (asc)	2.5E-02 (asc)
LS	0/12 Leaks	7.0E-02 (des)	5.3E-02 (des)	1.4E-02 (des)	1.6E-01 (des)
LU	N/A	1.0 (asc) 0.8333 (des)			
LZ	N/A	1.0 (asc) 0.8333 (des)			
SI	N/A	1.0 (LL) 0.88 (TU)			
SR	N/A	0.99432/start	0.99555/start	0.99857/start	0.98806/start
TU	N/A	6.962E-05	5.501E-05	1.974E-05	1.672E-04
UL	N/A	0.1	0.1	0.01	0.19

**Table 9.3-1: Posterior Probability Distributions**

#### **9.4 APU/HYD/WSB ANALYSIS FOR SSME MODEL**

The APU failure probability assessment for the SSME model being produced at SAIC is somewhat different than that for this APU model. First, the exposure time is at most 520 seconds instead of 20 minutes. Second, only 1 of the WSB failures is relevant (STS-3) for purposes of calculating engine hydraulic lockup probability.

We started with the prior distribution for IF, given in Table 9.2-6, multiplied against the 520 second time period to produce a probability of failure (POF). We updated with 1 failure in 63 missions to produce a posterior. This represents the case in which the WSB failure and APU shutdown continues to be representative of how MCC and crew will react to a WSB failure. Since STS-3, other WSB failures have not resulted in a call for APU shutdown before MECO. Flight Rules indicate that APU shutdowns should occur post-MECO.

We also updated the same prior distribution for IF with 0 failures in 63 missions. This is like saying that STS-3 never happened and gives an overly optimistic assessment. An accurate assessment lies somewhere in between. We used a weighted average of each posterior where each update was given equal probability of being the correct one.

The Bayesian calculation is shown in Figure 9.4.1.

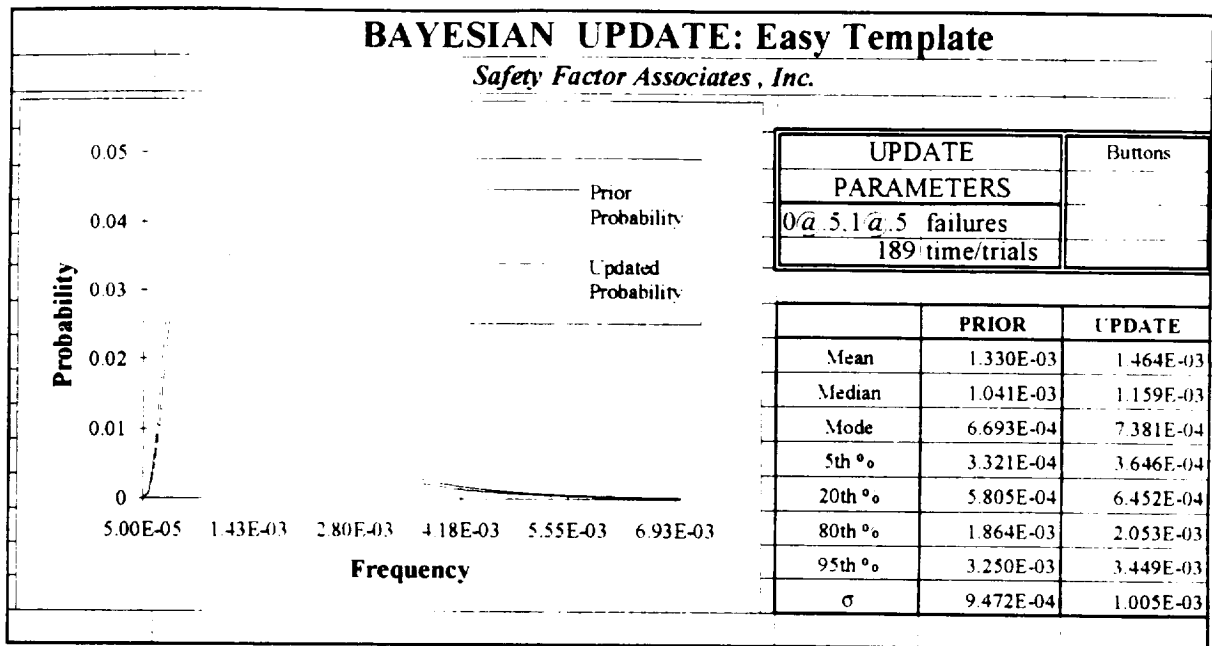
The MGL method was used to calculate the probability of loss of hydraulics for a single engine and for two engines as follows:

##### **1 Engine Goes into Hydraulic Lockup via Hydraulic Failure During Ascent**

$$Q = 3(1 - \beta)q_{APU} = 3(1 - 0.1)1.5E-04 = \mathbf{4E-04}$$

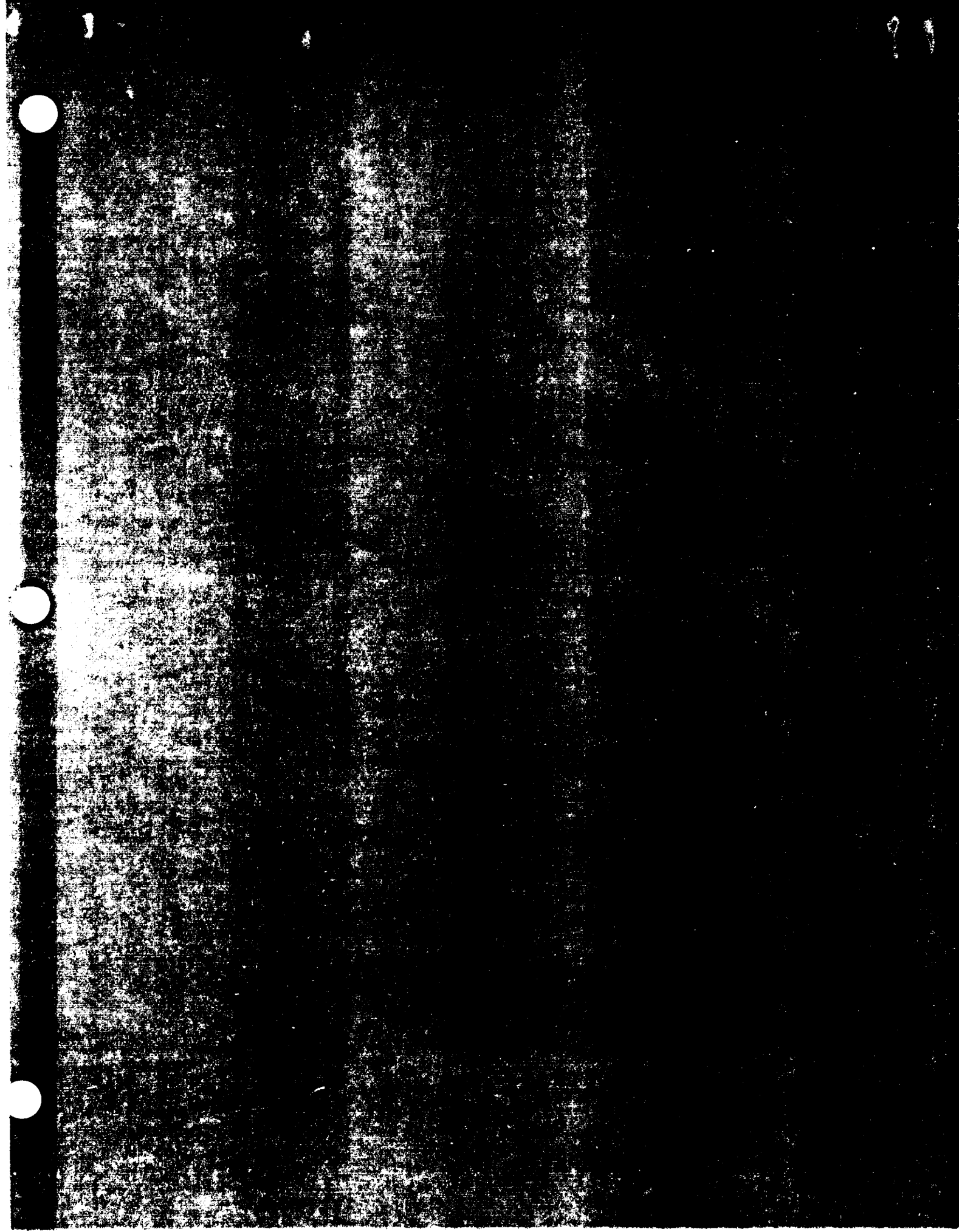
##### **2 Engines Go into Hydraulic Lockup via Hydraulic Failure During Ascent (First 5.6 minutes)**

$$Q = 3/2(1 - \gamma)\beta(336/520)q_{APU} + 3(1 - \beta)^2(336/520)^2 q_{APU}^2 = \\ 3/2(1 - 0.27)0.1(336/520)1.5E-04 + 3(1 - 0.1)^2(336/520)^2 1.5E-04 = \mathbf{1E-04}$$

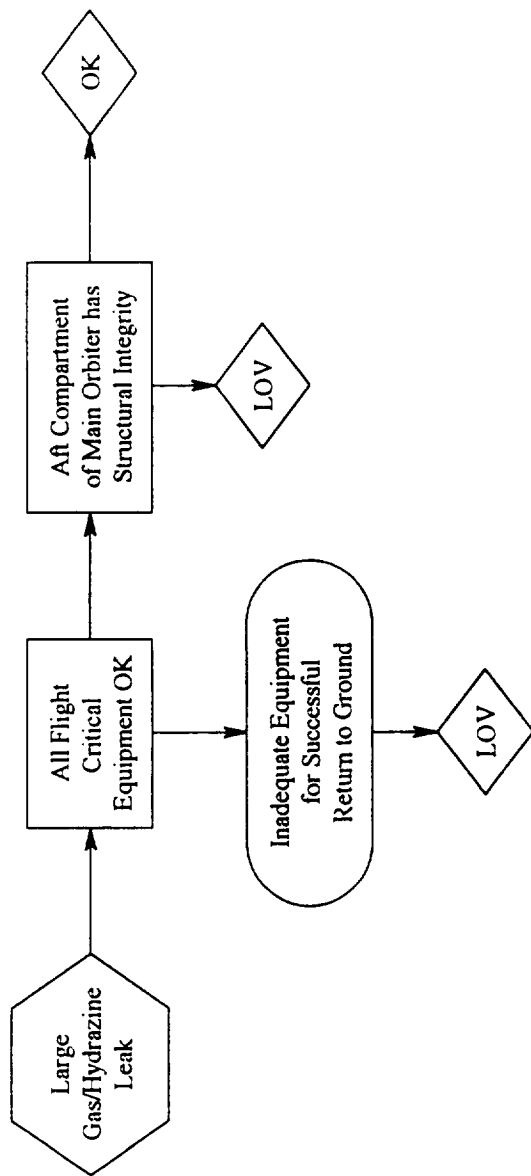


**Figure 9.4-1: APU Failures on Ascent Causing SSME Hydraulic Lockup (POF)**





## Event Sequence Diagram of a Large Gas/Hydrazine Leak



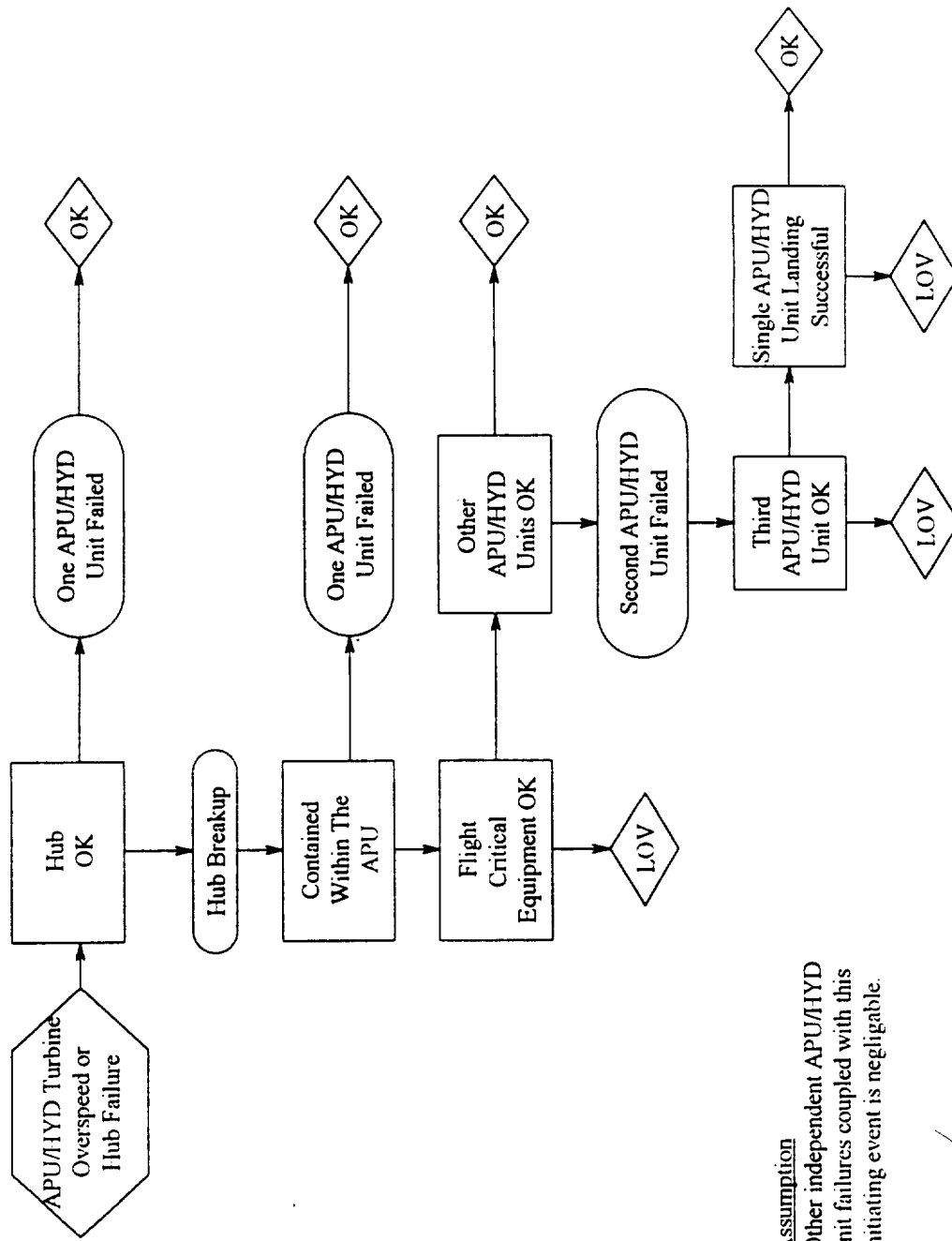
### Assumption

Because of the low frequency of severe exhaust gas leak, we have categorized this event with the unisolatable leaks. Separate categorization of the events would insignificantly change the estimated risk.

# EVENT TREE OF A LARGE GAS/HYDRAZINE LEAK

LL	SEQUENCE		SEQUENCE		STATE
	CE	SI	NUMBER	DESCRIPTION	
			1	LL	OK
			2	LLSI	LOV
			3	LLCE	LOV

# **Event Sequence Diagram for APU/HYD Turbine Overspeed and/or Hub Failure**

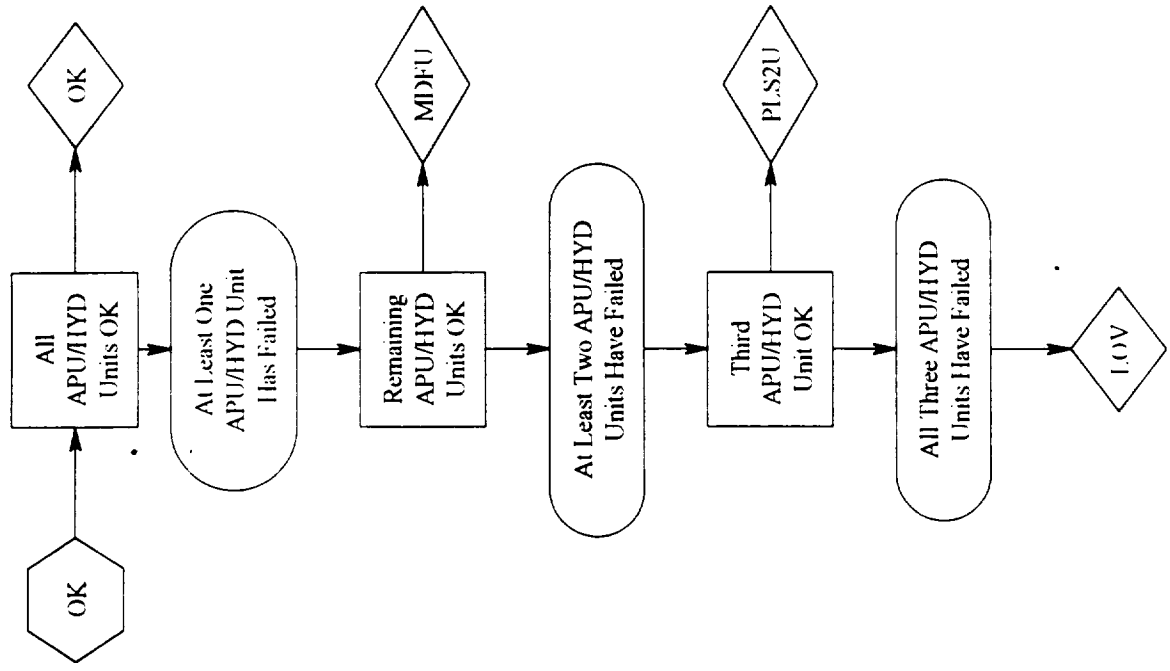


Assumption  
Other independent APU/HYD  
unit failures coupled with this  
initiating event is negligible.

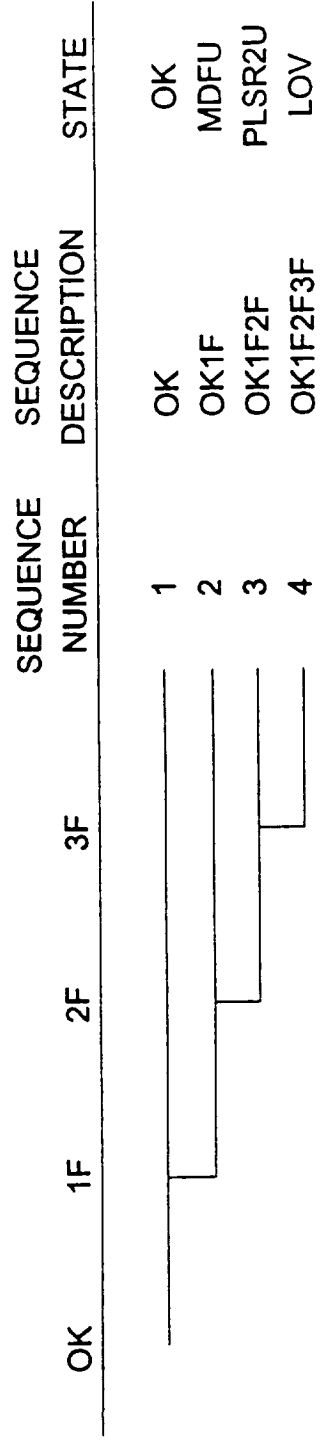
# EVENT TREE OF APU/HYD TURBINE OVERSPEED AND/OR BREAKUP

TU	HB	CO	CE	2F	3F	UL	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
							1	TU	OK
							2	TUHB	OK
							3	TUHBCO	OK
							4	TUHBCO2F	OK
							5	TUHBCO2FUL	LOV
							6	TUHBCO2F3F	LOV
							7	TUHBCOCE	LOV

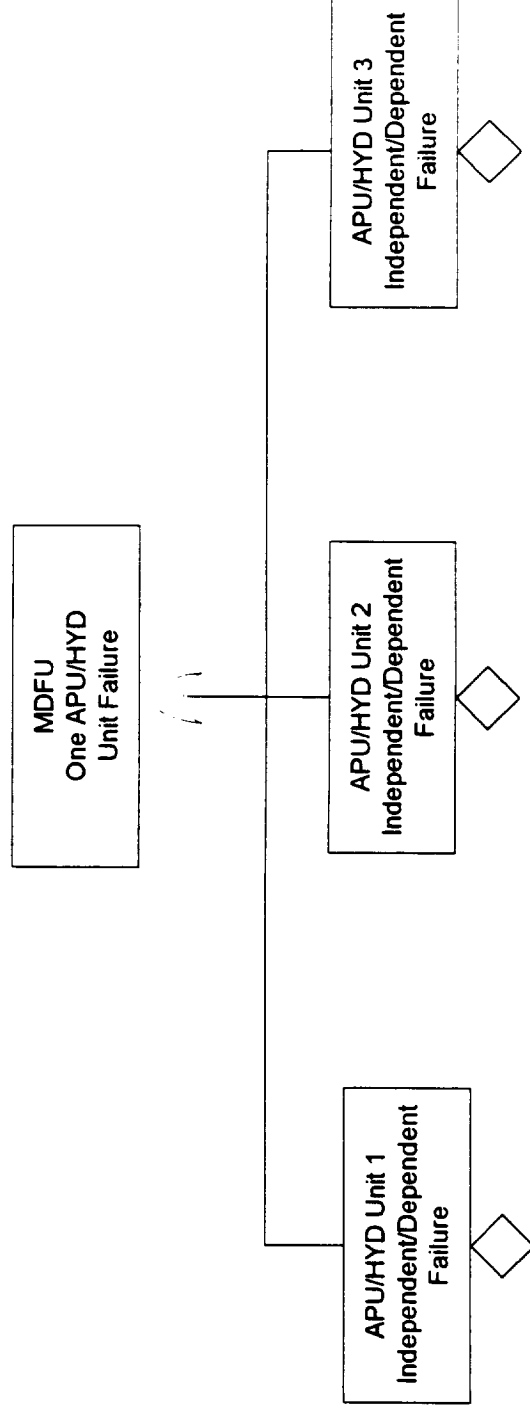
**Event Sequence Diagram for OK Start  
Without a Hydrazine Leak During Ascent**



# EVENT TREE OF AN OK START WITHOUT A HYDRAZINE LEAK DURING ASCENT

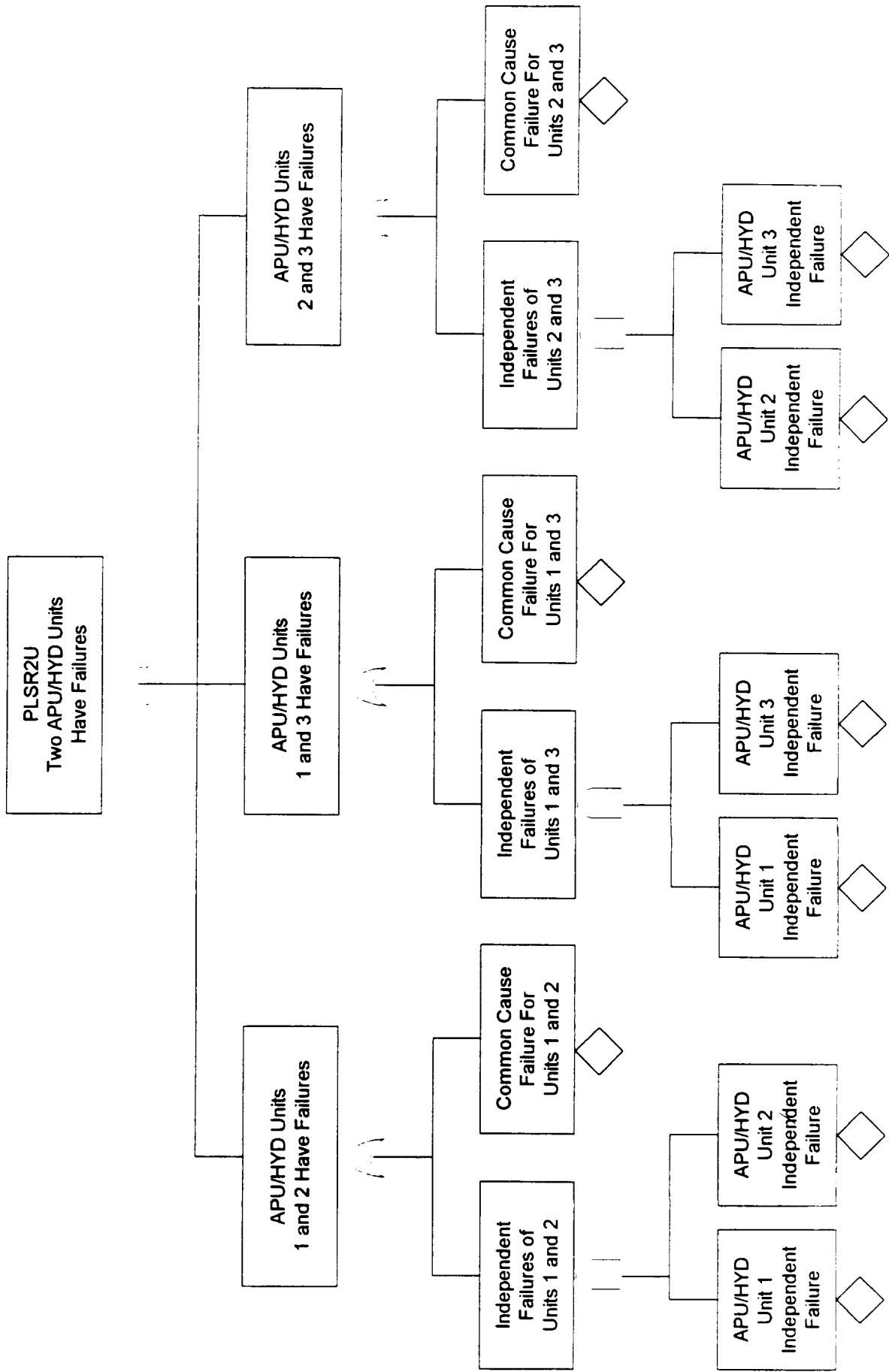


**Fault Tree For Sequence 2 MDFU  
State From OK Start Without A  
Hydrazine Leak During Ascent**

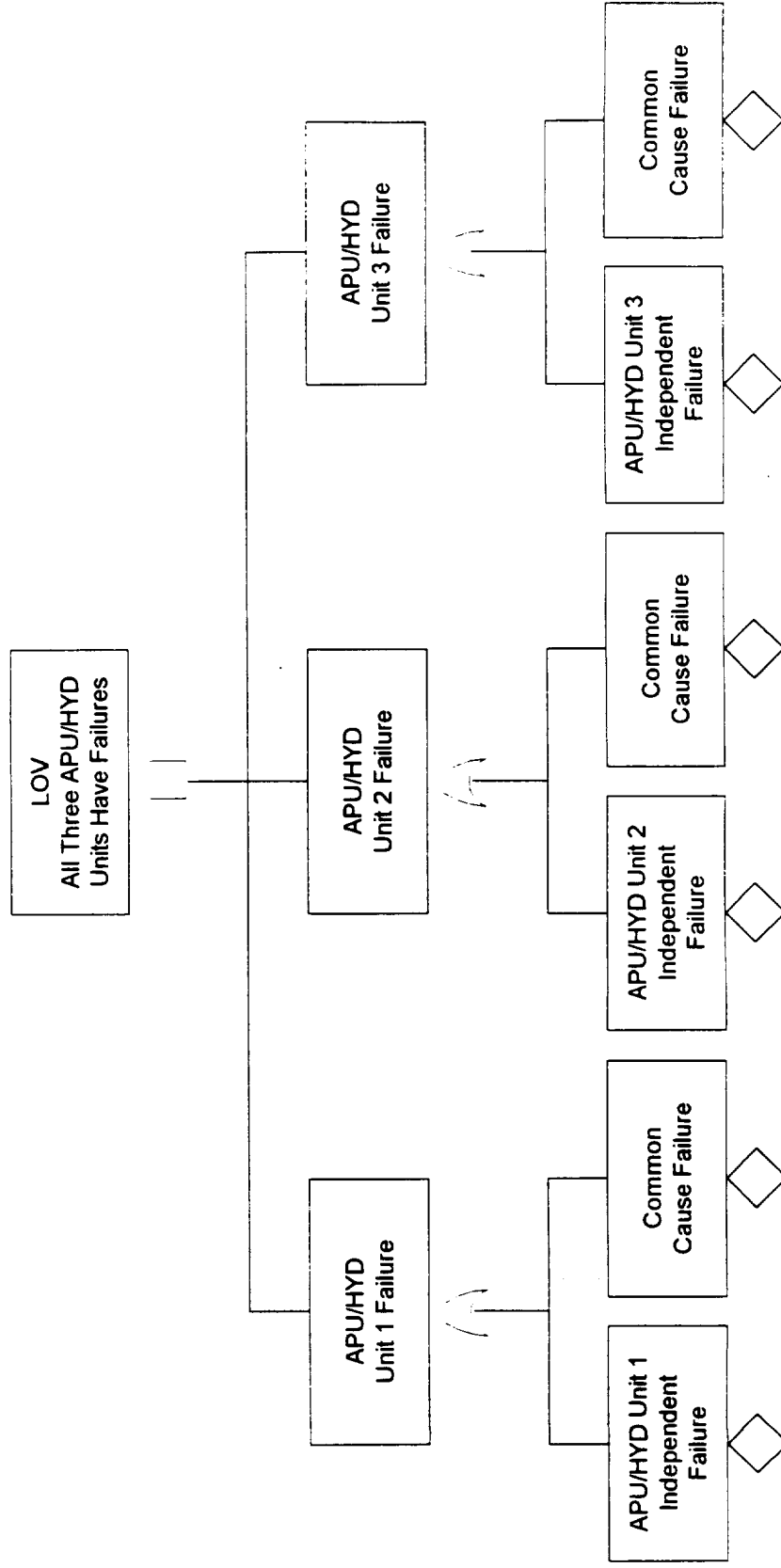




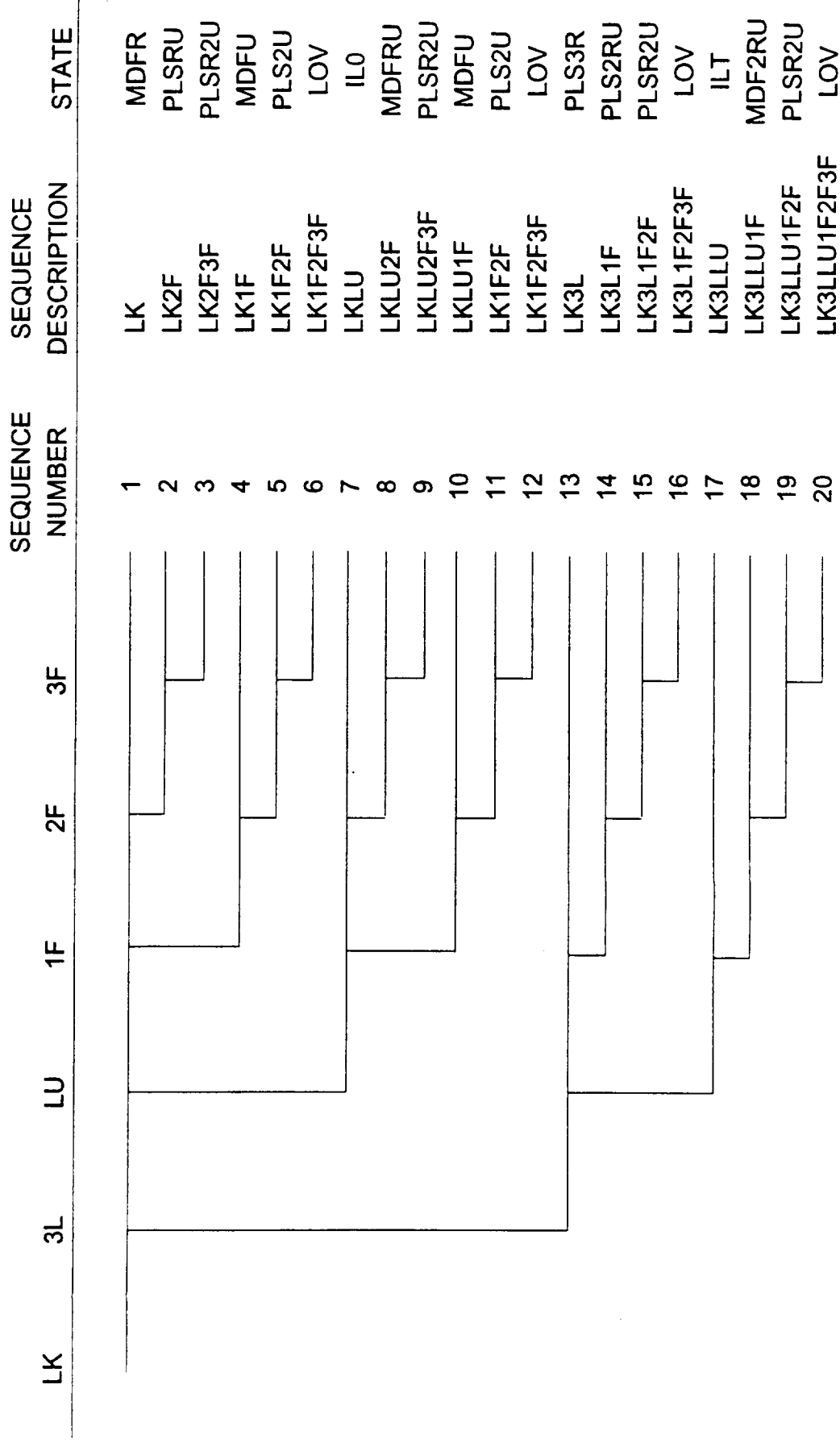
**Fault Tree For Sequence 3 PLSR2U  
State From OK Start Without A  
Hydrazine Leak During Ascent**



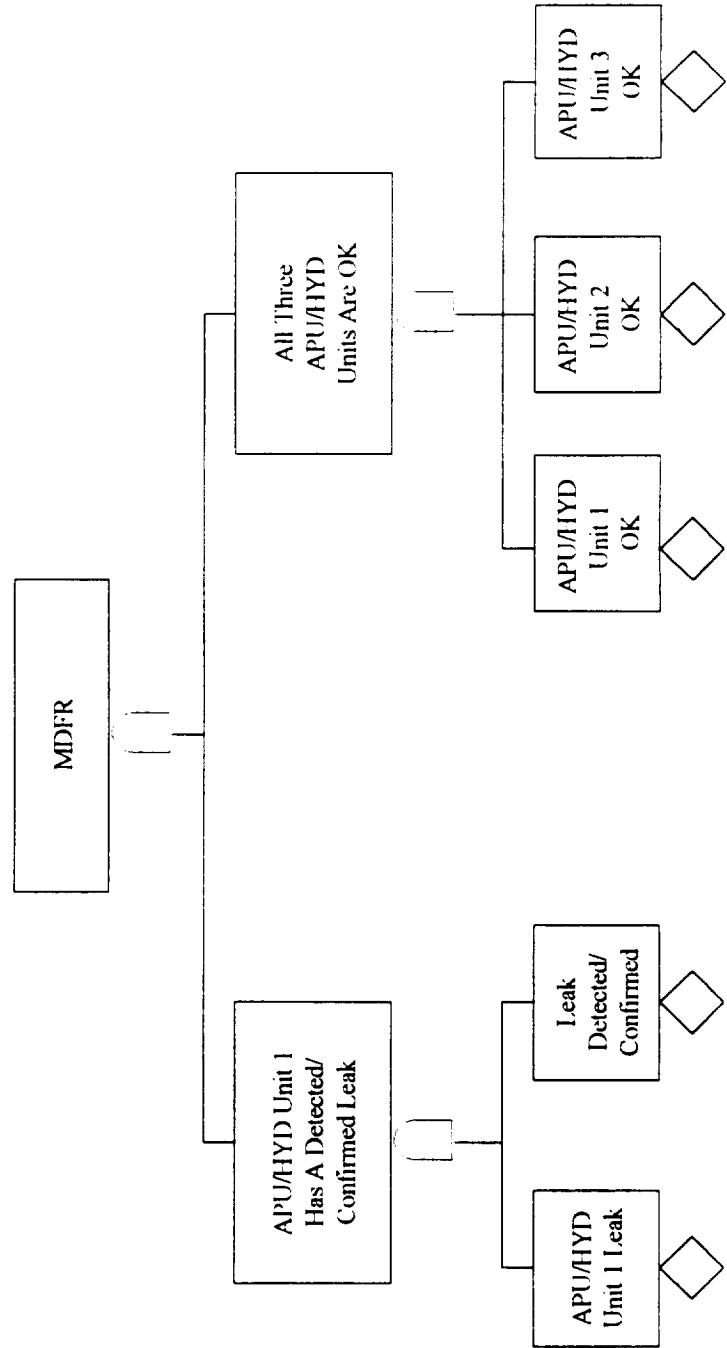
**Fault Tree For Sequence 4 LOV  
State From OK Start Without A  
Hydrazine Leak During Ascent**



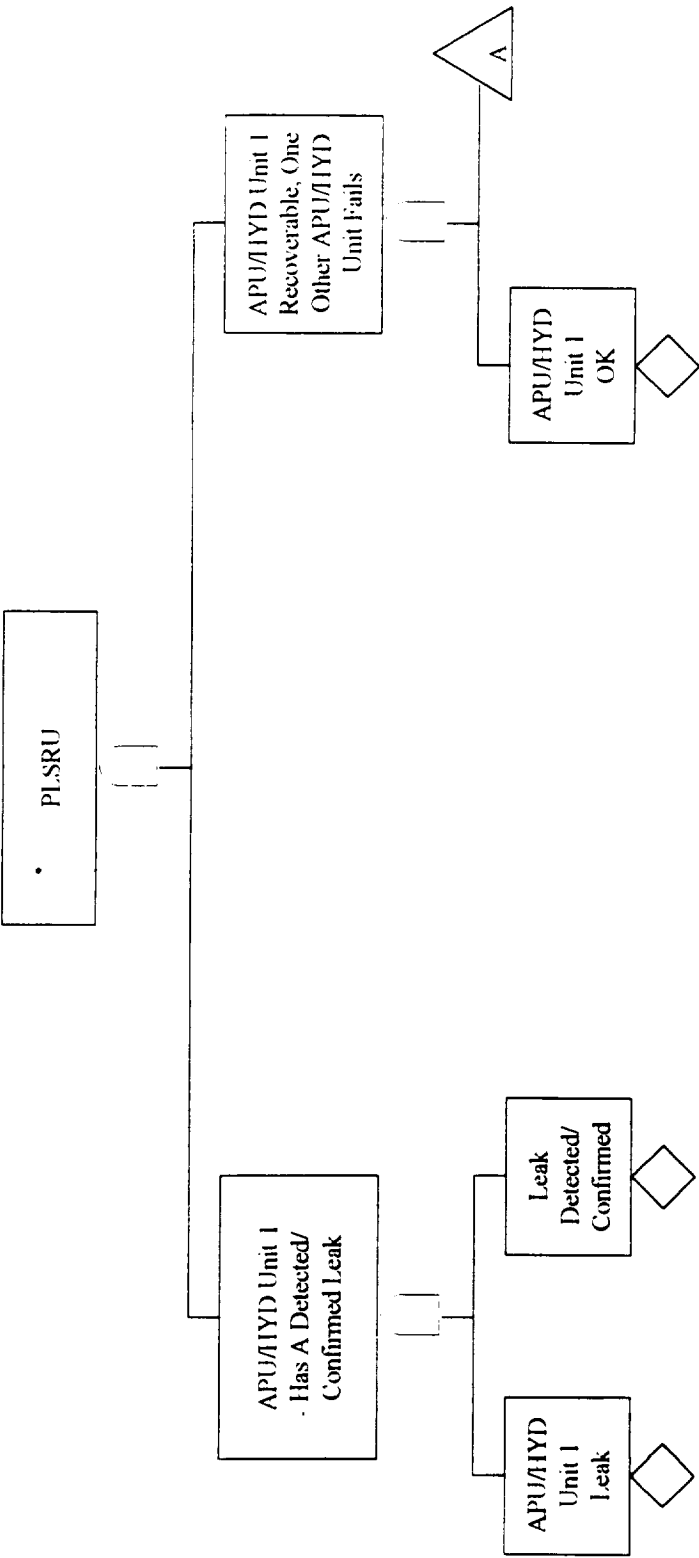
# EVENT TREE OF APU/HYD HYDRAZINE LEAK STATE DURING ASCENT



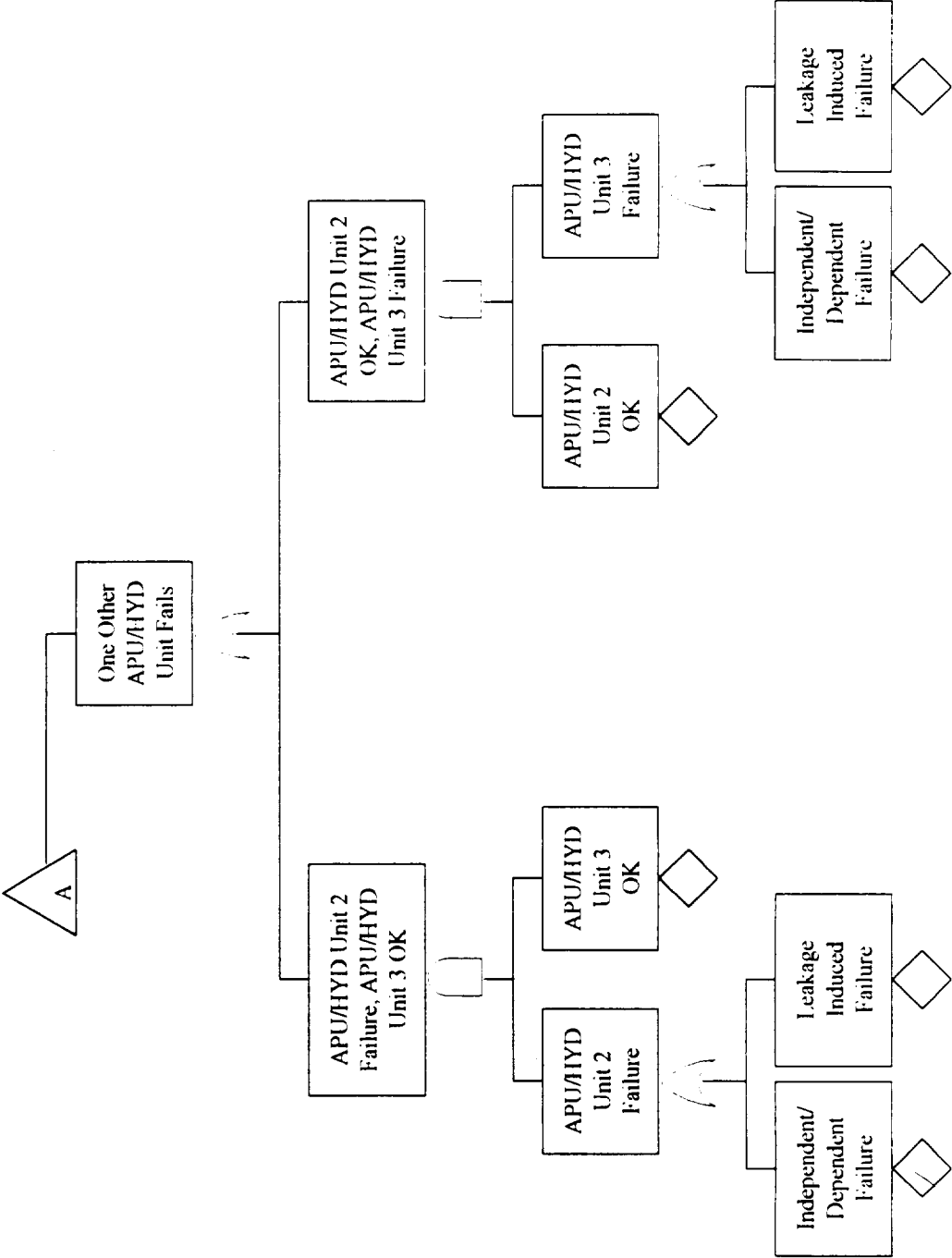
**Fault Tree for Sequence 1: MDRF State  
From a Hydrazine Leak State During Ascent  
one APU/HYD Unit has a Detected/Confirmed Leak  
and is Recoverable**



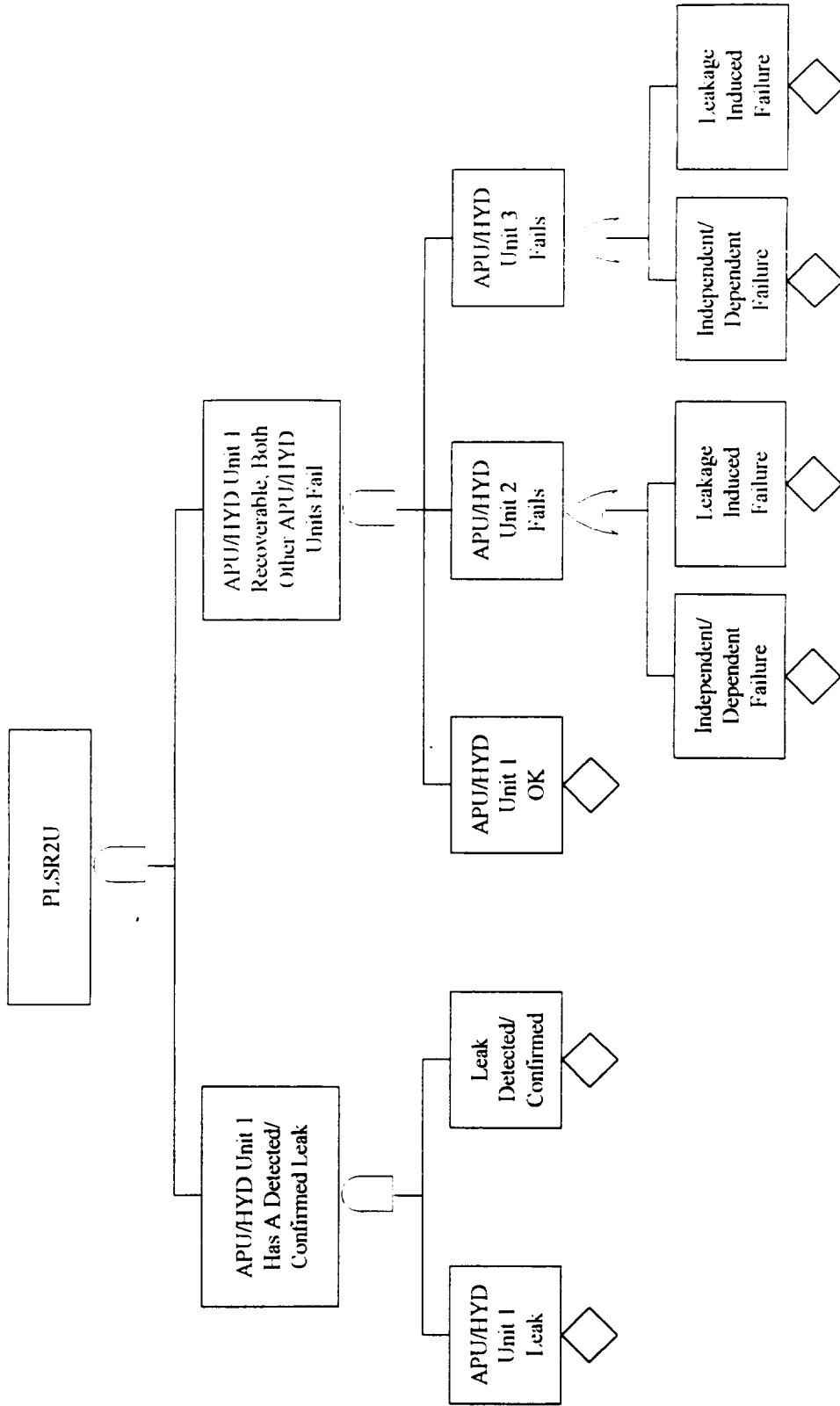
**Fault Tree for Sequence 2: PLSRU End State**  
**From a Hydrazine Leak During Ascent,**  
**one APU/HYD Unit has a Detected/Confirmed Leak**  
**and is Recoverable, one Other APU/HYD Unit Fails**



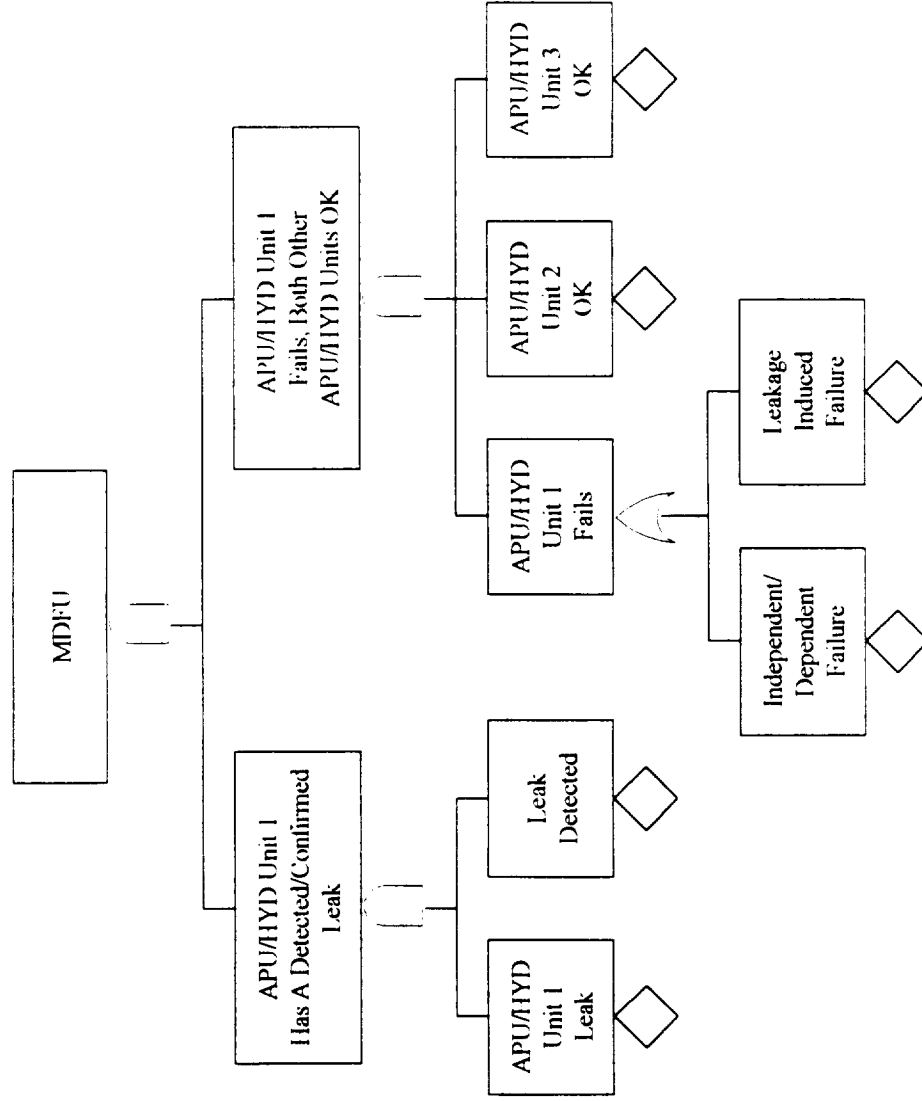
**Fault Tree for Sequence 2: PLSRU End State**  
**From a Hydrazine Leak During Ascent,**  
**one APU/HYD Unit has a Detected/Confirmed Leak**  
**and is Recoverable, one Other APU/HYD Unit Fails**  
**(Continued)**



**Fault Tree for Sequence 3: PLSR2U End State**  
**From a Hydrazine Leak During Ascent, one APU/HYD**  
**Unit has a Detected/Confirmed Leak and is Recoverable,**  
**Both Other APU/HYD Units Fail**

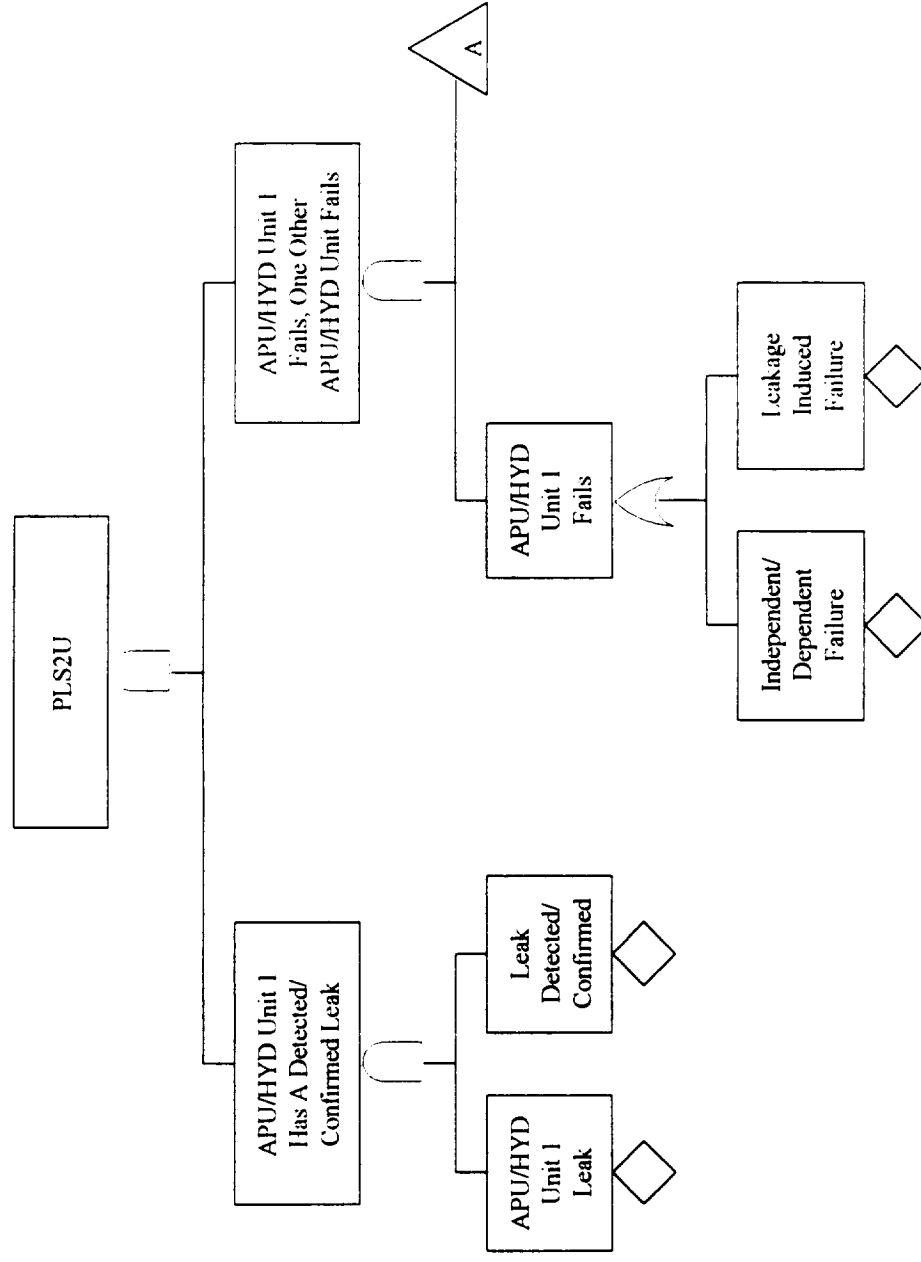


# **Fault Tree for Sequence 4: MDFU End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has a Detected/Confirmed Leak and Subsequent Failure**

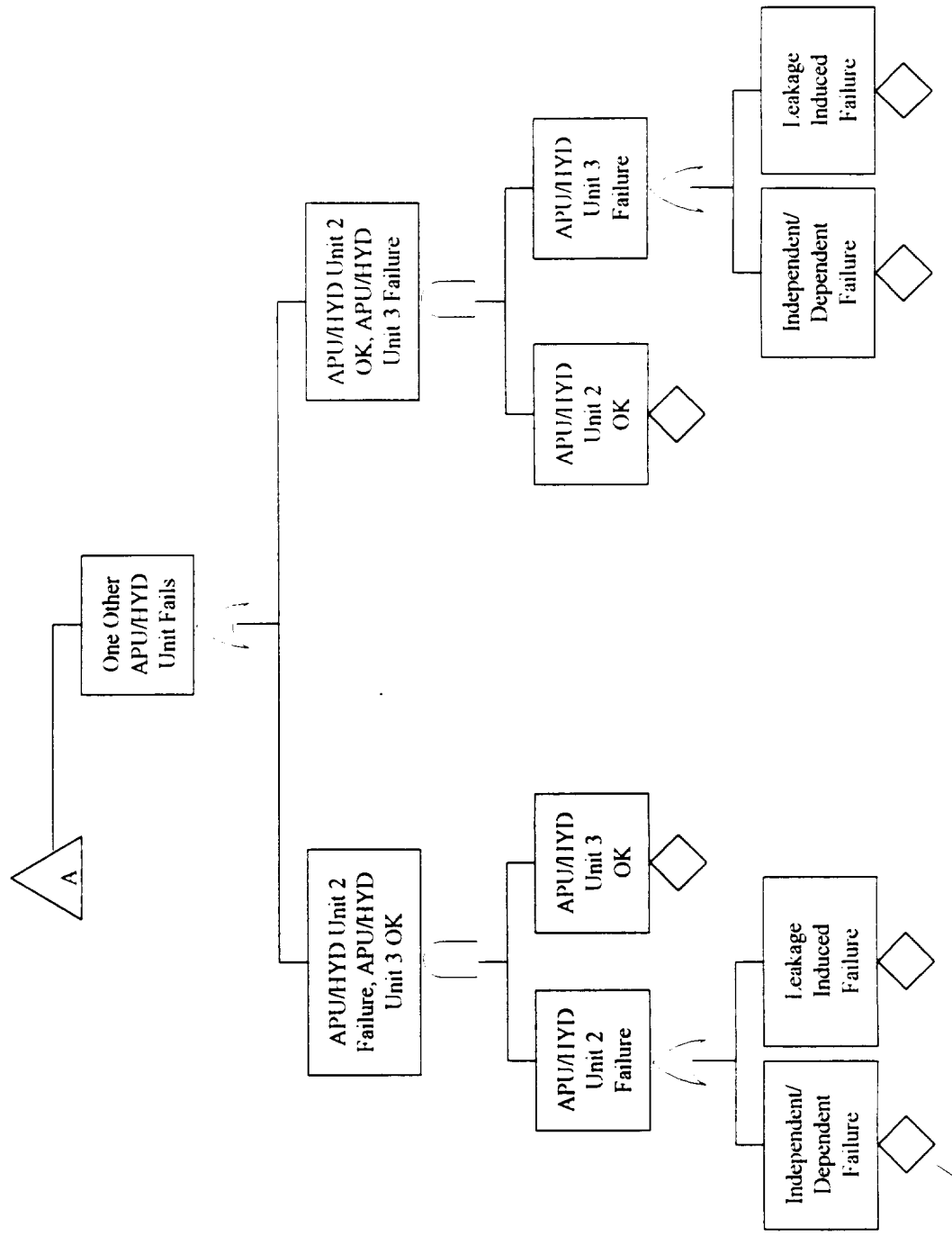




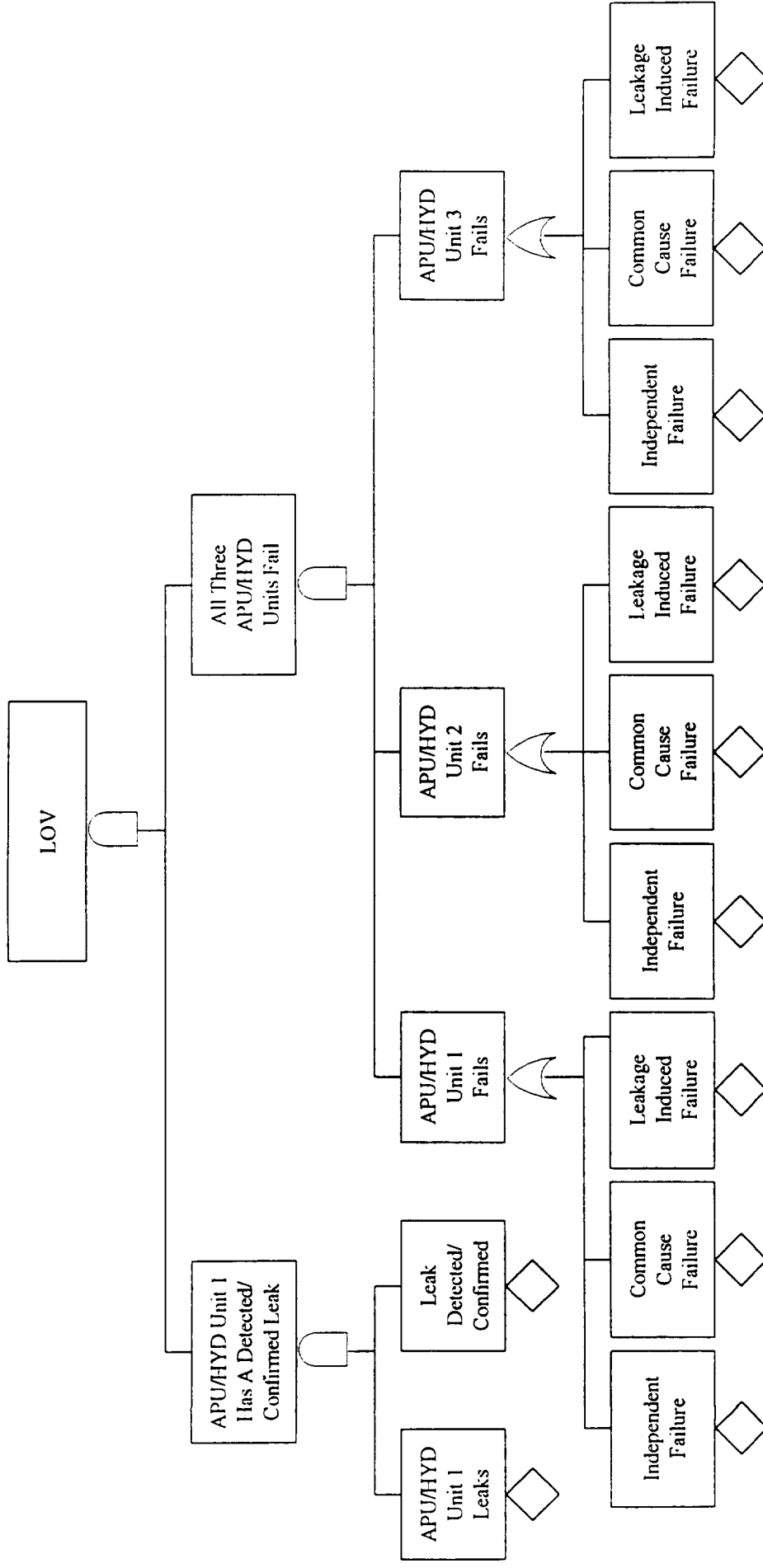
**Fault Tree for Sequence 5: r'LS2U End State From  
a Hydrazine Leak During Ascent, one APU/HYD Unit  
has a Detected/Confirmed Leak and Subsequent Failure,  
one Other APU/HYD Unit Also Fails**



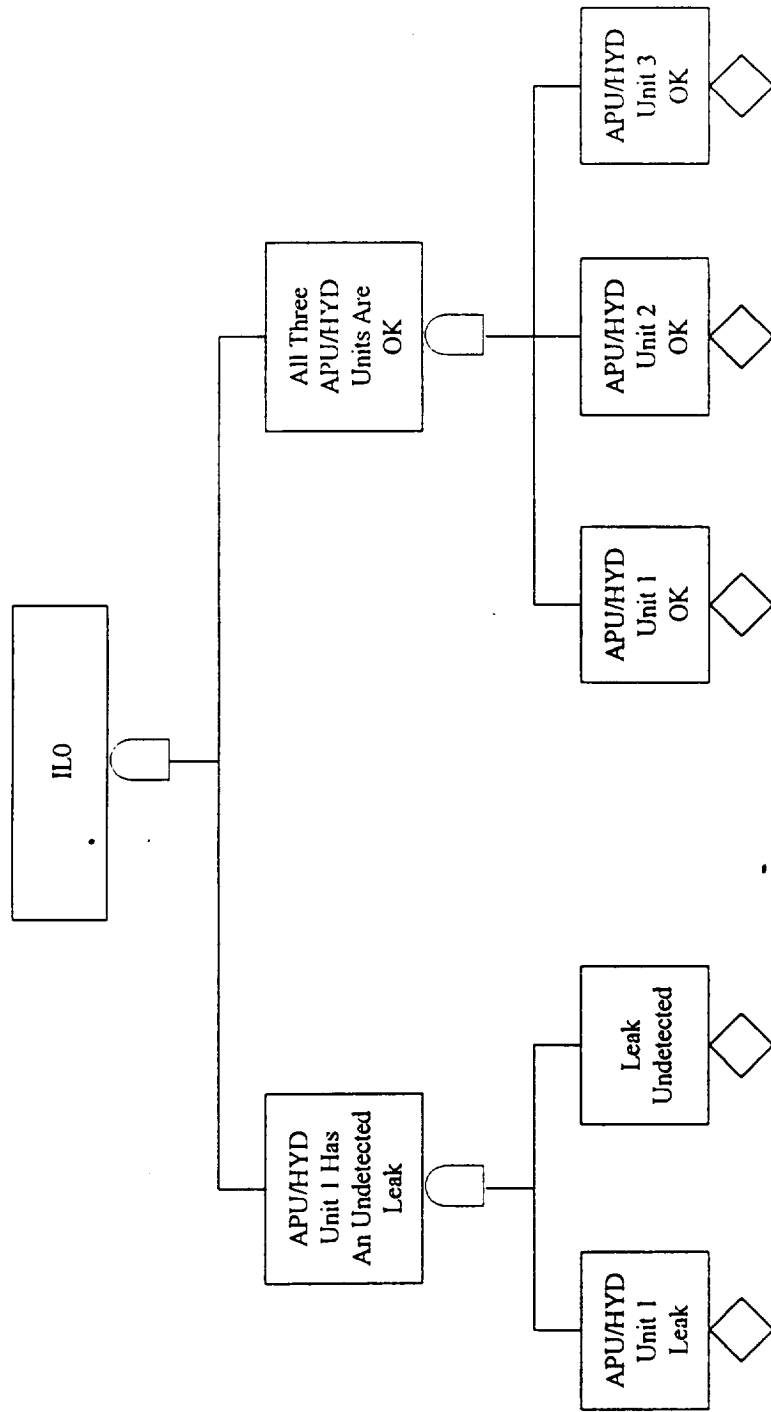
**Fault Tree for Sequence 5: PLS2U End State From a Hydrazine Leak During Ascent, one APU/HYD Unit has a Detected/Confirmed Leak and Subsequent Failure, one Other APU/HYD Unit Also Fails (Continued)**



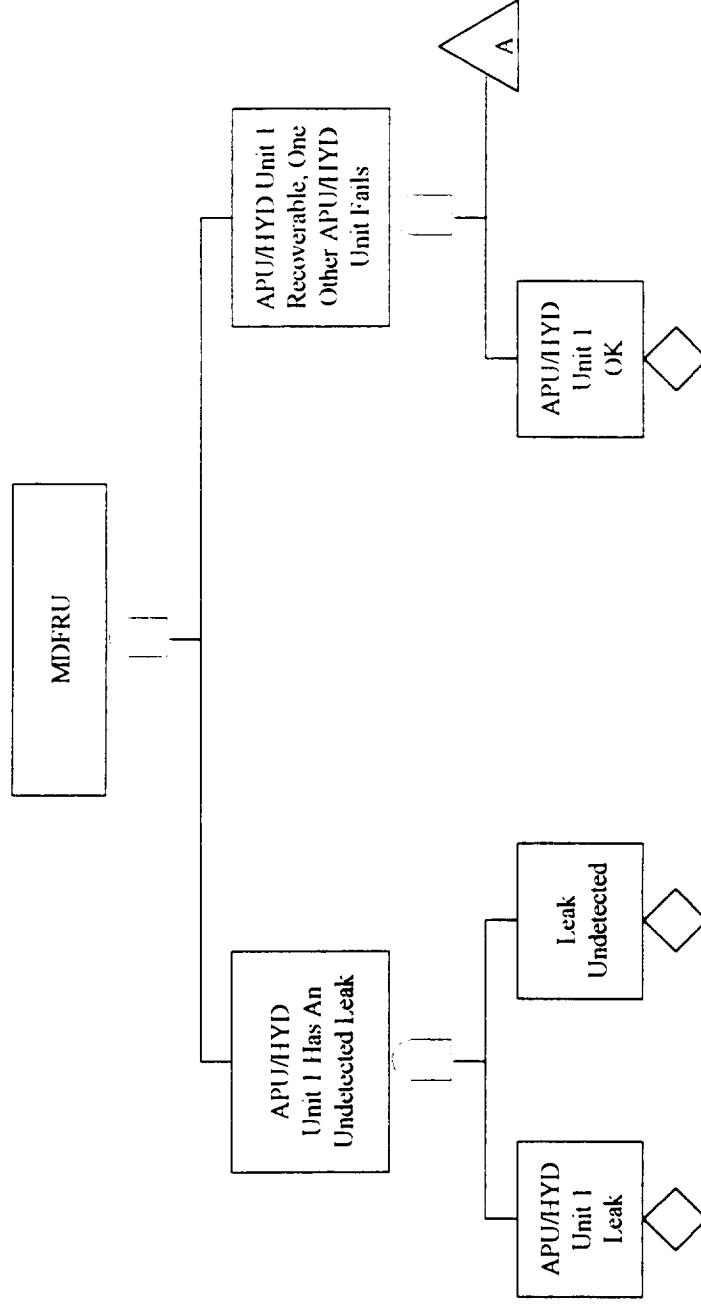
**Fault Tree for Sequence 3: LOV End State From  
a Hydrazine Leak During Ascent, one APU/HYD Unit  
has a Detected/Confirmed Hydrazine Leak and all  
Three APU/HYD Units Have Failures**



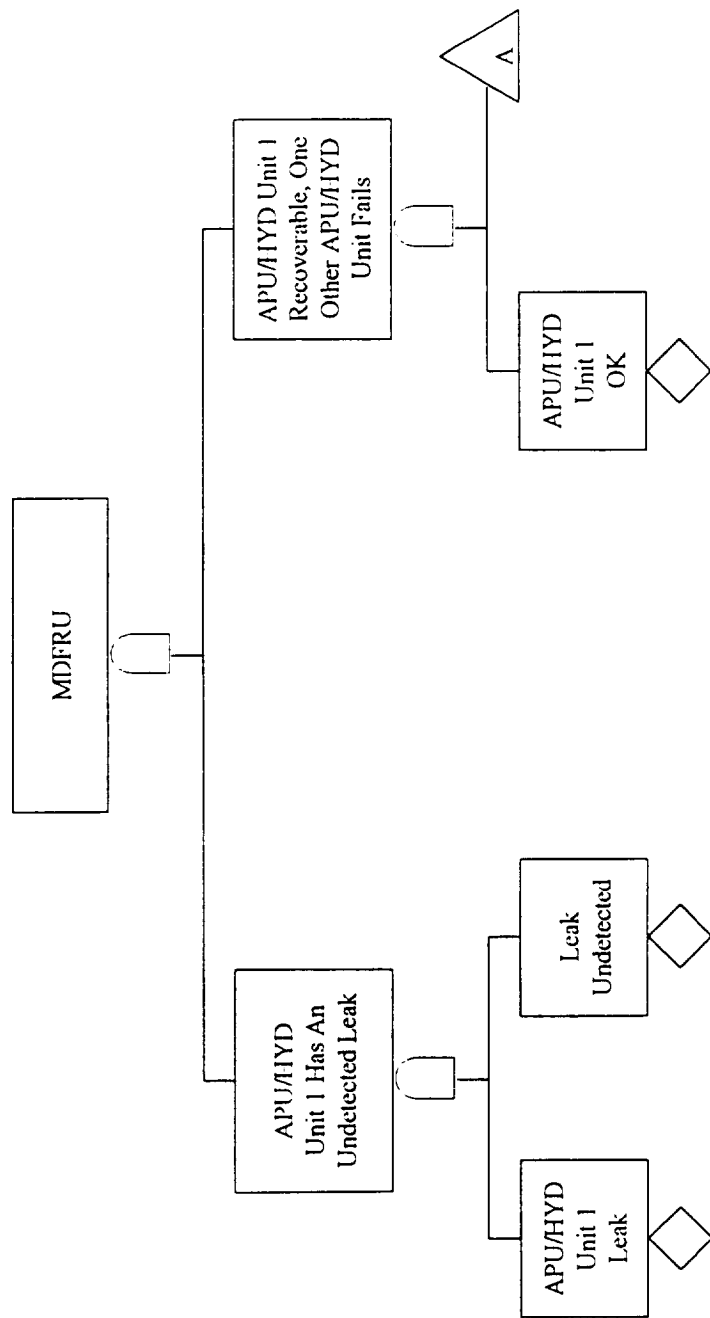
**Fault Tree for Sequence 7: IL0 End State From Hydrazine  
Leak During Ascent, one APU/HYD Unit has an Undetected  
Leak and no APU/HYD Units Have Failures**



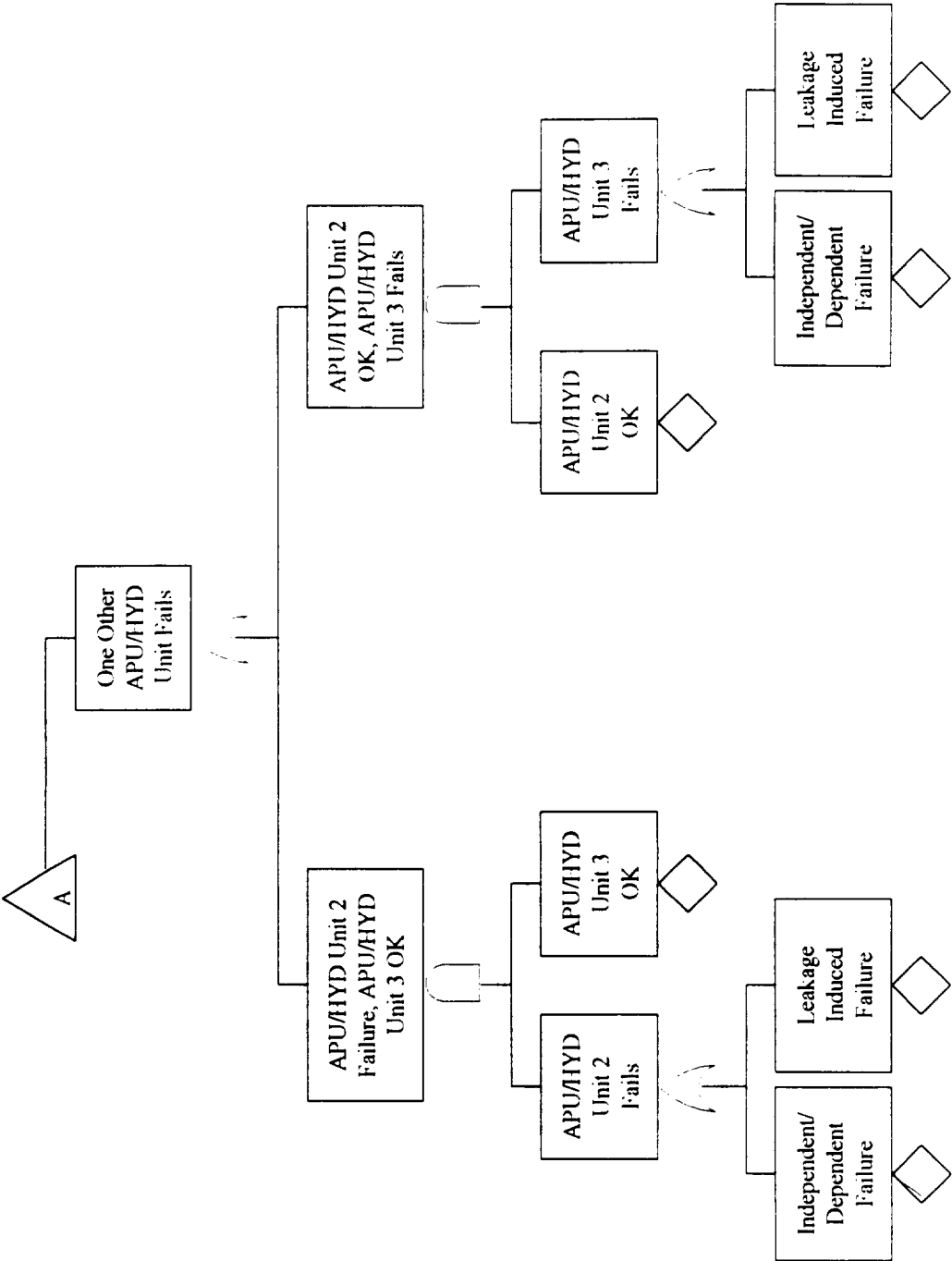
**Fault Tree for Sequence  $\alpha$ : MDRU End State  
From a Hydrazine Leak During Ascent,  
one APU/HYD Unit has an Undetected Leak and is  
Recoverable, one Other APU/HYD Unit Fails**



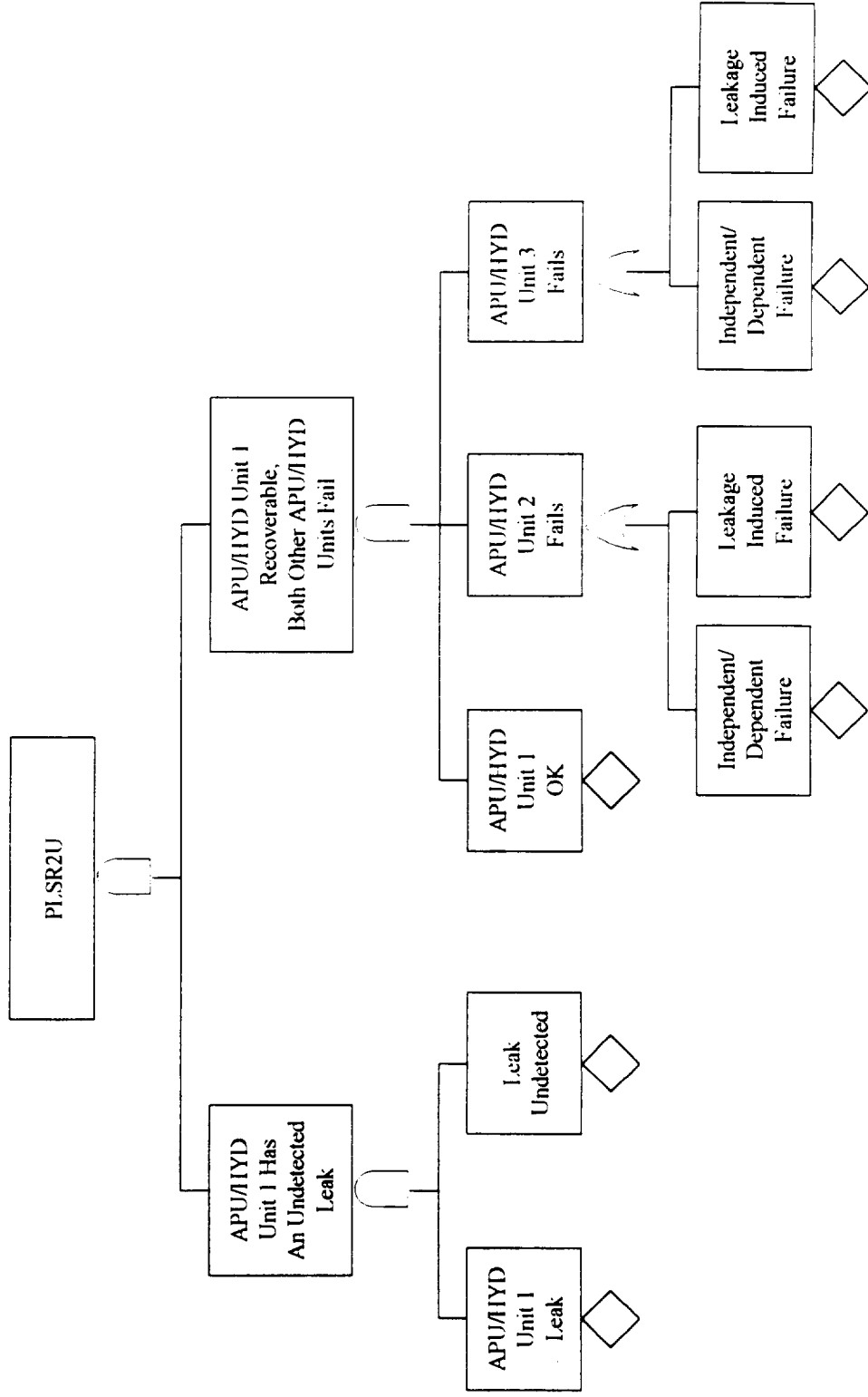
**Fault Tree for Sequence 6: MDRU End State  
From a Hydrazine Leak During Ascent,  
one APU/HYD Unit has an Undetected Leak and is  
Recoverable, one Other APU/HYD Unit Fails**



**Fault Tree for Sequence 8: MDFRU End State**  
**From a Hydrazine Leak During Ascent,**  
**one APU/HYD Unit has an Undetected Leak and is**  
**Recoverable, one Other APU/HYD Unit Fails**  
**(Continued)**

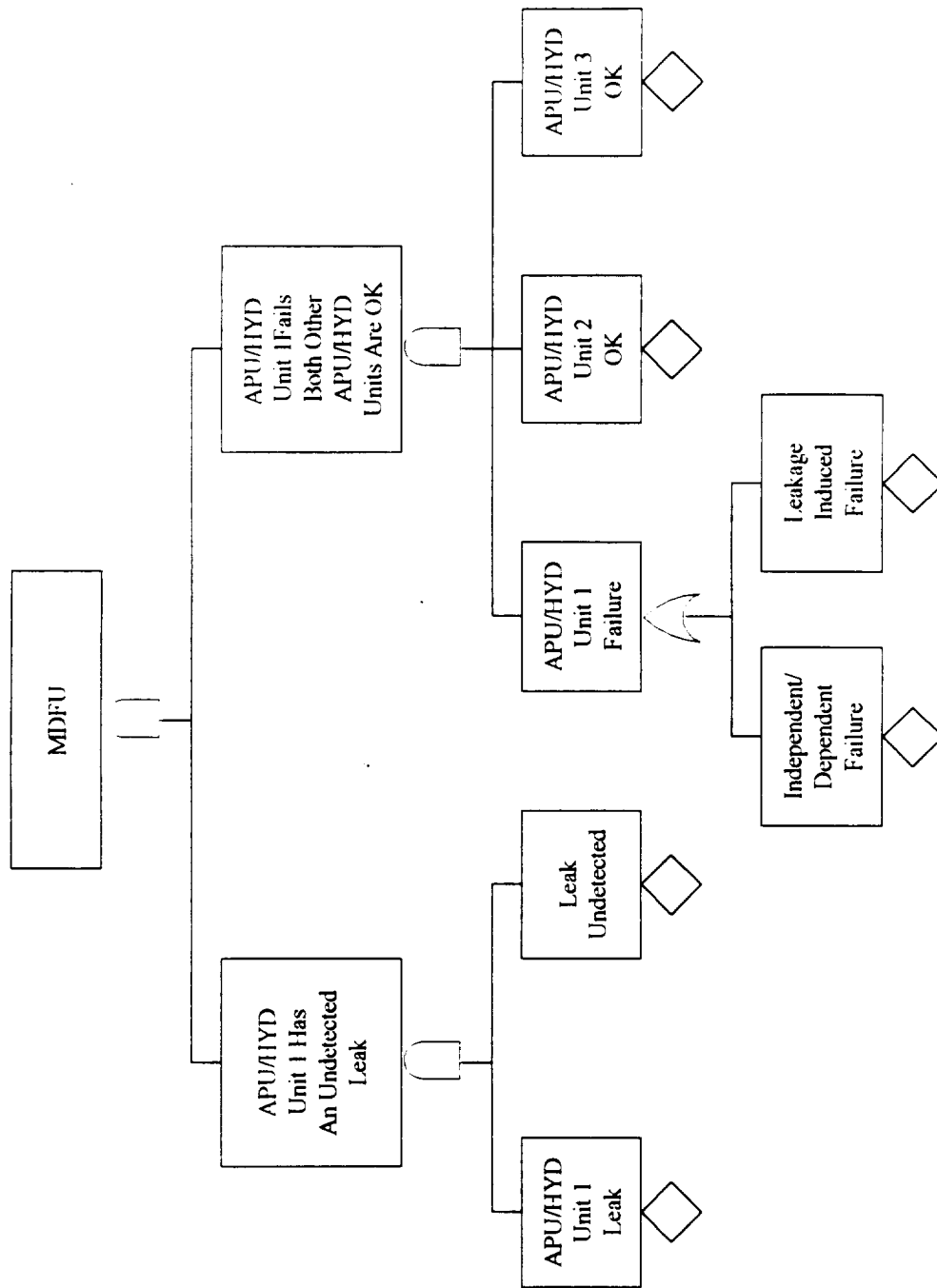


**Fault Tree for Sequence 9: PLSR2U End State**  
**From a Hydrazine Leak During Ascent, one APU/HYD**  
**Unit has an Undetected Leak and is Recoverable, Both Other**  
**APU/HYD Units Fail**

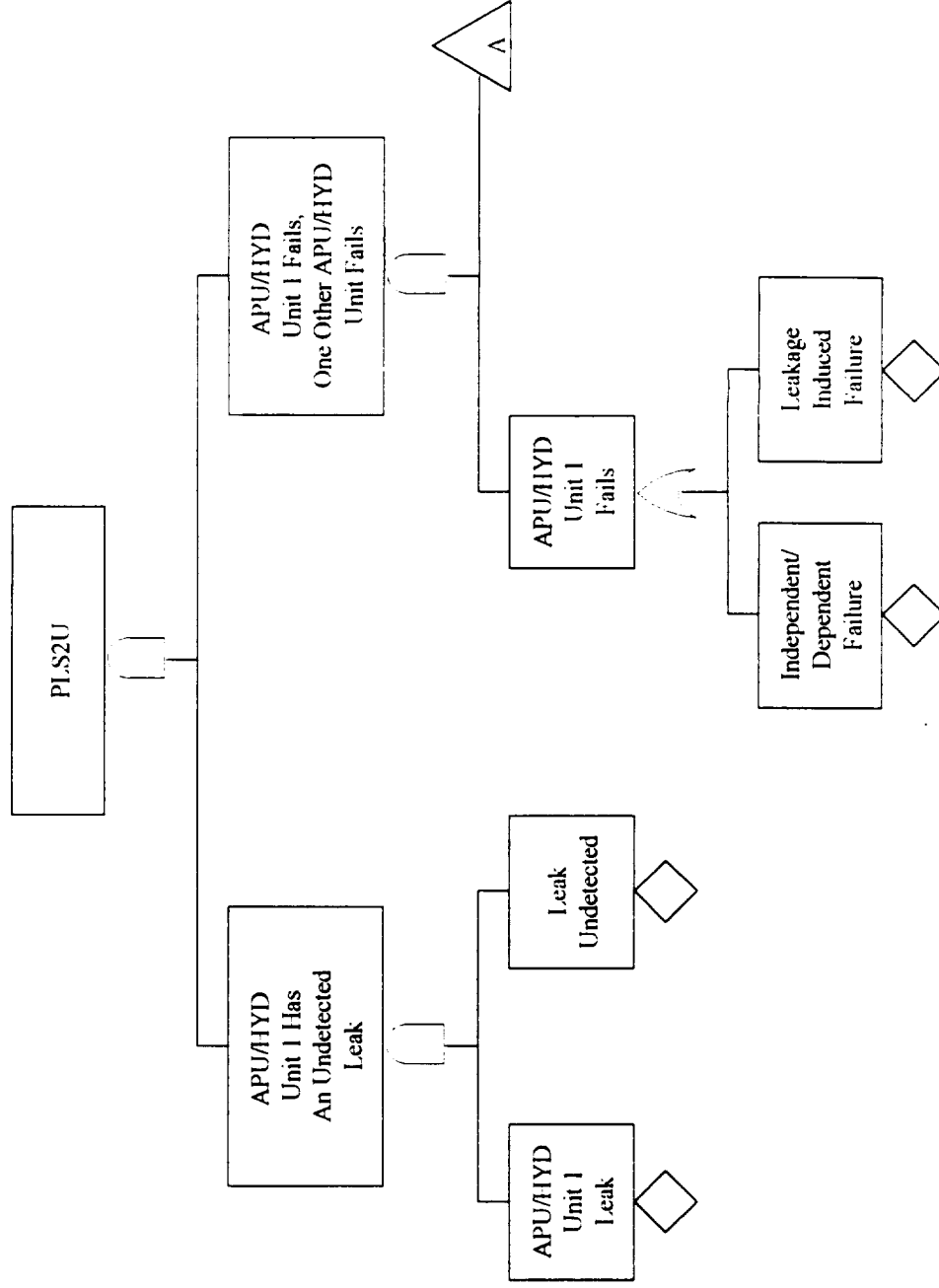




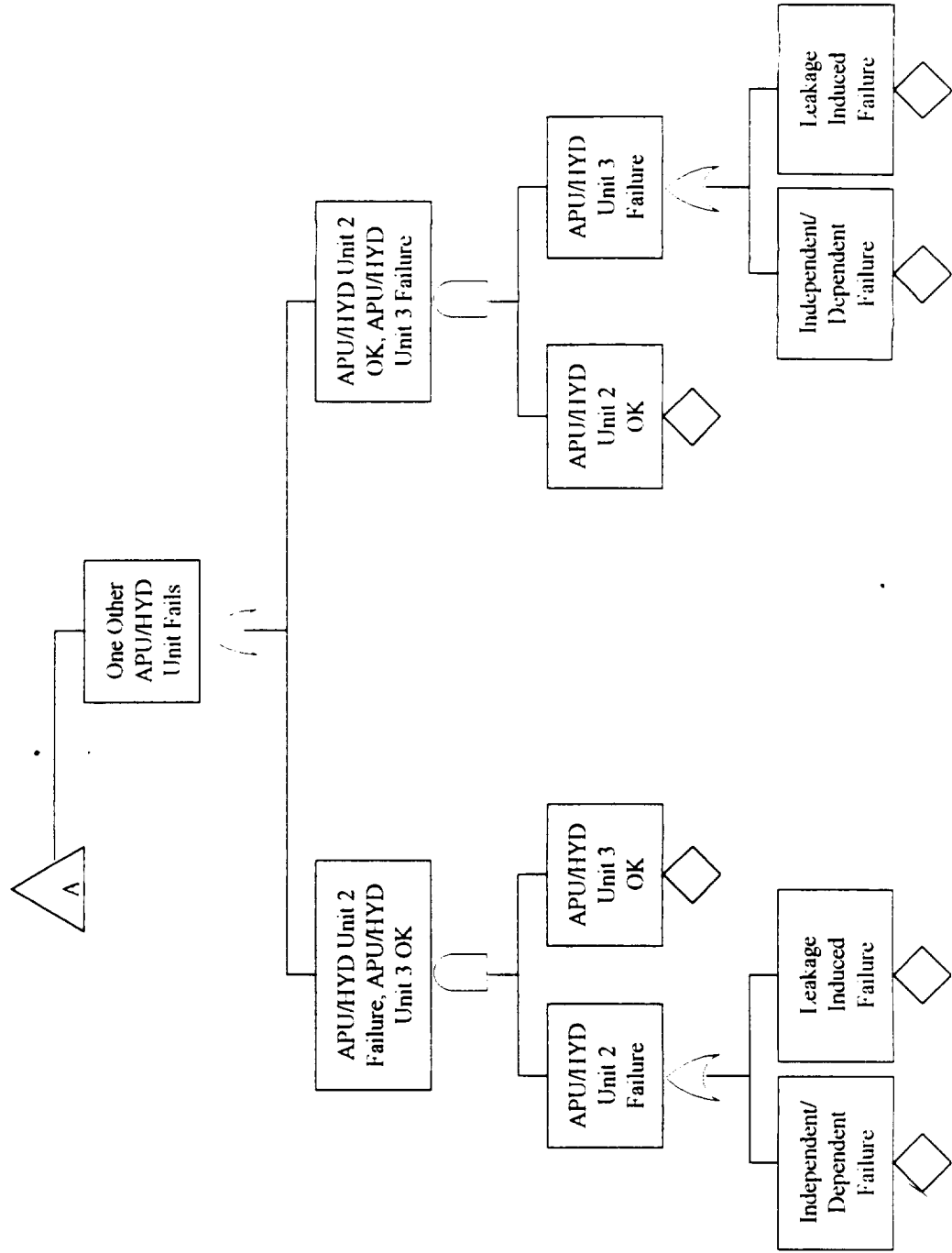
**Fault Tree for Sequence 10: MDFU End State From  
a Hydrazine Leak During Ascent, one APU/HYD Unit has  
an Undetected Leak and Subsequent Failure, no Other  
APU/HYD Units Fail**



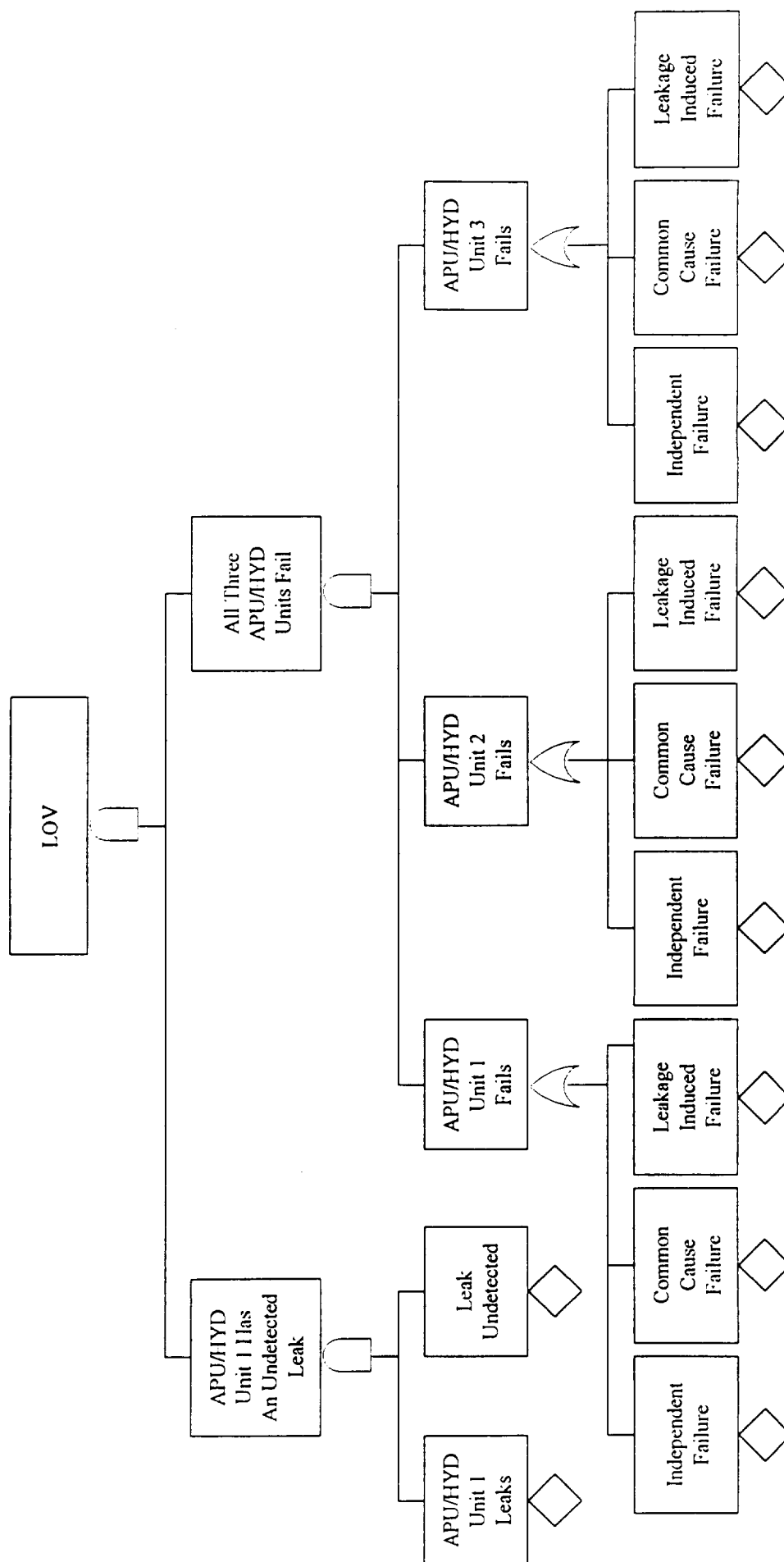
**Fault Tree for Sequence 11: PLS2U End State From  
a Hydrazine Leak During Ascent, one APU/HYD Unit has an  
Undetected Leak and Subsequent Failure, one Other APU/HYD  
Unit Also Fails**



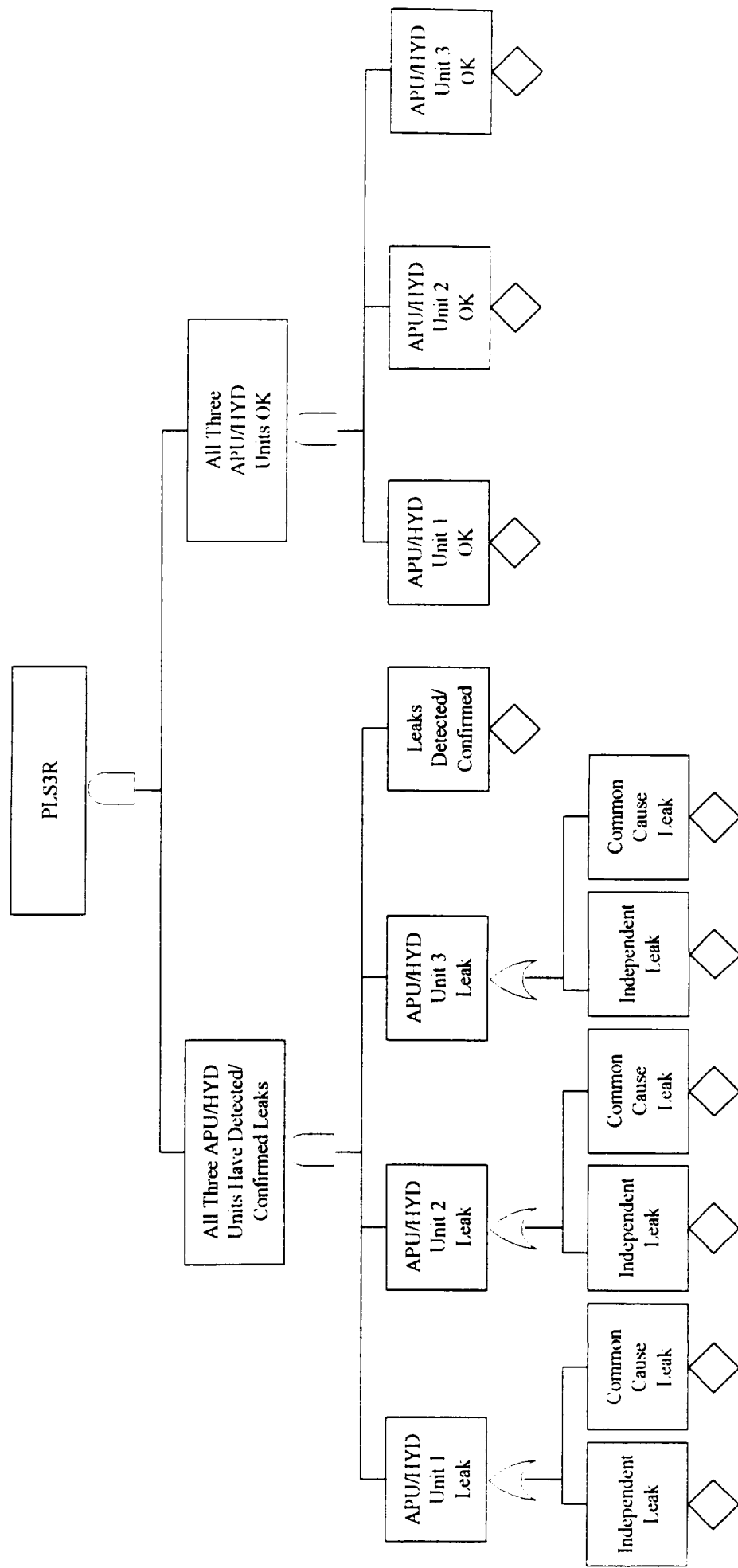
**Fault Tree for Sequence 11: PLS2U End State From  
a Hydrazine Leak During Ascent, one APU/HYD Unit has an  
Undetected Leak and Subsequent Failure, one Other APU/HYD  
Unit Also Fails (Continued)**



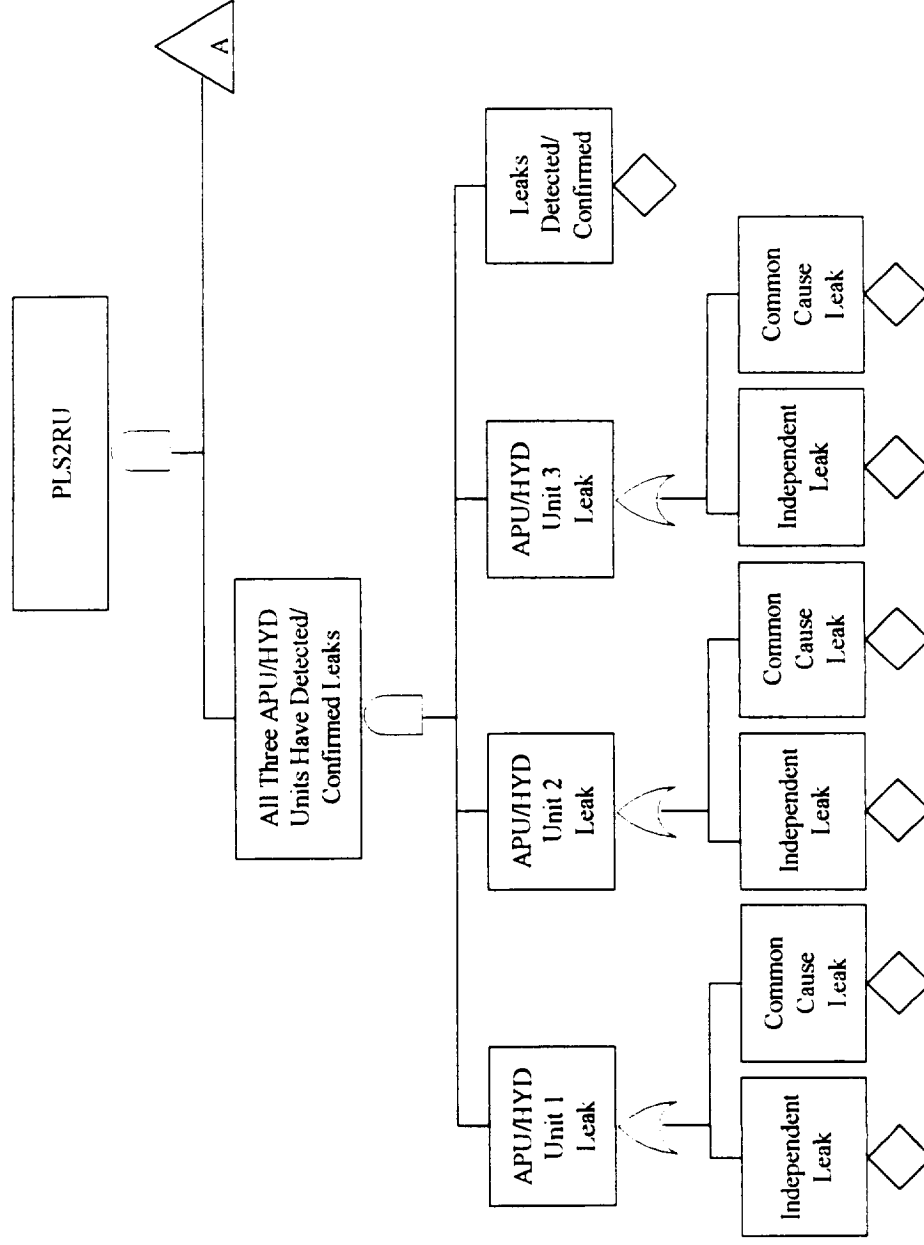
**Fault Tree for Sequence 12. LOV End State From  
a Hydrazine Leak During Ascent, one APU/HYD Unit  
has an Undetected Leak and all Three APU/HYD Units Fail**



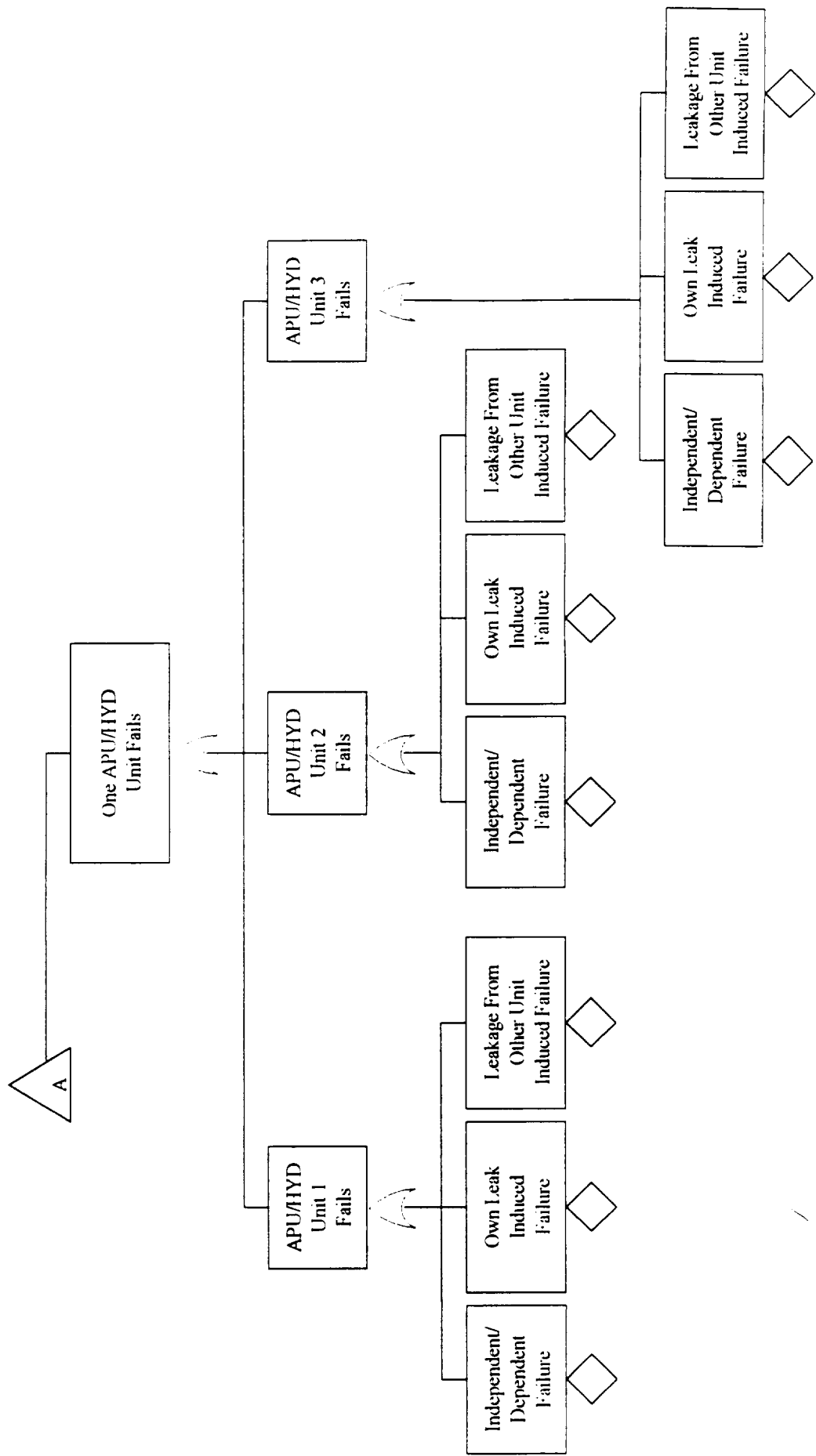
**Fault Tree for Sequence 13: PLS3R End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Detected/Confirmed Leaks and no Failures**



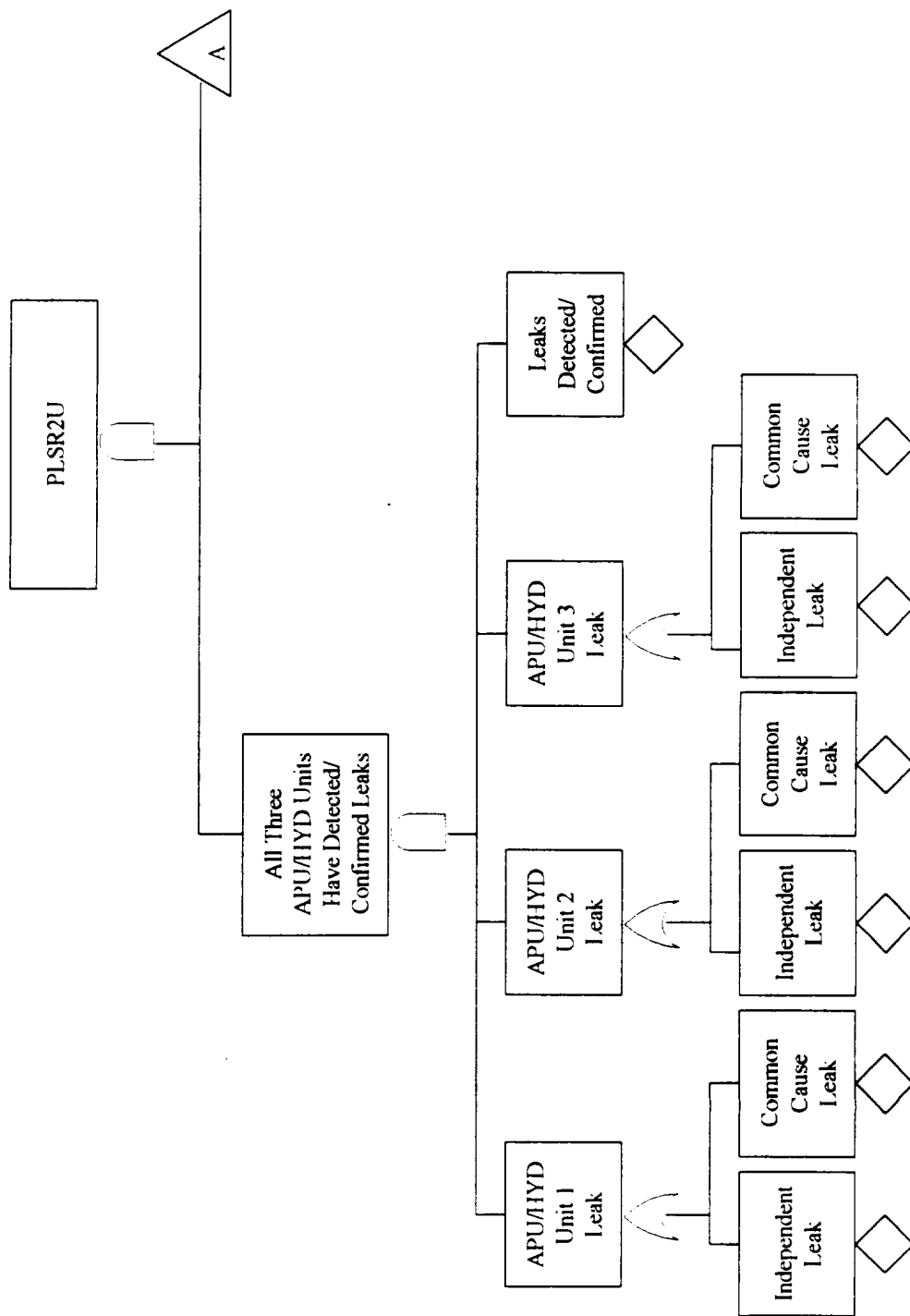
**Fault Tree for Sequence 14: PLS2RU End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Detected/Confirmed Leaks and one APU/HYD Unit Fails**



**Fault Tree for Sequence 14: PLS2RU End State From a  
Hydrazine Leak During Ascent, all Three APU/HYD Units  
Have Detected/Confirmed Leaks and one APU/HYD Unit Fails  
(Continued)**

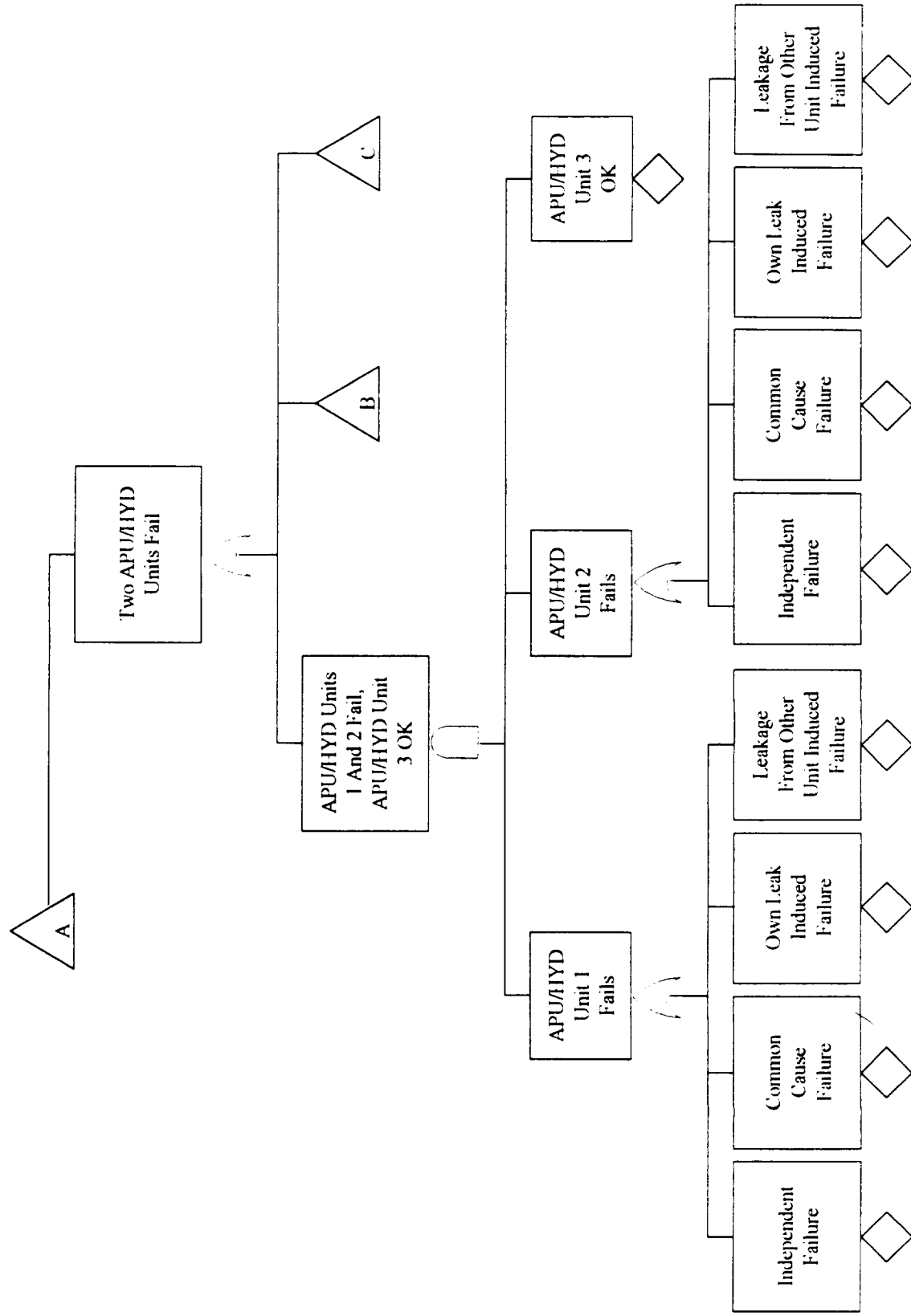


**Fault Tree for Sequence 15: PLSR2U End State From  
Hydrazined Leak During Ascent, all Three APU/HYD Units  
Have Detected/Confirmed Leaks, two APU/HYD Units Fail**

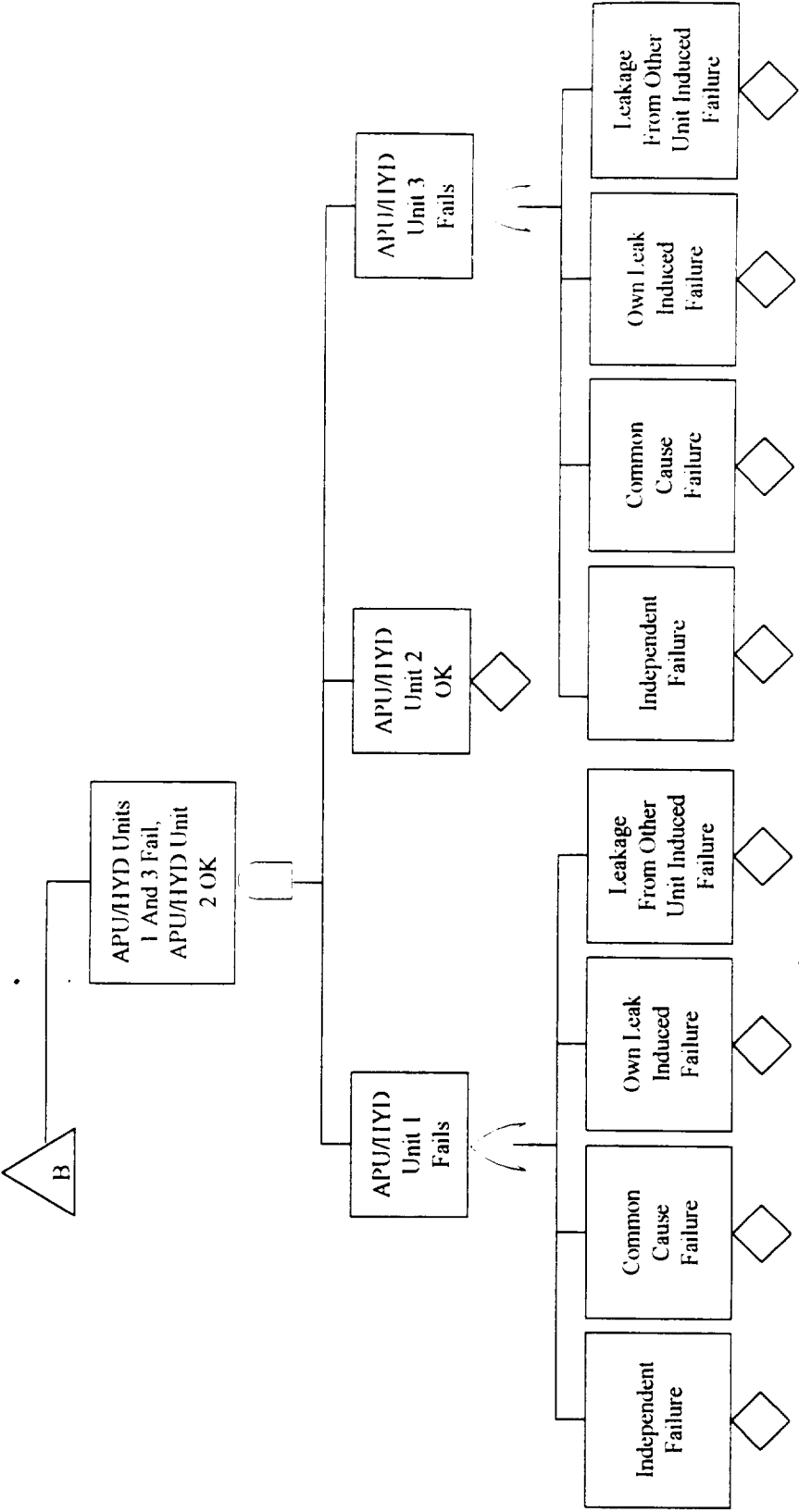




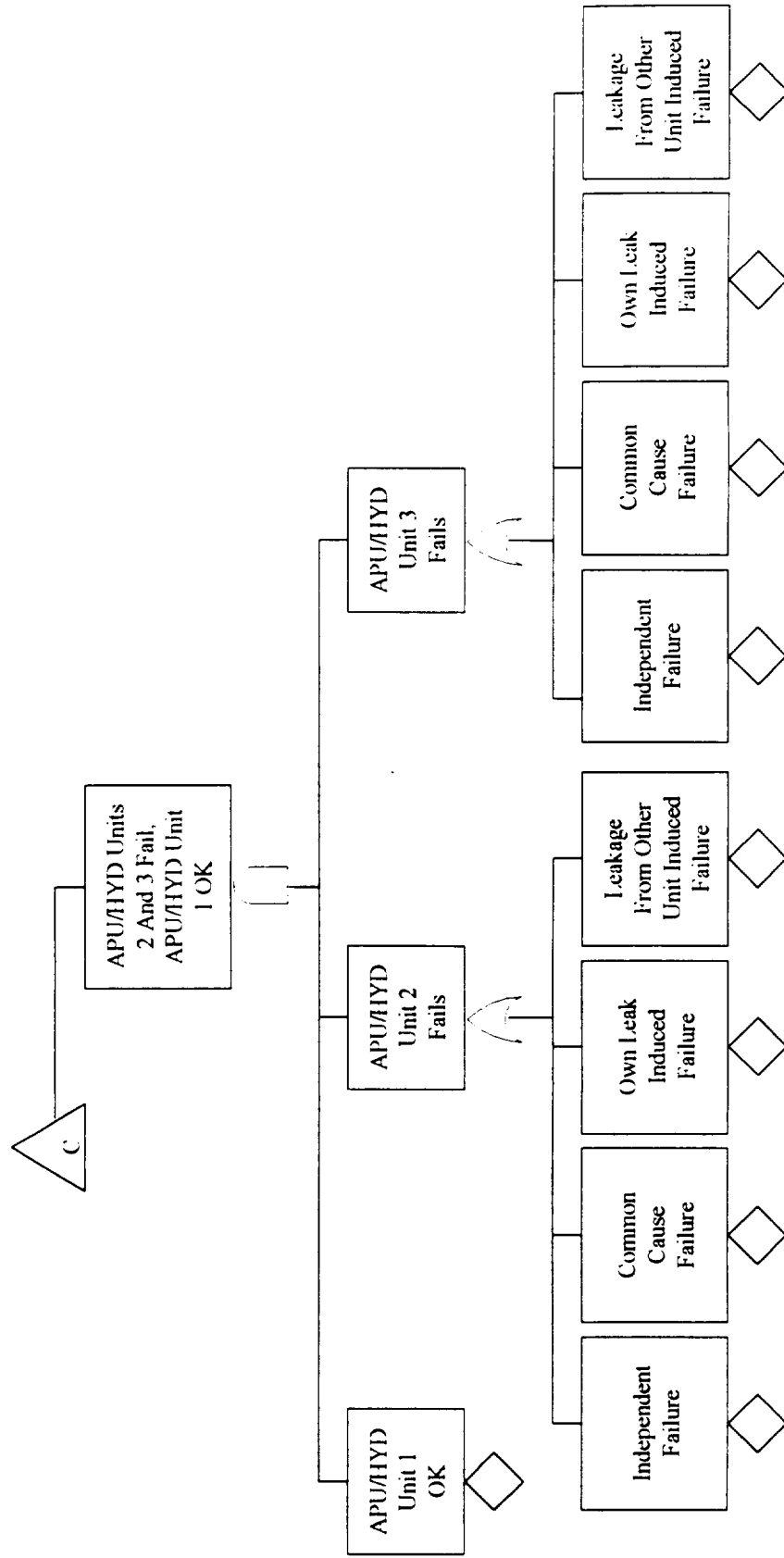
**Fault Tree for Sequence 1b: PLSR2U End State From  
Hydrazined Leak During Ascent, all Three APU/HYD Units  
Have Detected/Confirmed Leaks, two APU/HYD Units Fail  
(Continued)**



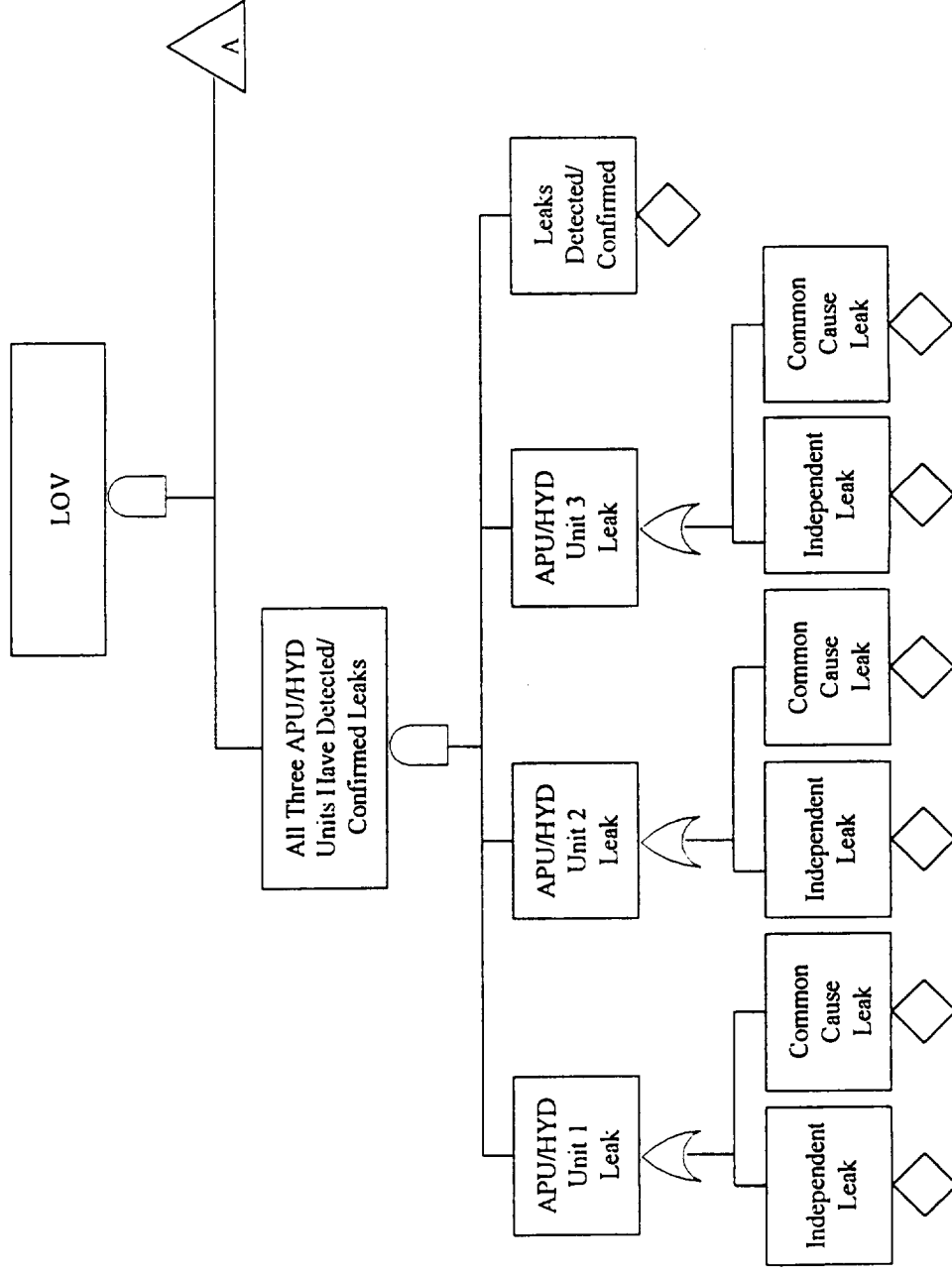
**Fault Tree for Sequence 15: PLSR2U End State From  
Hydrazined Leak During Ascent, all Three APU/HYD Units  
Have Detected/Confirmed Leaks, two APU/HYD Units Fail  
(Continued)**



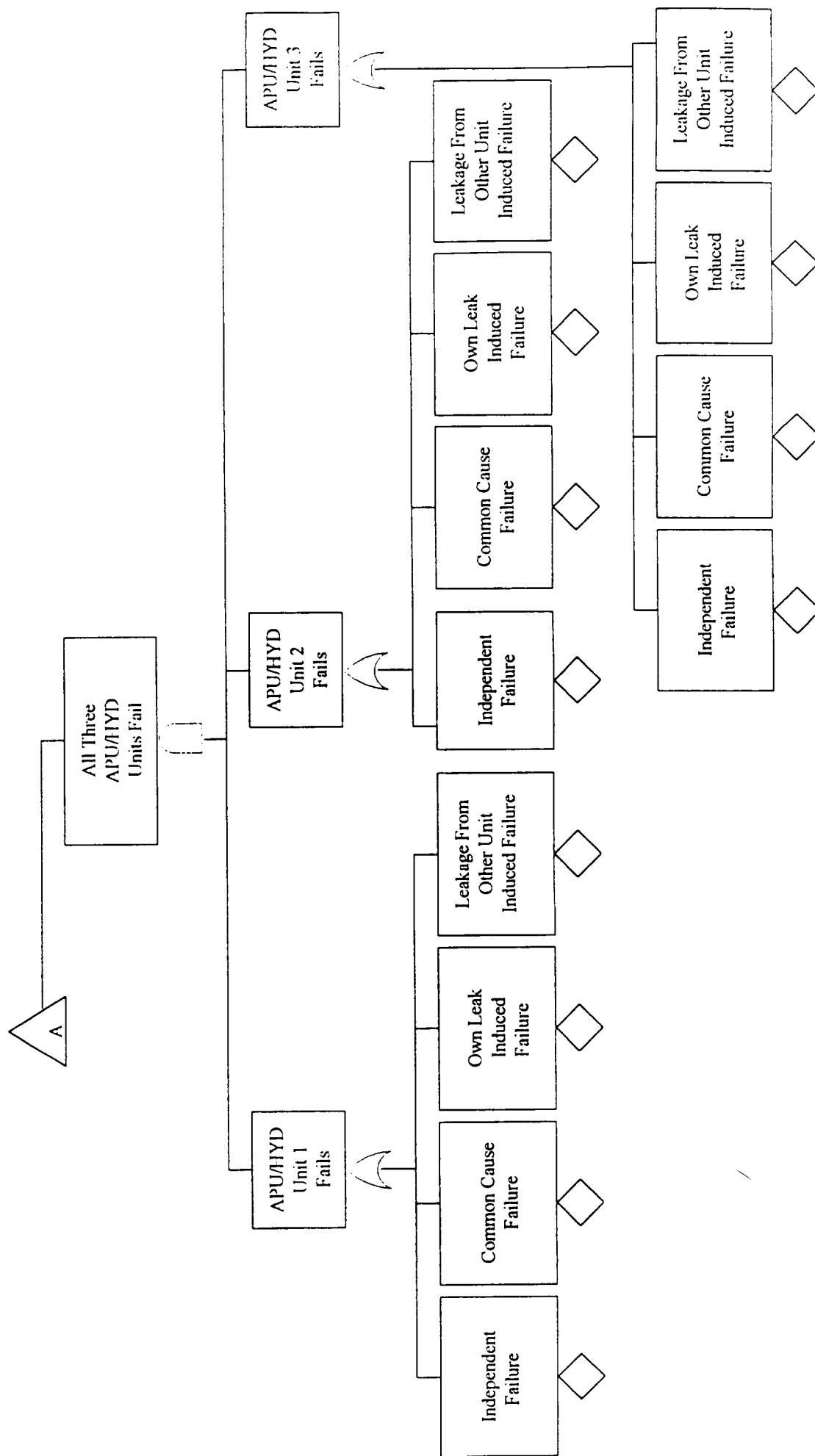
**Fault Tree for Sequence 15: PLSR2U End State From  
Hydrazined Leak During Ascent, all Three APU/HYD Units  
Have Detected/Confirmed Leaks, two APU/HYD Units Fail  
(Continued)**



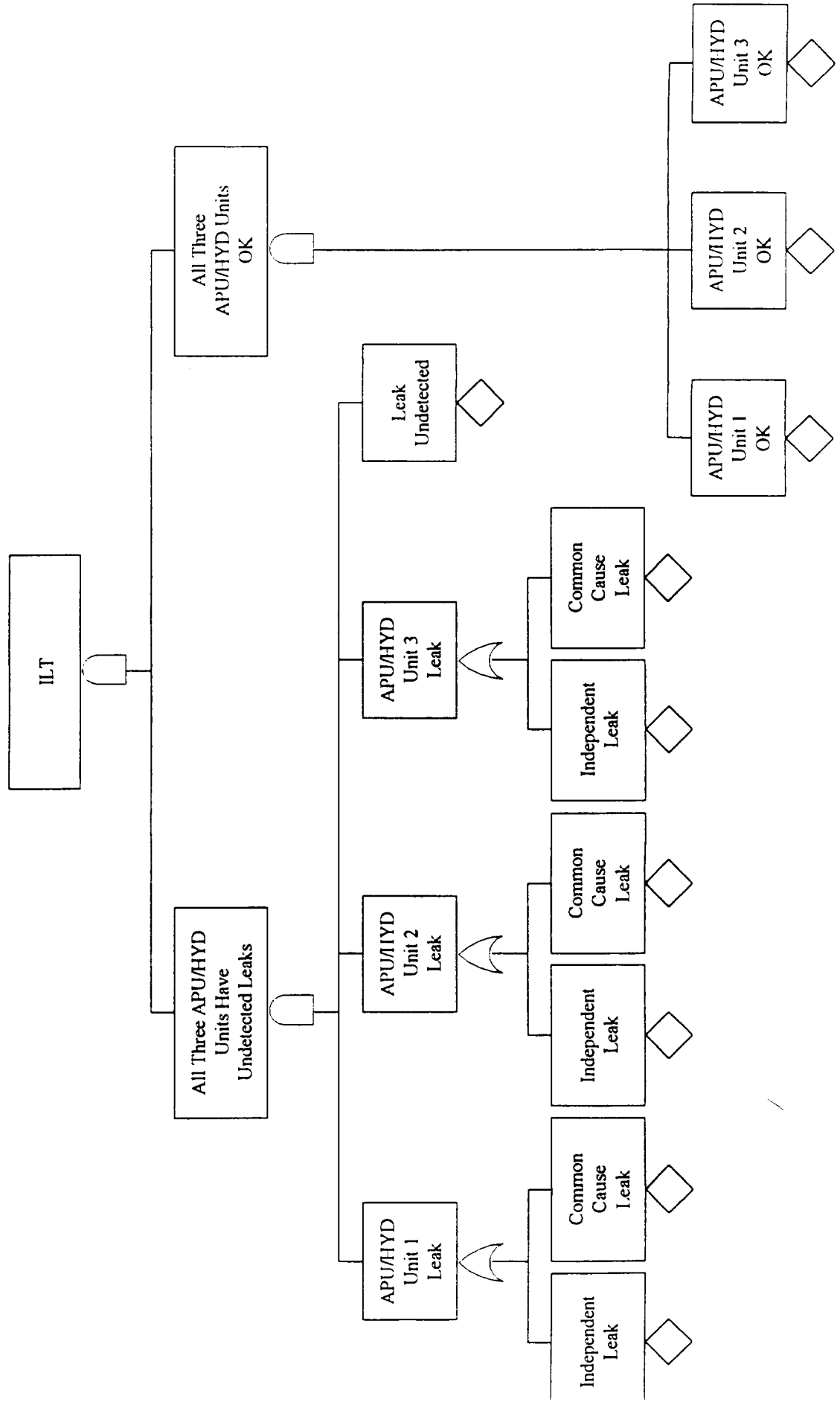
**Fault Tree for Sequence 16: LOV End State From Hydrazine Leak During Ascent, all Three APU/HYD Units Have Detected/Confirmed Leaks and all Three APU/HYD Units Fail**



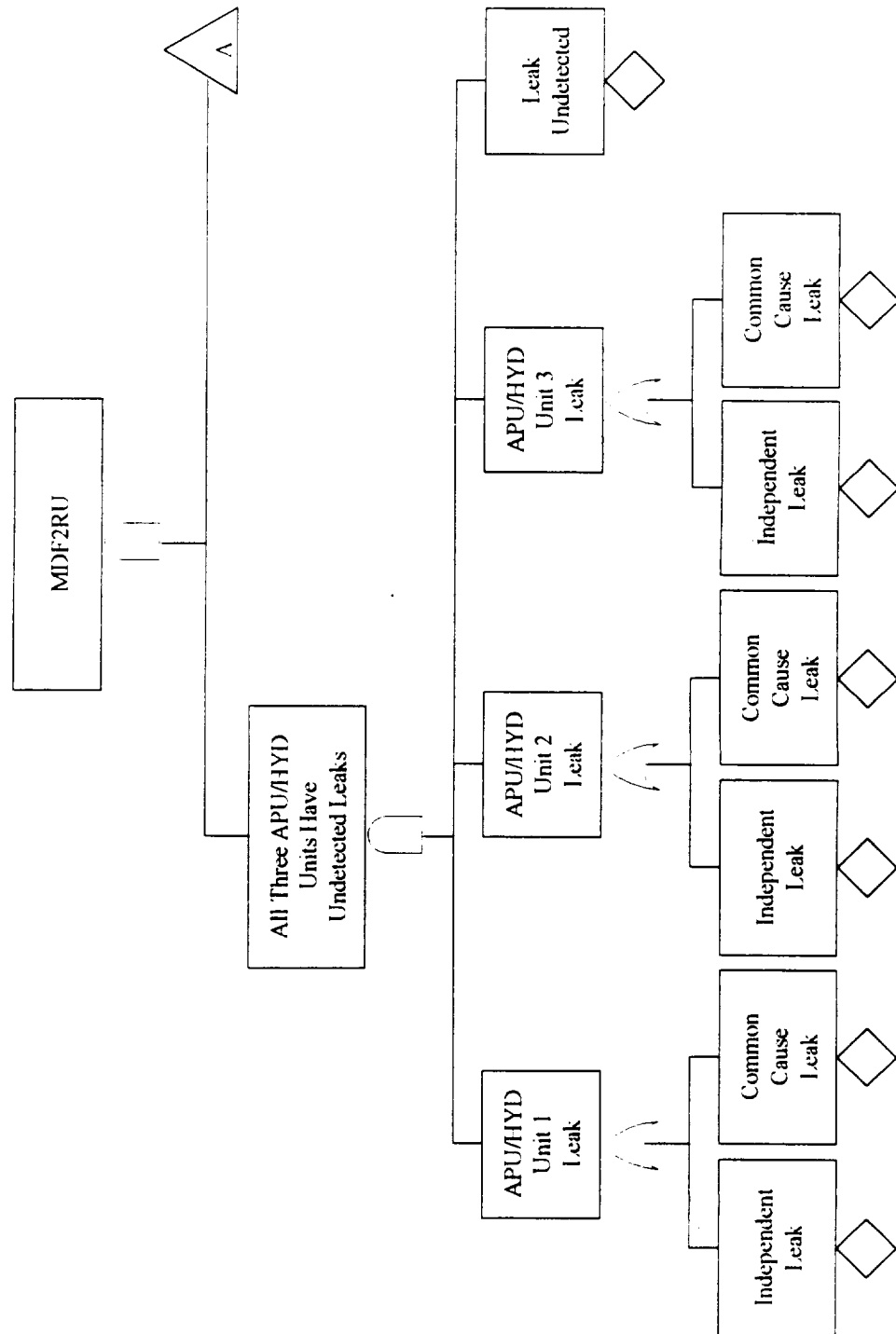
**Fault Tree for Sequence 16: LOV End State From Hydrazine  
Leak During Ascent, all Three APU/HYD Units Have Detected/  
Confirmed Leaks and all Three APU/HYD Units Fail  
(Continued)**



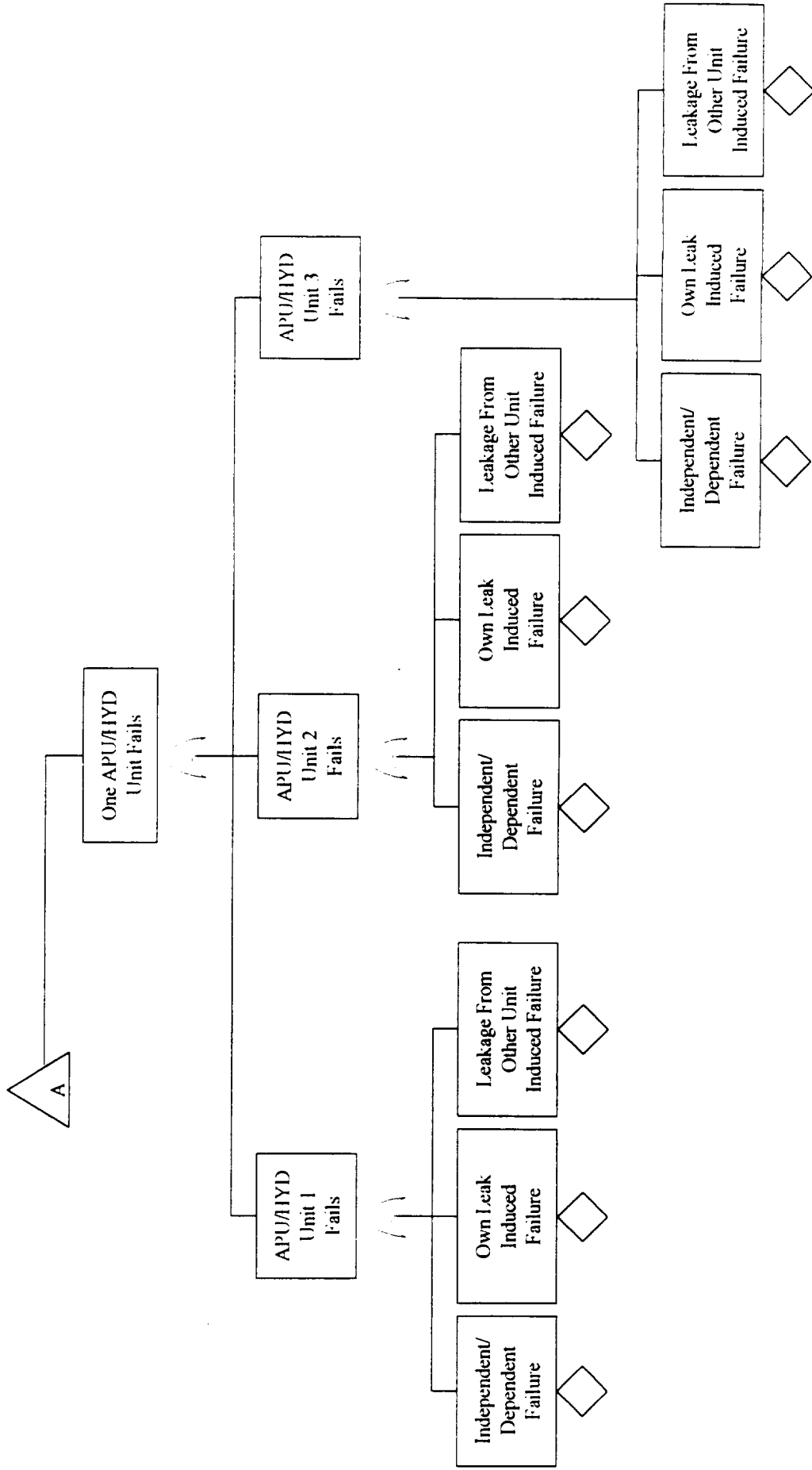
# **Fault Tree for Sequence 17: ILT End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks and no Failures**



**Fault Tree for Sequence 18: MDF2RU End State From a Hydrazine Leak During Ascent, one APU/HYD Unit Fails**

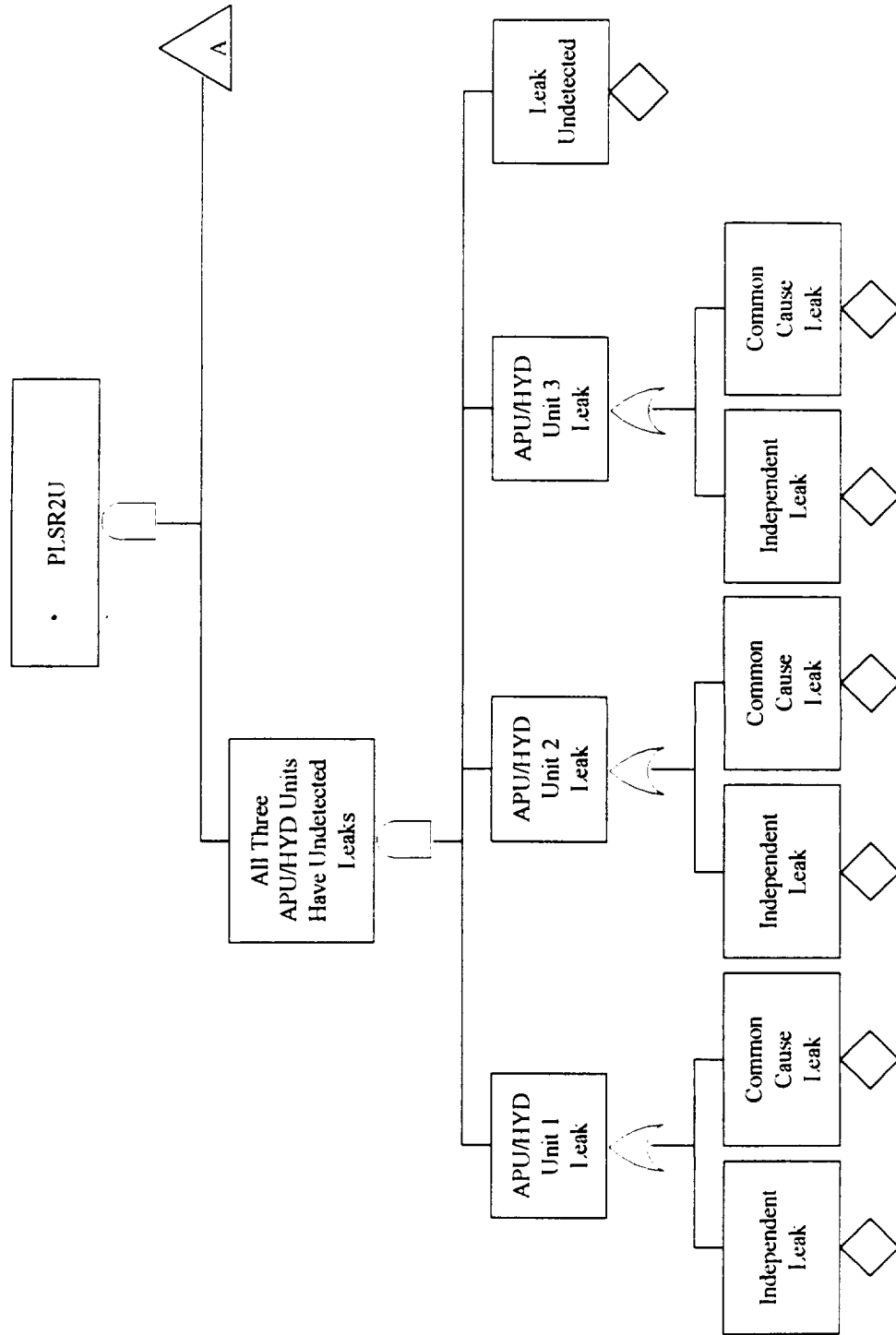


**Fault Tree for Sequence 18: MDF2RU End State  
From a Hydrazine Leak During Ascent, one  
APU/HYD Unit Fails (Continued)**

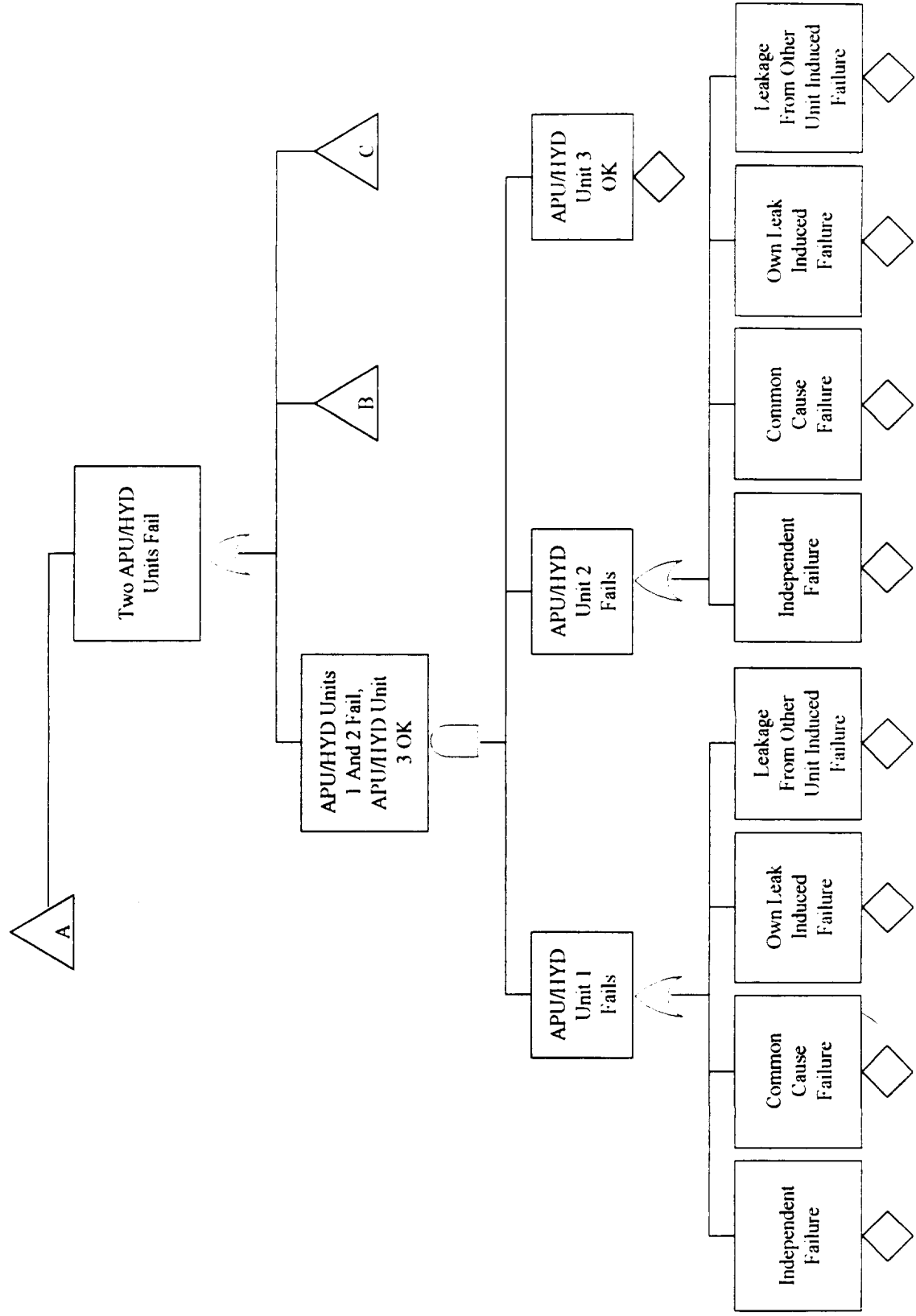




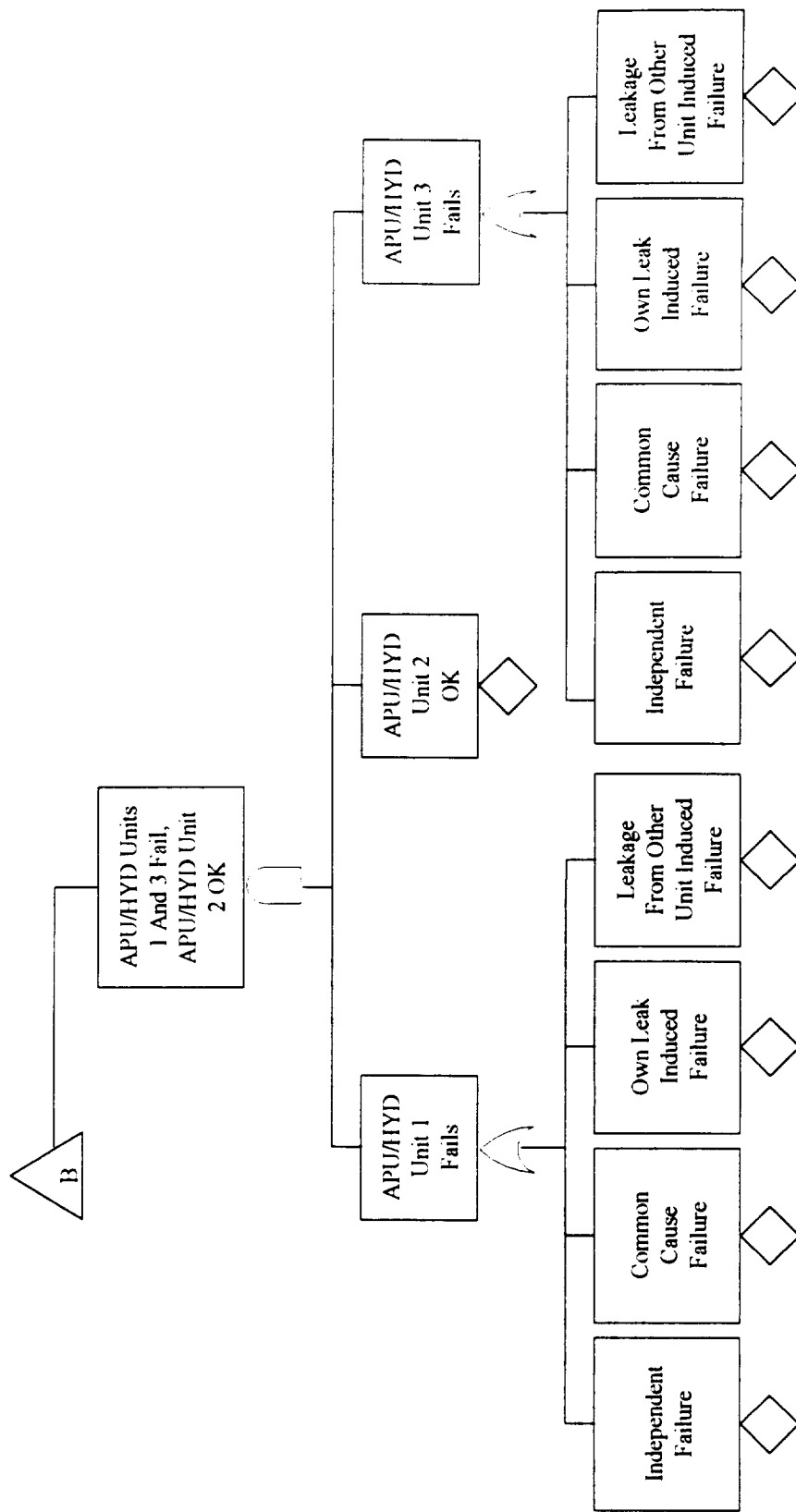
**Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail**



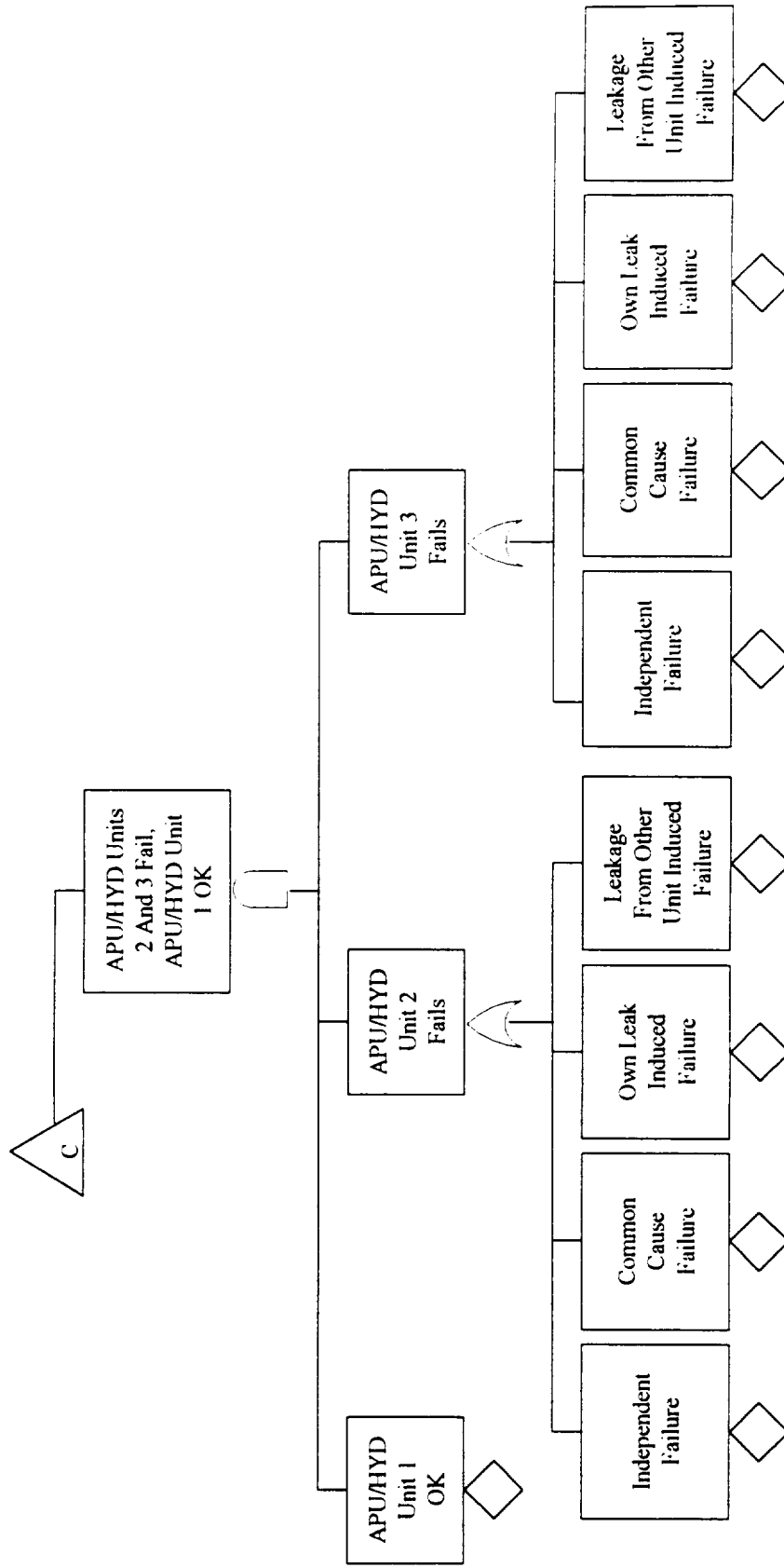
**Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail (Continued)**



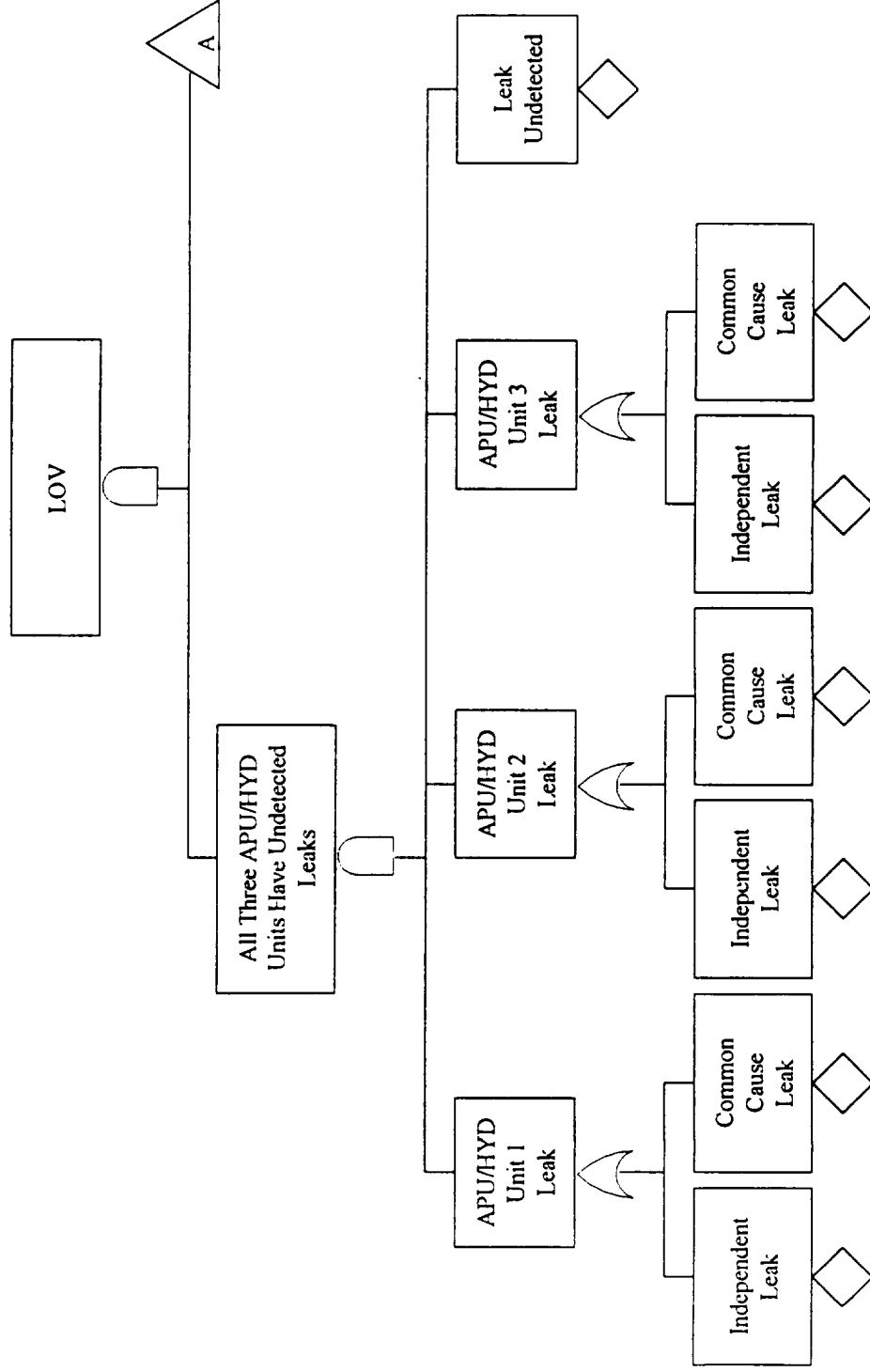
**Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail (Continued)**



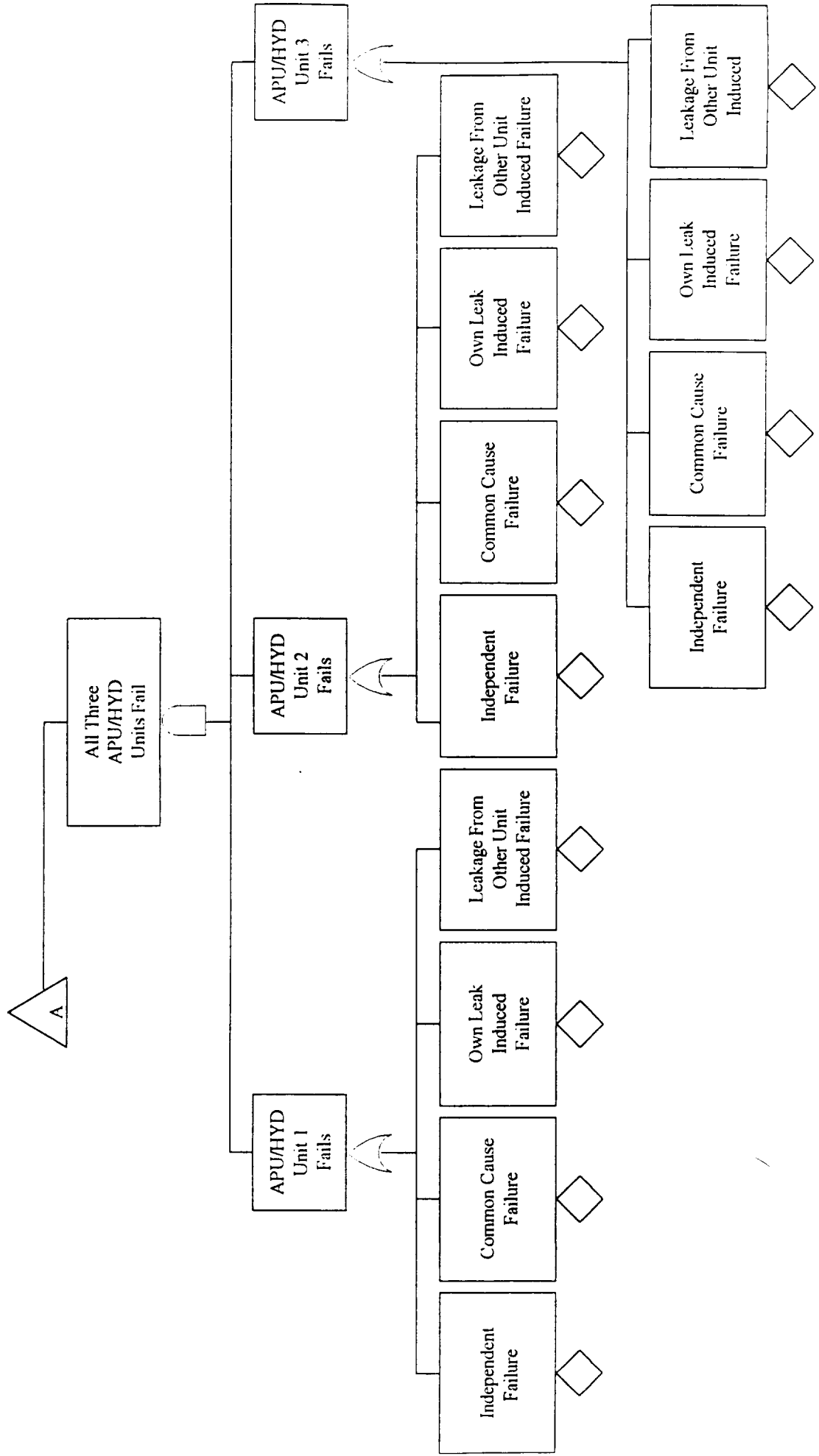
**Fault Tree for Sequence 19: PLSR2U End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Have Undetected Leaks, two APU/HYD Units Fail (Continued)**



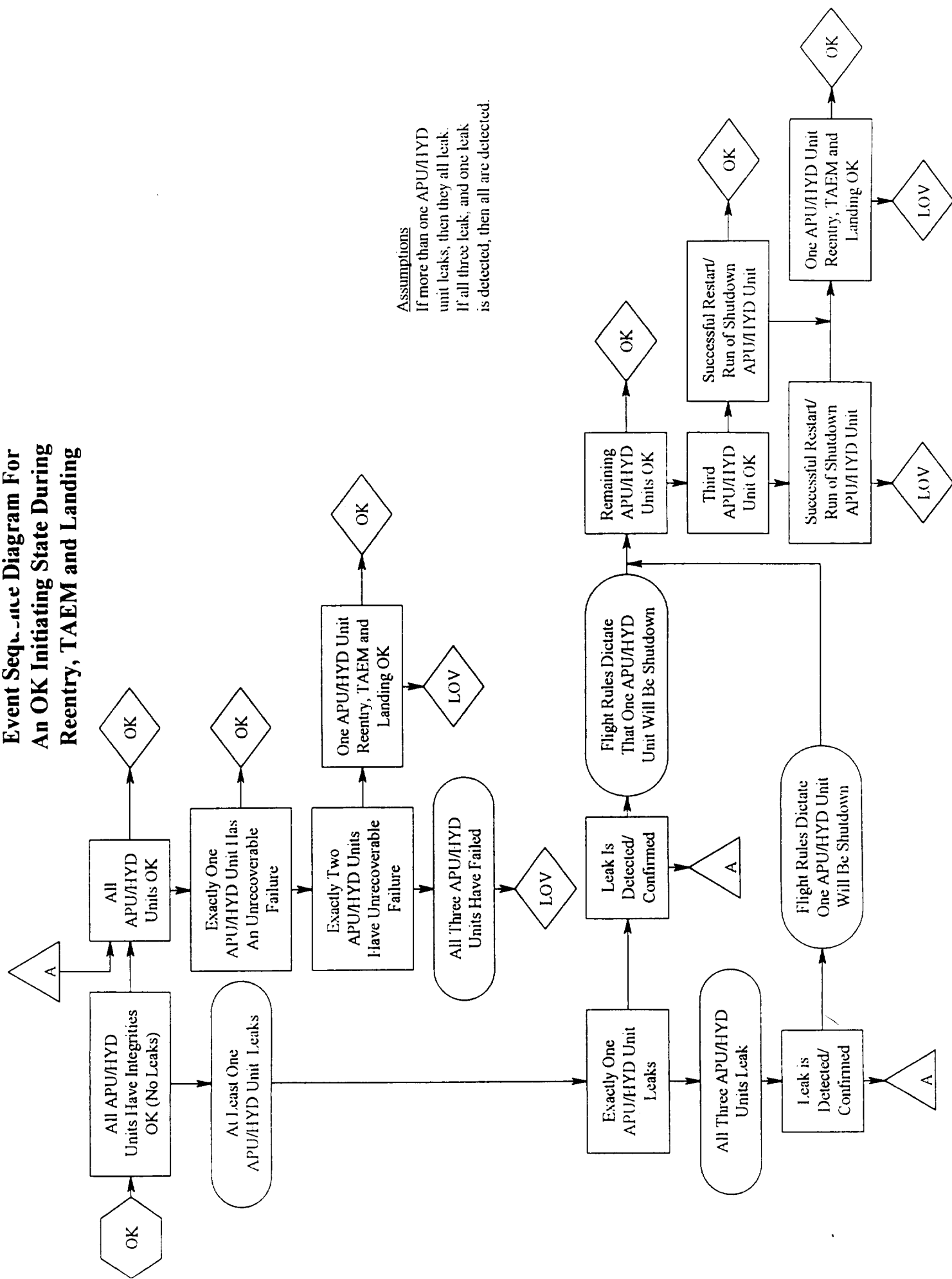
**Fault Tree for Sequence 20: LOV End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Fail**



# **Fault Tree for Sequence 20: LOV End State From a Hydrazine Leak During Ascent, all Three APU/HYD Units Fail** **(Continued)**



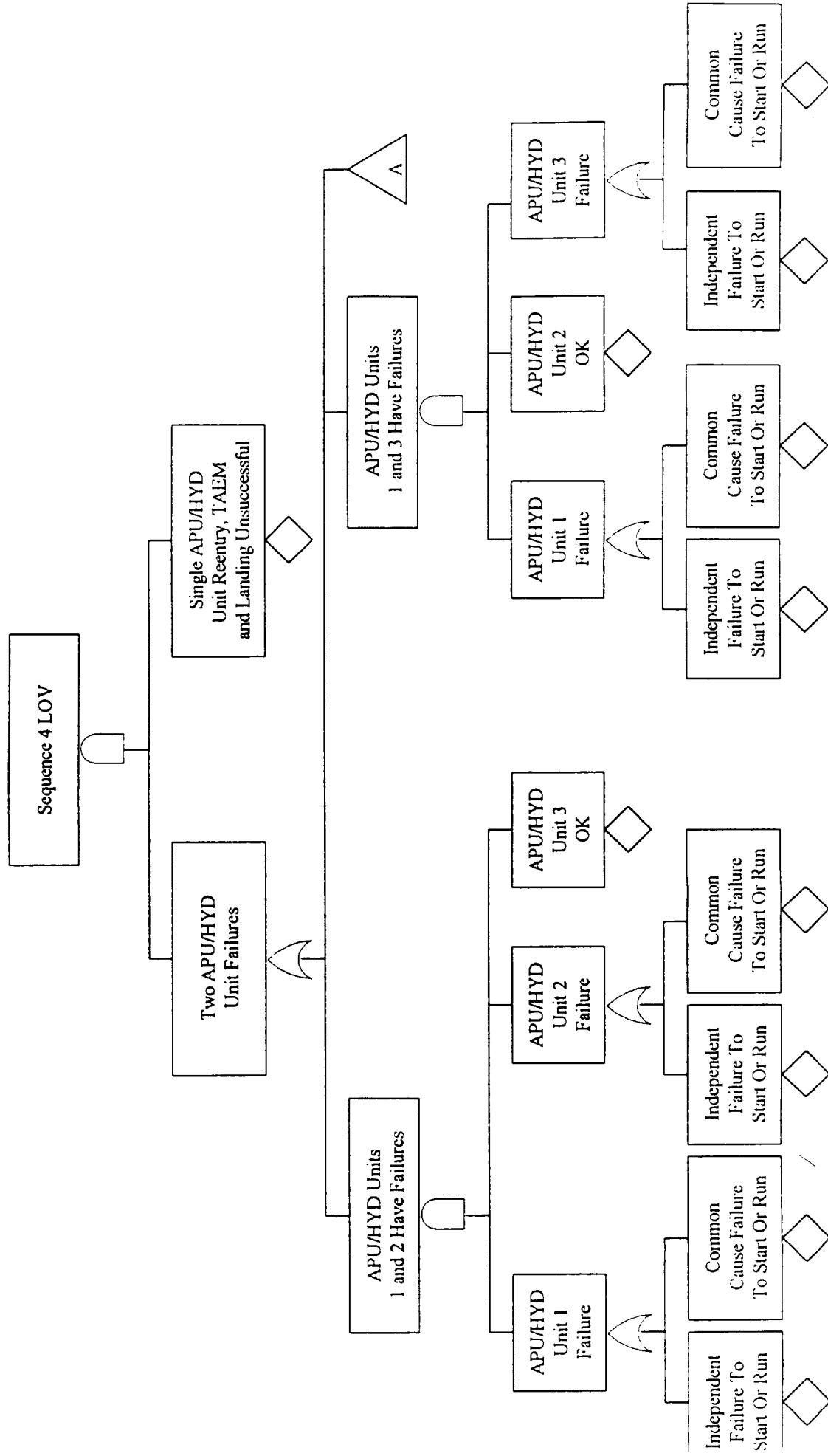
# Event Sequence Diagram For An OK Initiating State During Reentry, TAEM and Landing



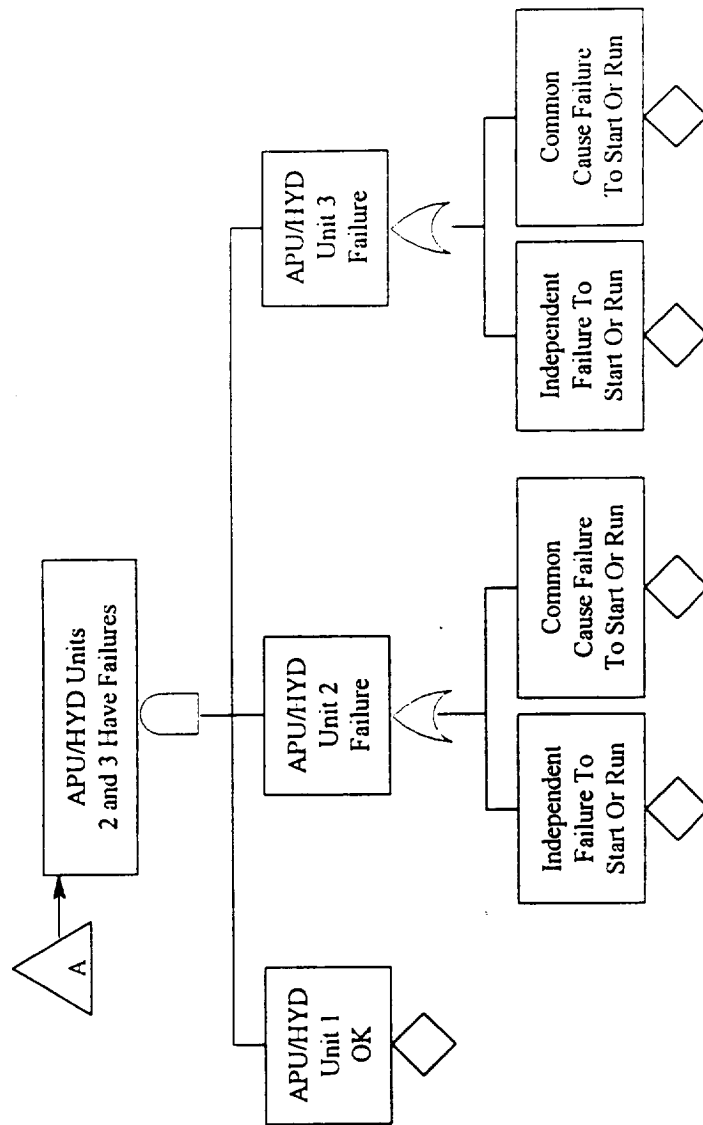




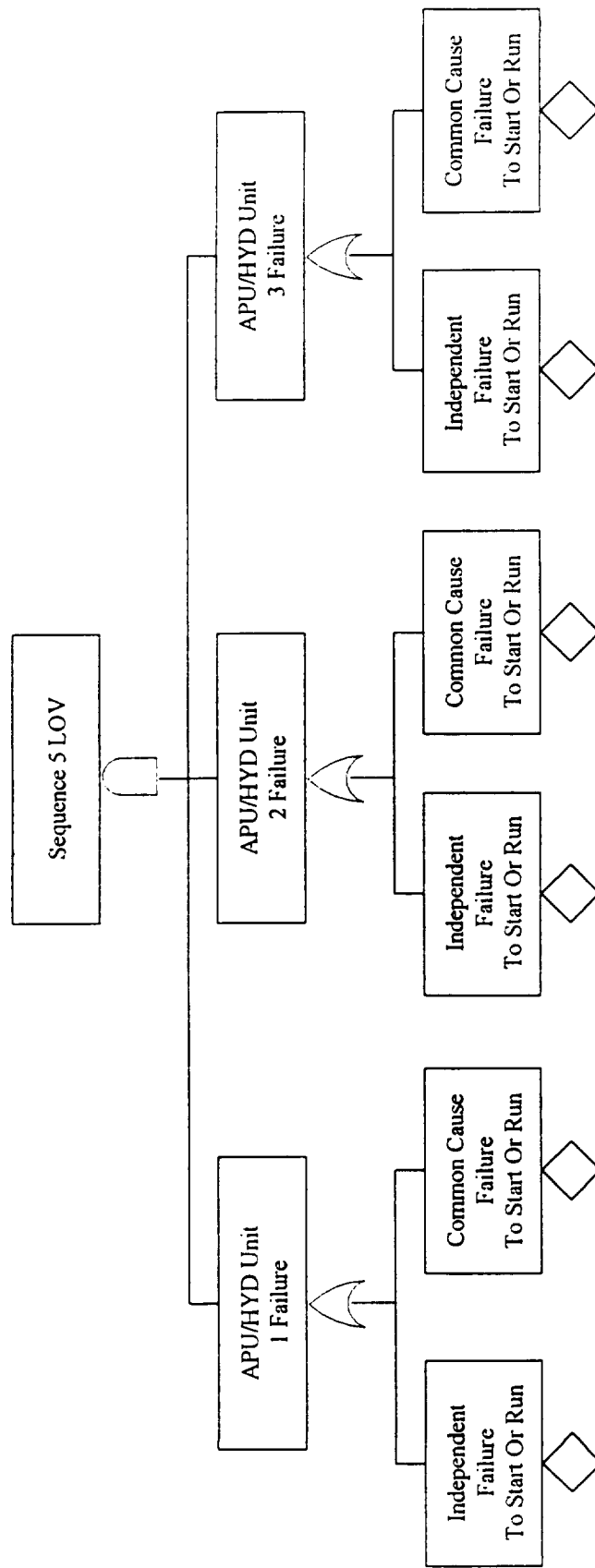
# **Fault Tree for Sequence 4 LOV: Two APU/HYD Units Fail Without Hydrazine Leaks and Single APU/HYD Unit Reentry, TAEM and Landing is Unsuccessful**



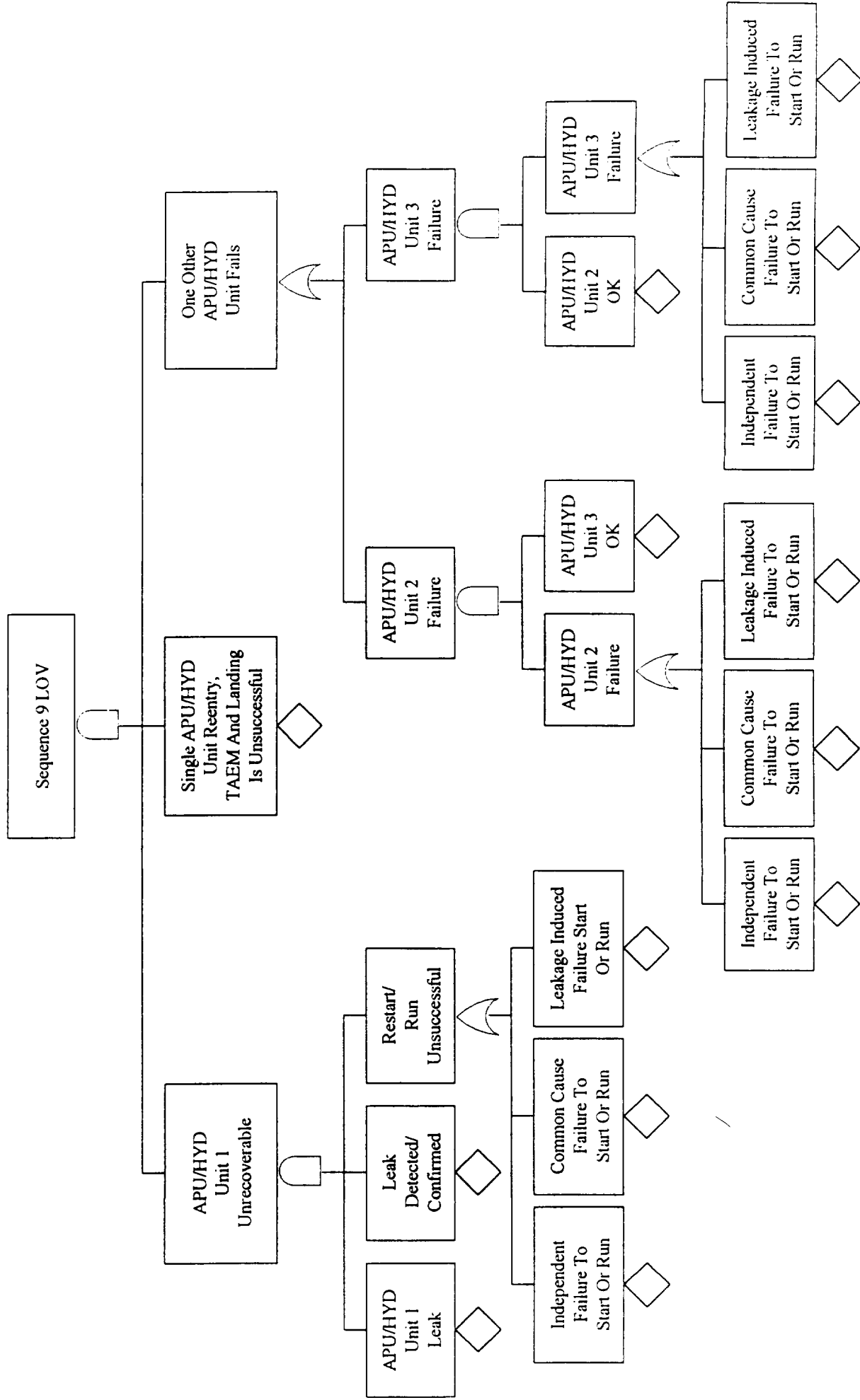
**Fault Tree for Sequence 4 LOV: Two APU/HYD  
Units Fail Without Hydrazine Leaks and Single  
APU/HYD Unit Reentry, TAEM and Landing is Unsuccessful  
(Continued)**



**Fault Tree for Sequence 5 LOV: All Three  
APU/HYD Units Fail Without Hydrazine  
Leaks During Reentry, TAEM and Landing**

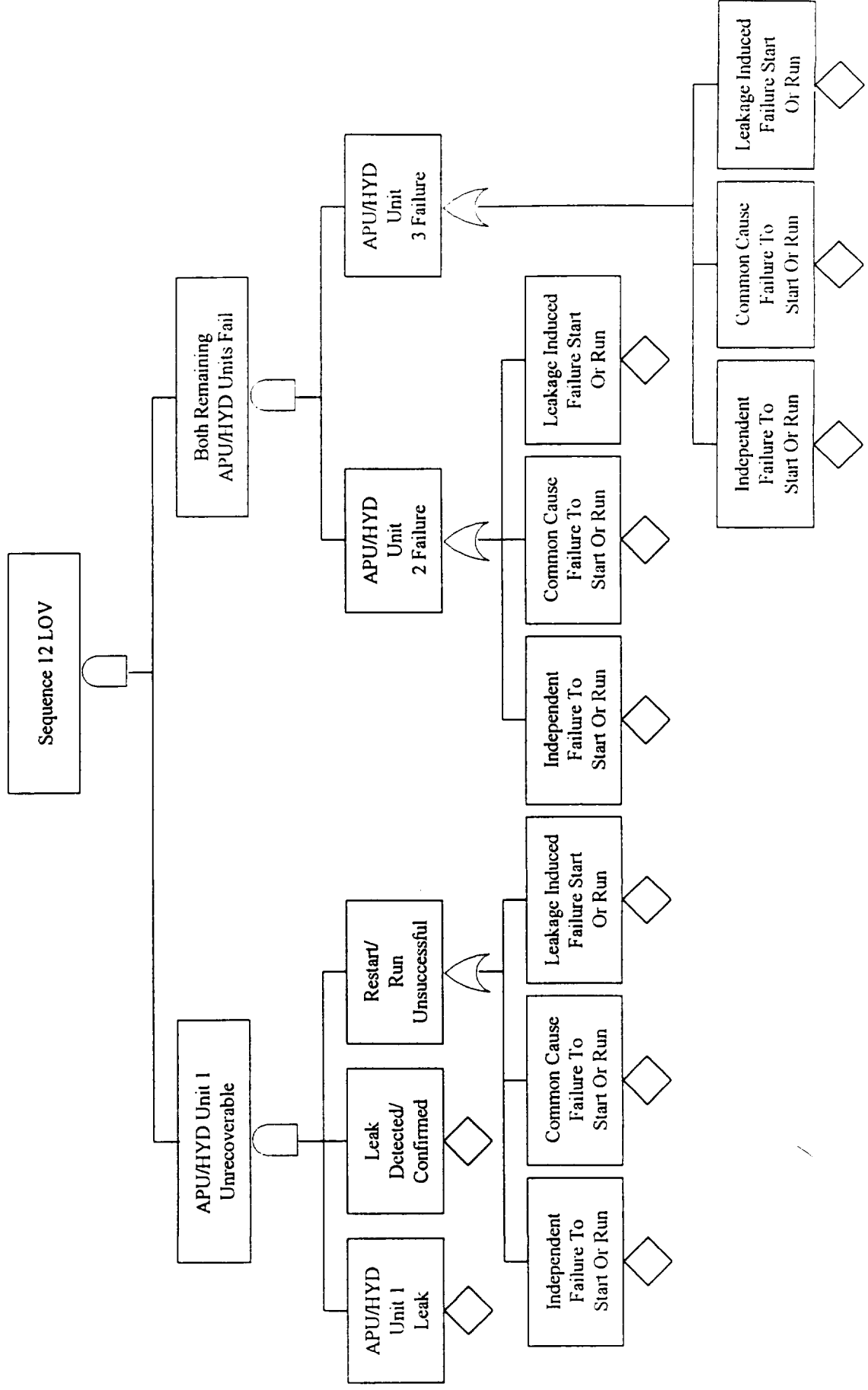


**Fault Tree for Sequence 9 LOV: One APU/HYD Unit Leaks and is Shutdown, One Other Unit Fails, Restart of Shutdown APU/HYD Unit is Unsuccessful, and Single APU/HYD Unit Reentry, TAEM and Landing is Unsuccessful**

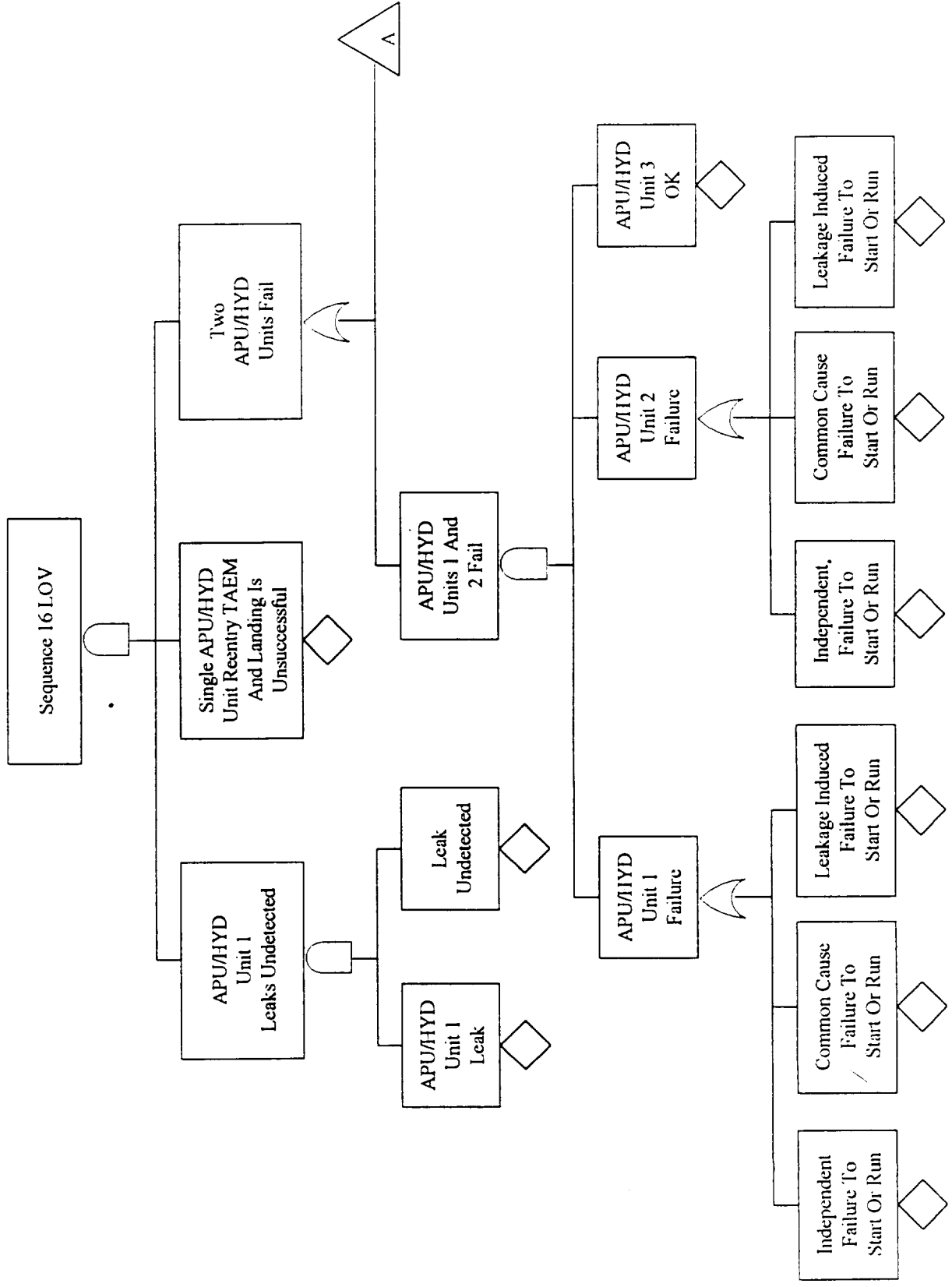




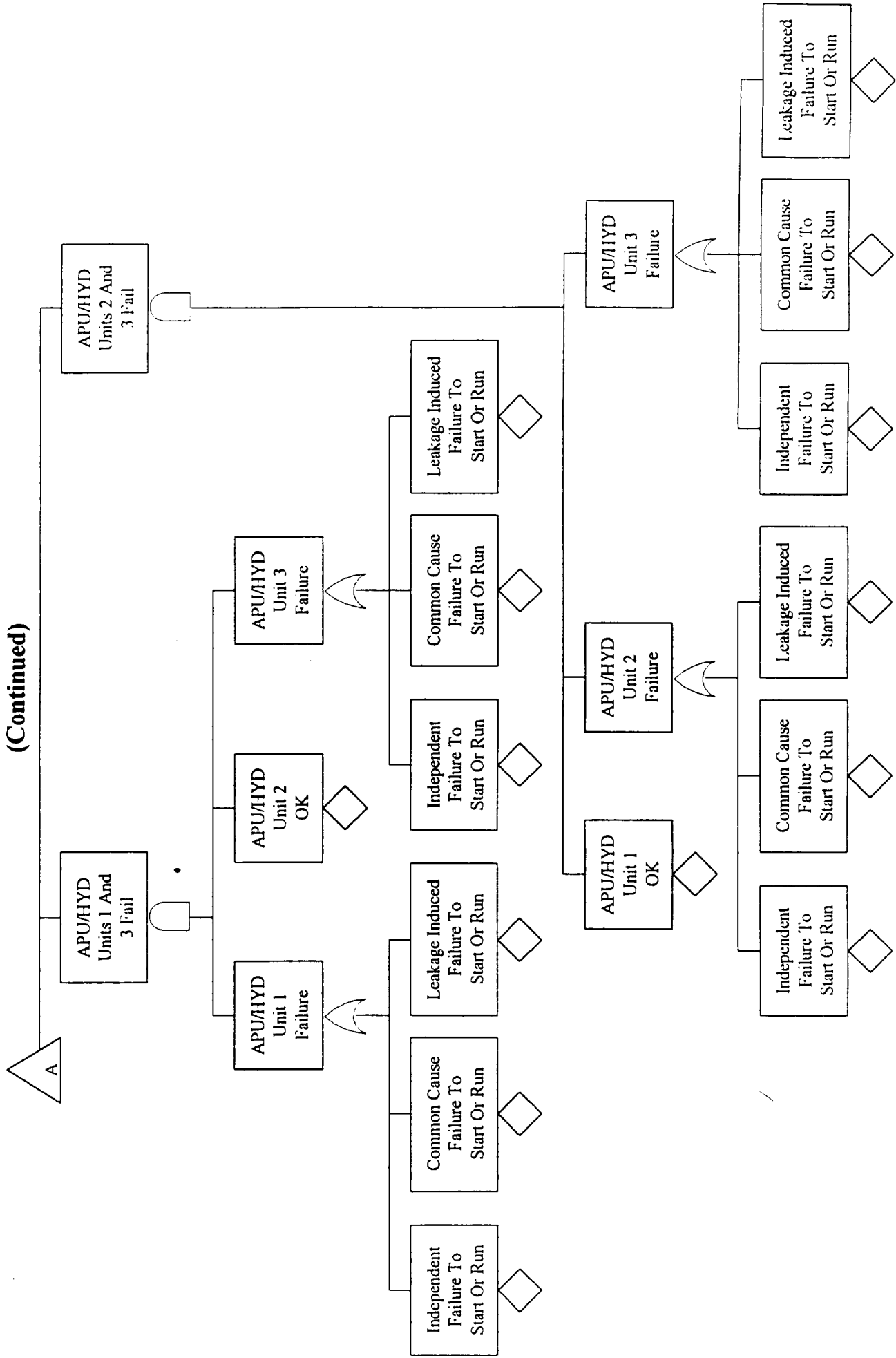
# **Fault Tree for Sequence 12 LOV: One APU/HYD Unit Leaks and is Shutdown, Both Remaining APU/HYDs Have Failures, and Restart of APU/HYD Unit 1 is Unsuccessful**



**Sequence 16 LOV: One APU/HYD Unit  
Leaks Undetected, Two APU/HYD  
Units Fail and Single APU/HYD Unit  
Reentry, TAEM and Landing is Unsuccessful**



**Sequence 16 LOV: One APU/HYD Unit  
Leaks Undetected, Two APU/HYD  
Units Fail and Single APU/HYD Unit  
Reentry, TAEM and Landing is Unsuccessful  
(Continued)**

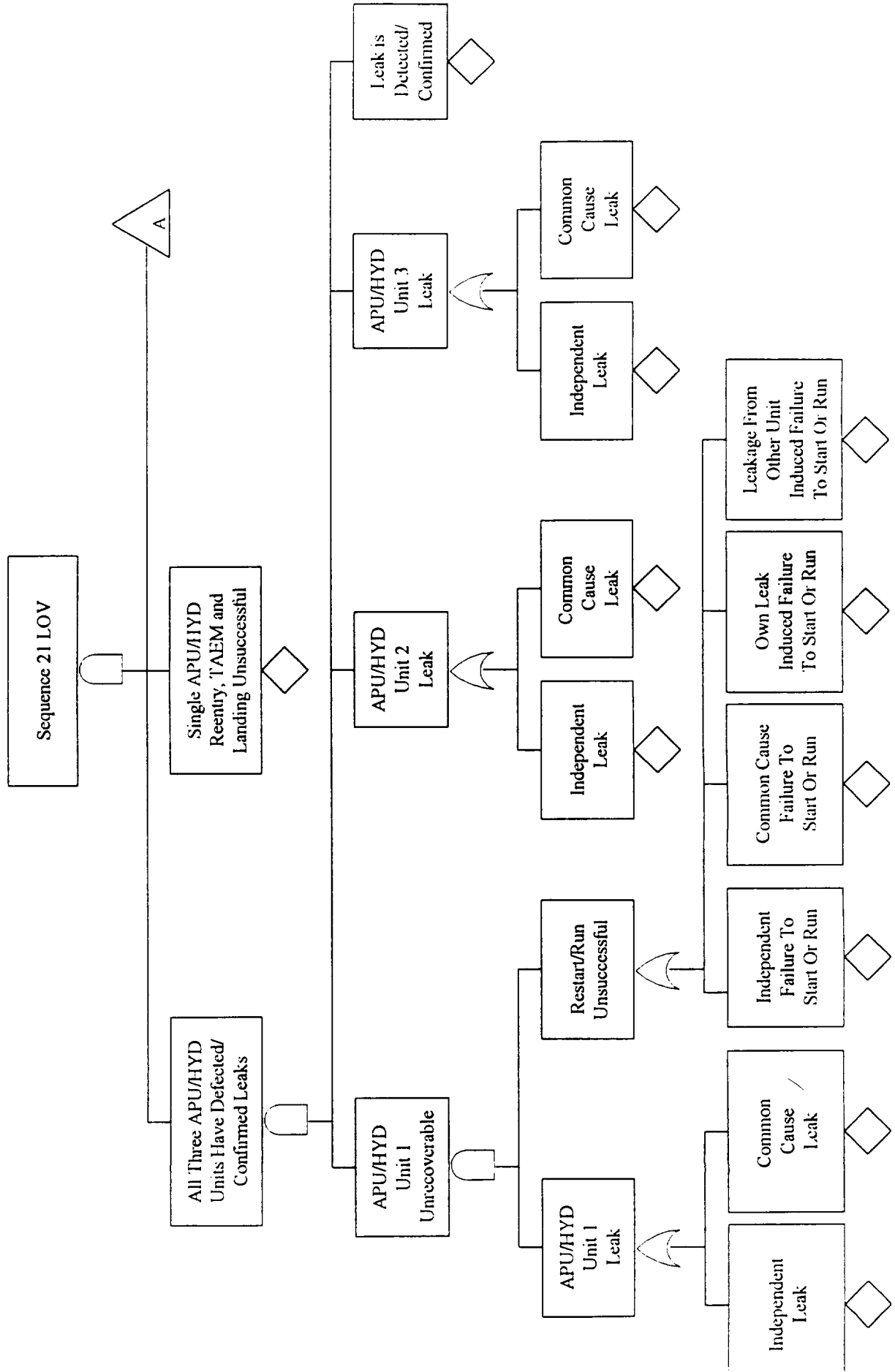




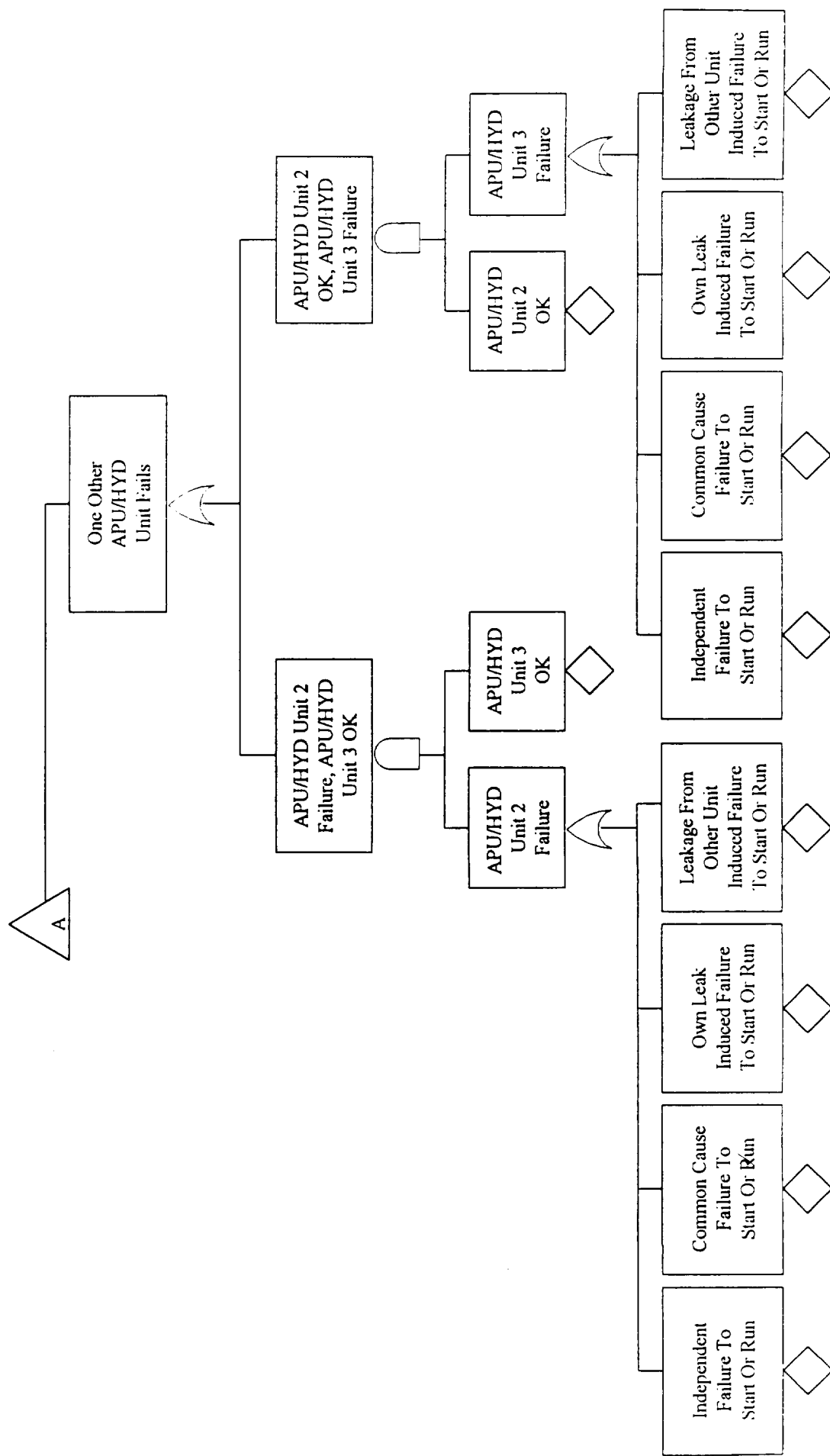
```

graph TD
    S17LOV[Sequence 17 LOV] --> U1LU[APU/HYD Unit 1 Leaks Undetected]
    S17LOV --> A3U[All Three APU/HYD Units Fail]
    
    U1LU --> U1L[APU/HYD Unit 1 Leak]
    U1LU --> LU[Leak Undetected]
    
    U1L --> I1L[Independent Failure To Start Or Run]
    U1L --> C1L[Common Cause Failure To Start Or Run]
    
    LU --> C2L[Common Cause Failure To Start Or Run]
    LU --> LI1L[Leakage Induced Failure To Start Or Run]
    
    A3U --> U1F[APU/HYD Unit 1 Failure]
    A3U --> U2F[APU/HYD Unit 2 Failure]
    A3U --> U3F[APU/HYD Unit 3 Failure]
    
    U1F --> I1F[Independent Failure To Start Or Run]
    U1F --> C1F[Common Cause Failure To Start Or Run]
    U1F --> LI1F[Leakage Induced Failure To Start Or Run]
    
    U2F --> I2F[Independent Failure To Start Or Run]
    U2F --> C2F[Common Cause Failure To Start Or Run]
    U2F --> LI2F[Leakage Induced Failure To Start Or Run]
    
    U3F --> I3F[Independent Failure To Start Or Run]
    U3F --> C3F[Common Cause Failure To Start Or Run]
    U3F --> LI3F[Leakage Induced Failure To Start Or Run]
  
```

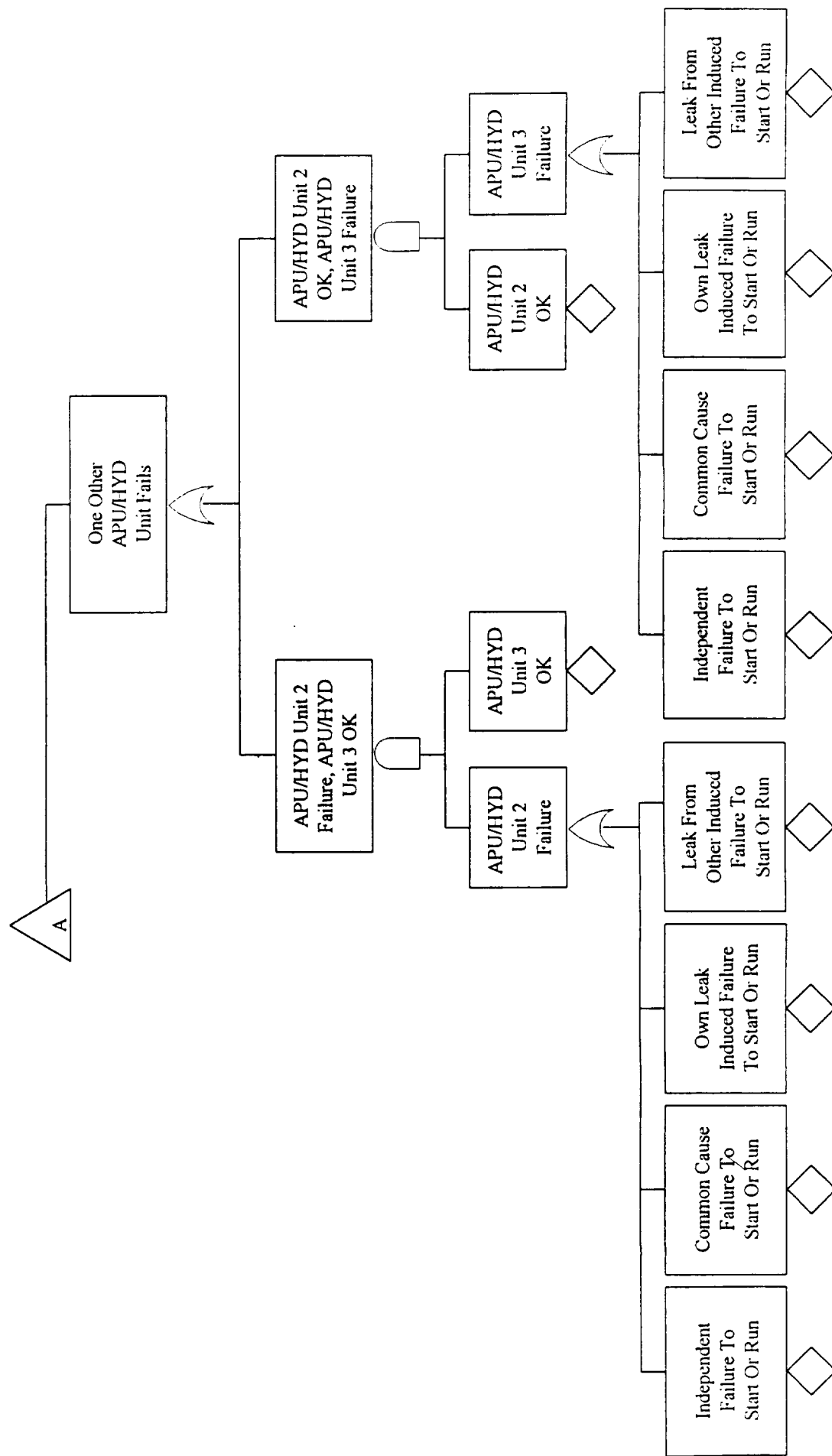
**Fault Tree for Sequence 21 LOV: All Three APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, One Other Unit Fails, Restart of Shutdown Unit is Unsuccessful and Single APU/HYD Unit Loading is Unsuccessful**



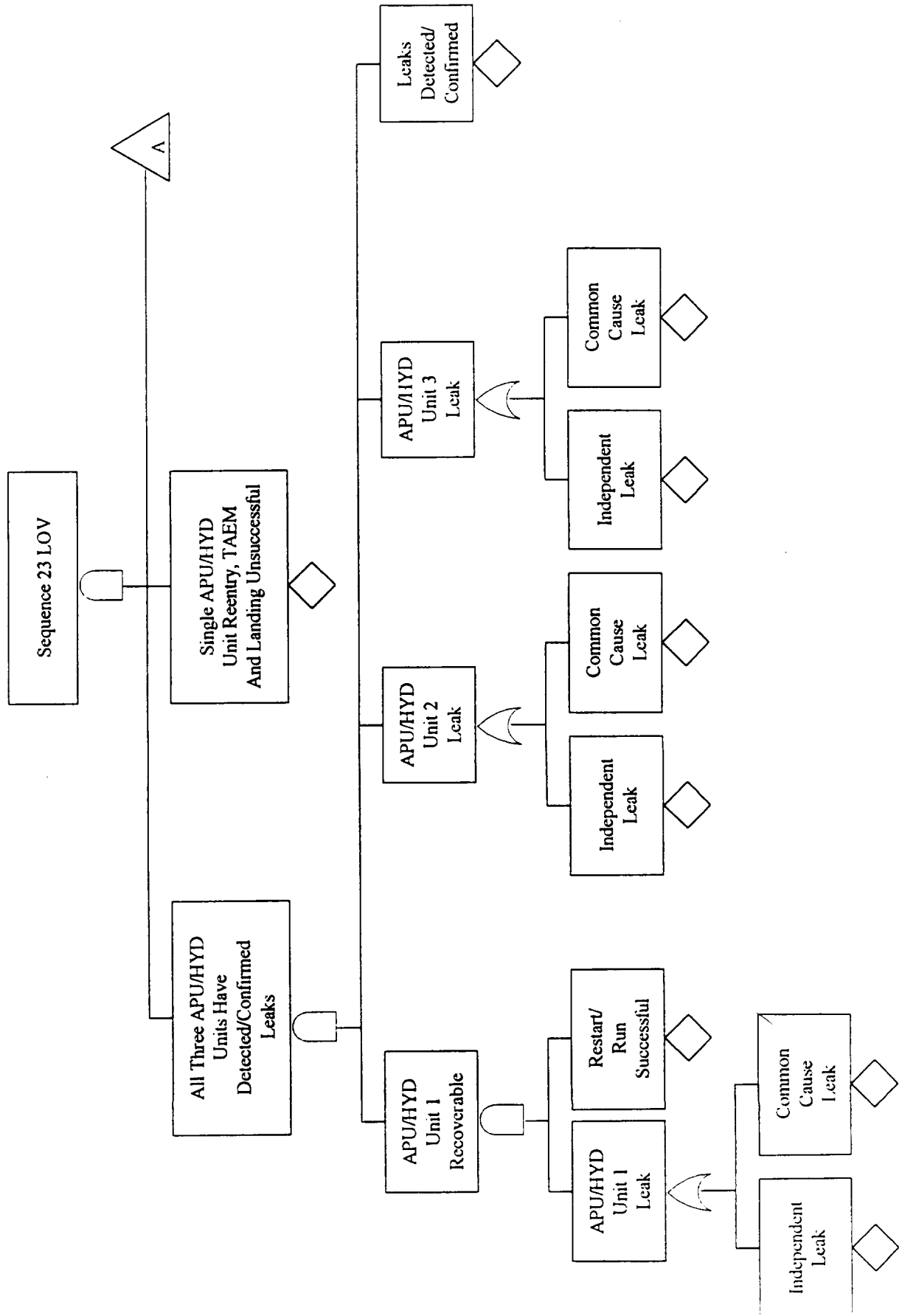
**Fault Tree for Sequence 2.1 LOV: All Three  
APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, One  
Other Unit Fails, Restart of Shutdown Unit is Unsuccessful  
and Single APU/HYD Unit Loading is Unsuccessful  
(Continued)**



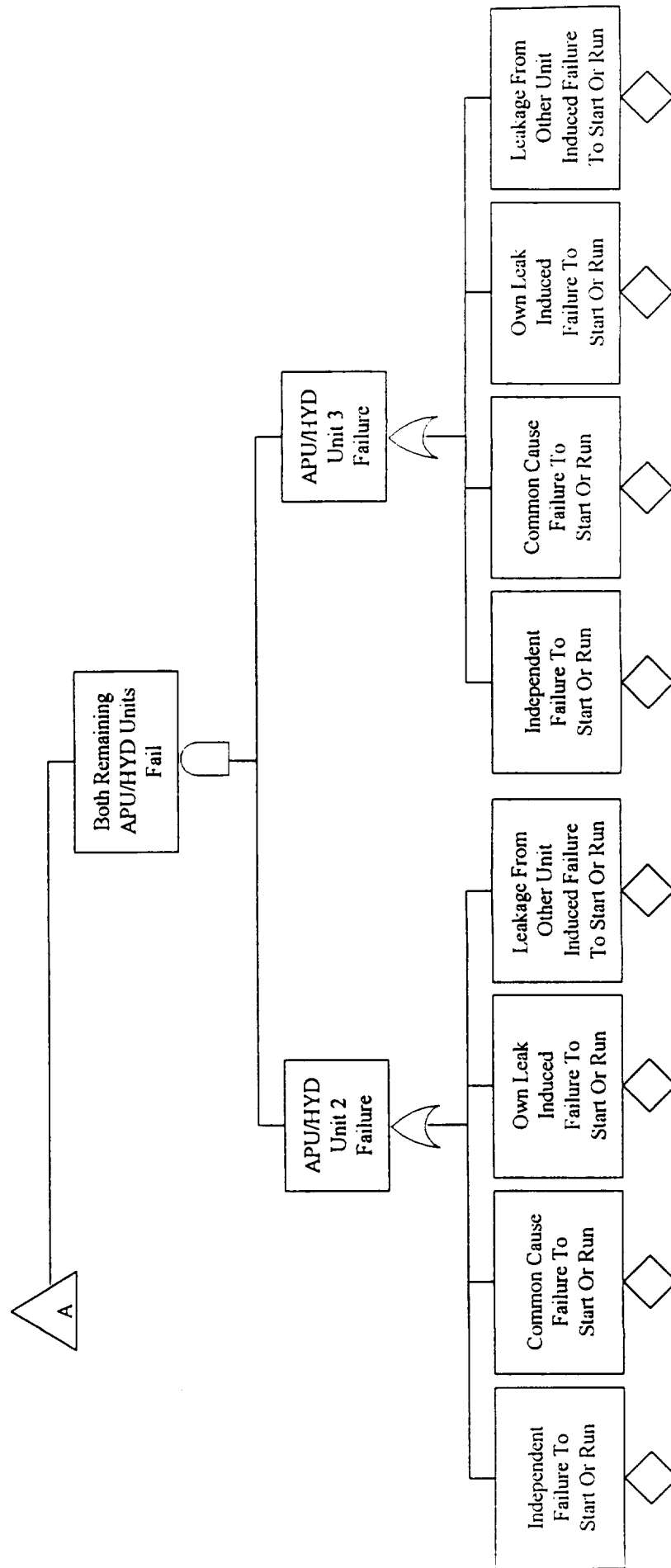
**Fault Tree for Sequence 21 LOV: All Three  
APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, One  
Other Unit Fails, Restart of Shutdown Unit is Unsuccessful  
and Single APU/HYD Unit Loading is Unsuccessful  
(Continued)**



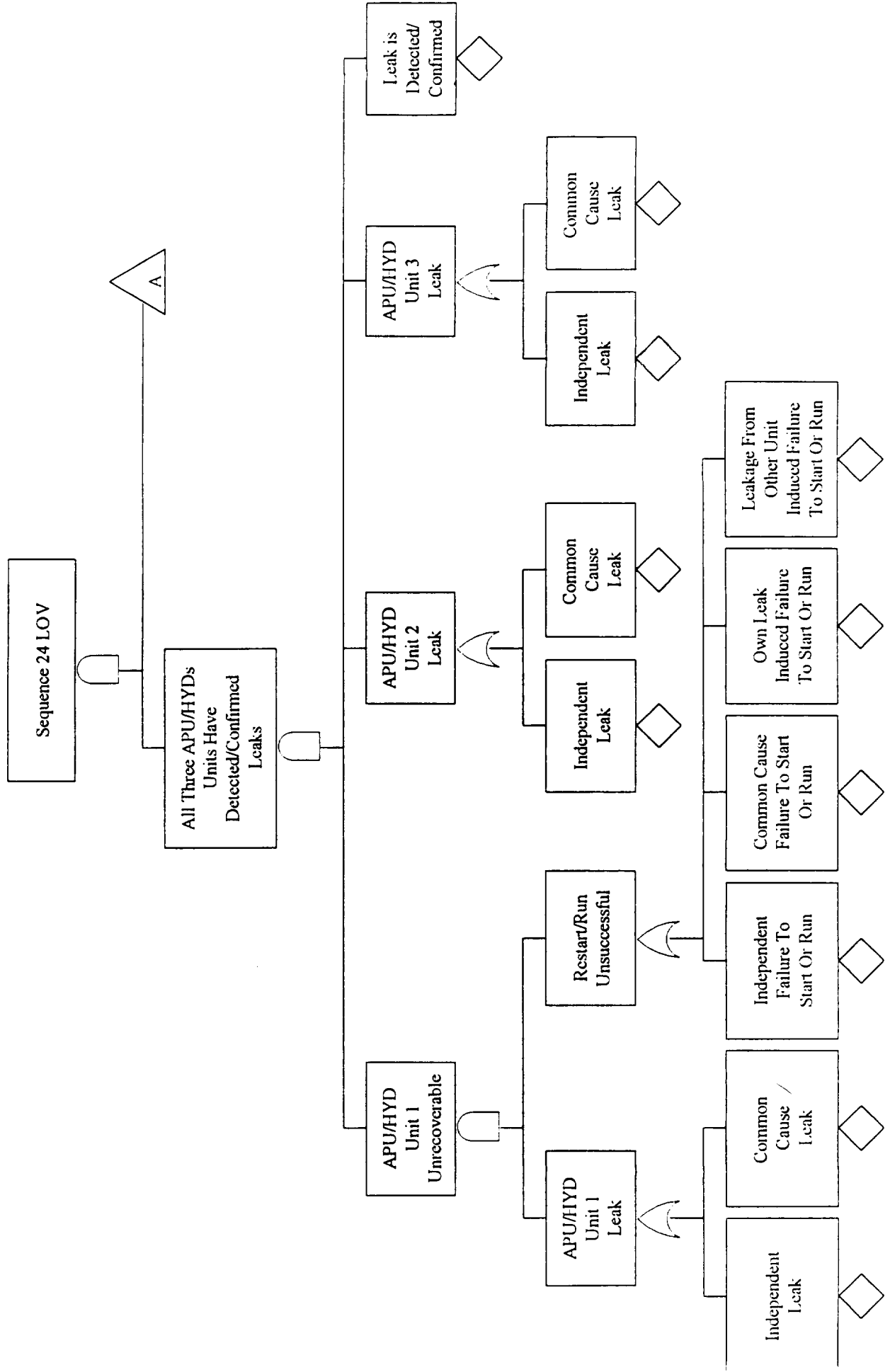
**Fault Tree for Sequence 23 LOV: All Three  
APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, Both  
Remaining APU/HYD Units Fail, the Shutdown  
Unit is Restarted, but the Single APU/HYD Unit  
Reentry, TAEM and Landing is Unsuccessful**



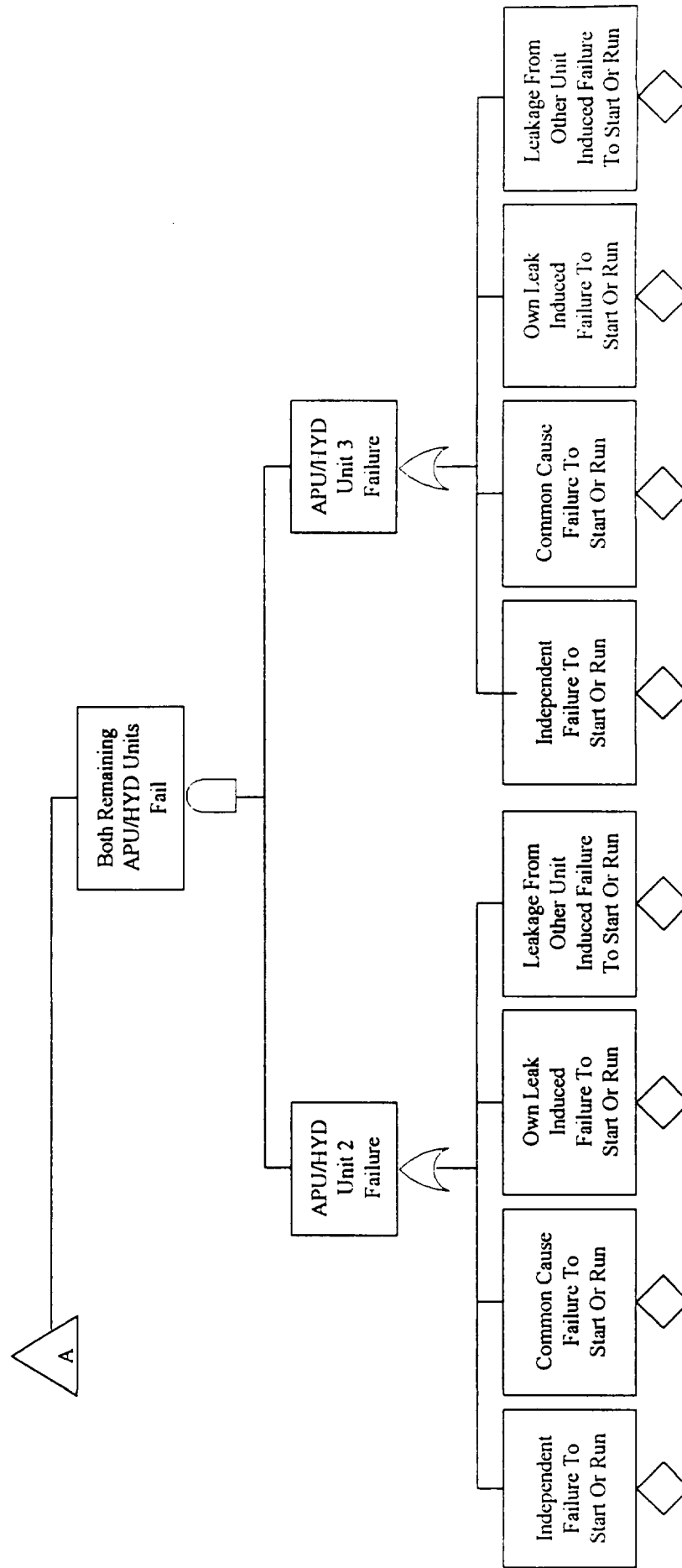
**Fault Tree for Sequence 23 LOV: All Three  
APU/HYD Units Leak, APU/HYD Unit 1 Shutdown, Both  
Remaining APU/HYD Units Fail and Restart of  
Shutdown APU/HYD Unit is Unsuccessful  
(Continued)**



**Fault Tree for Sequence 24 LOV: All Three APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, Both Remaining APU/HYD Units Fail and Restart of Shutdown APU/HYD Unit is Unsuccessful**

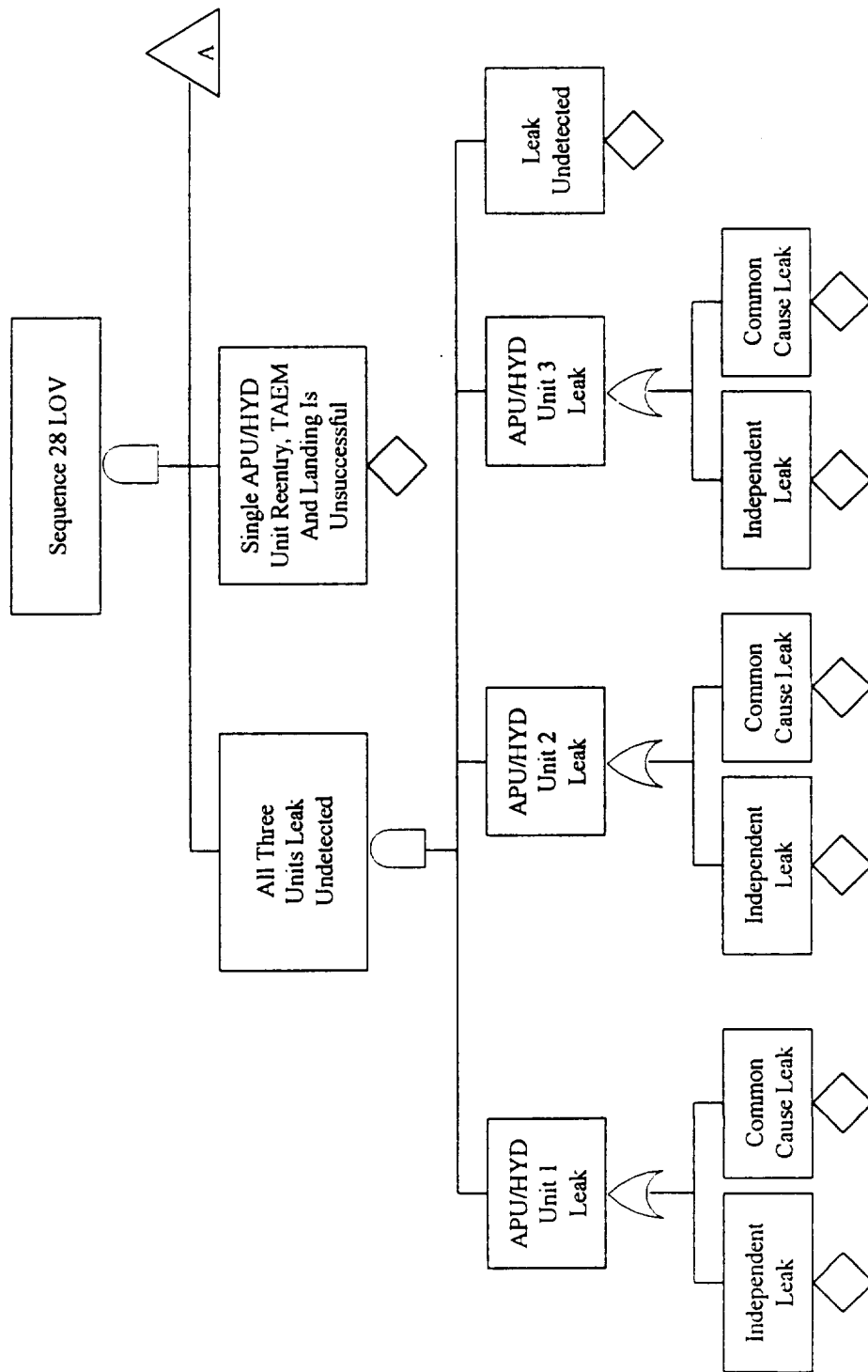


**Fault Tree for Sequence 24 LOV: All Three  
APU/HYD Units Leak, APU/HYD Unit 1 is Shutdown, Both  
Remaining APU/HYD Units Fail and Restart of  
Shutdown APU/HYD Unit is Unsuccessful  
(Continued)**

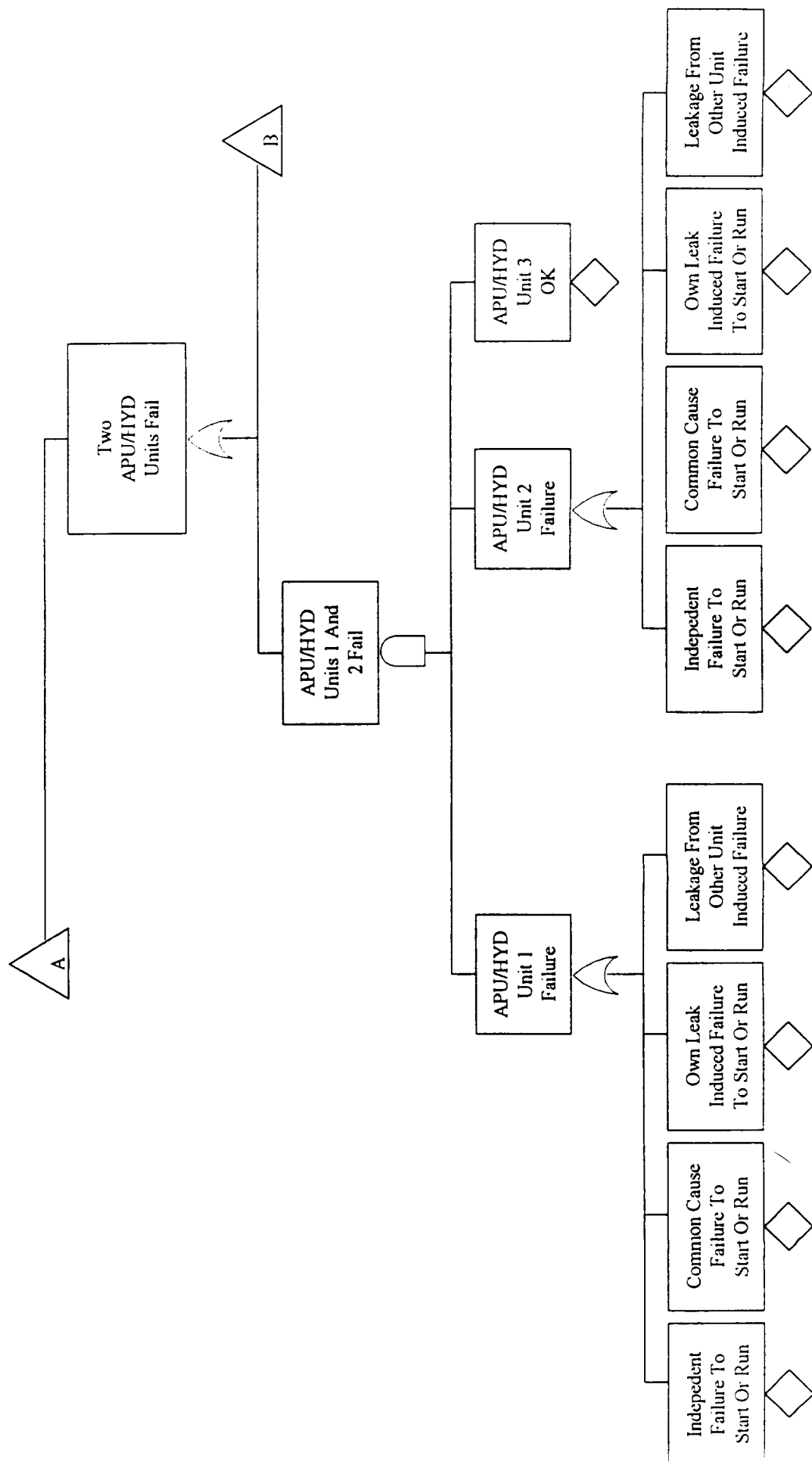




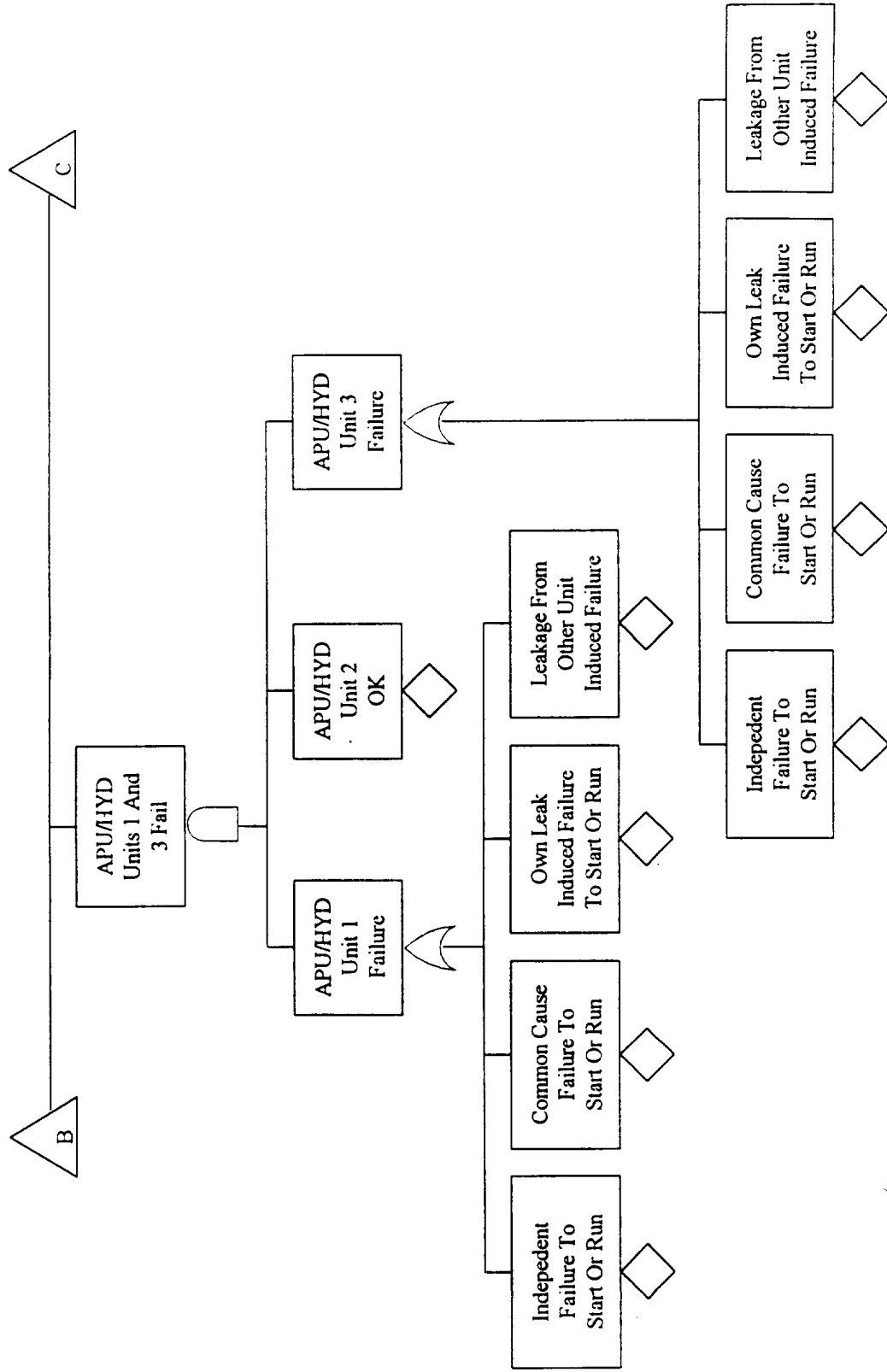
# **Fault Tree for Sequence 28 LOV: All Three APU/HYD Units Leak Undetected, Two APU/HYD Units Fail, Single APU/HYD Unit Landing Unsuccessful**



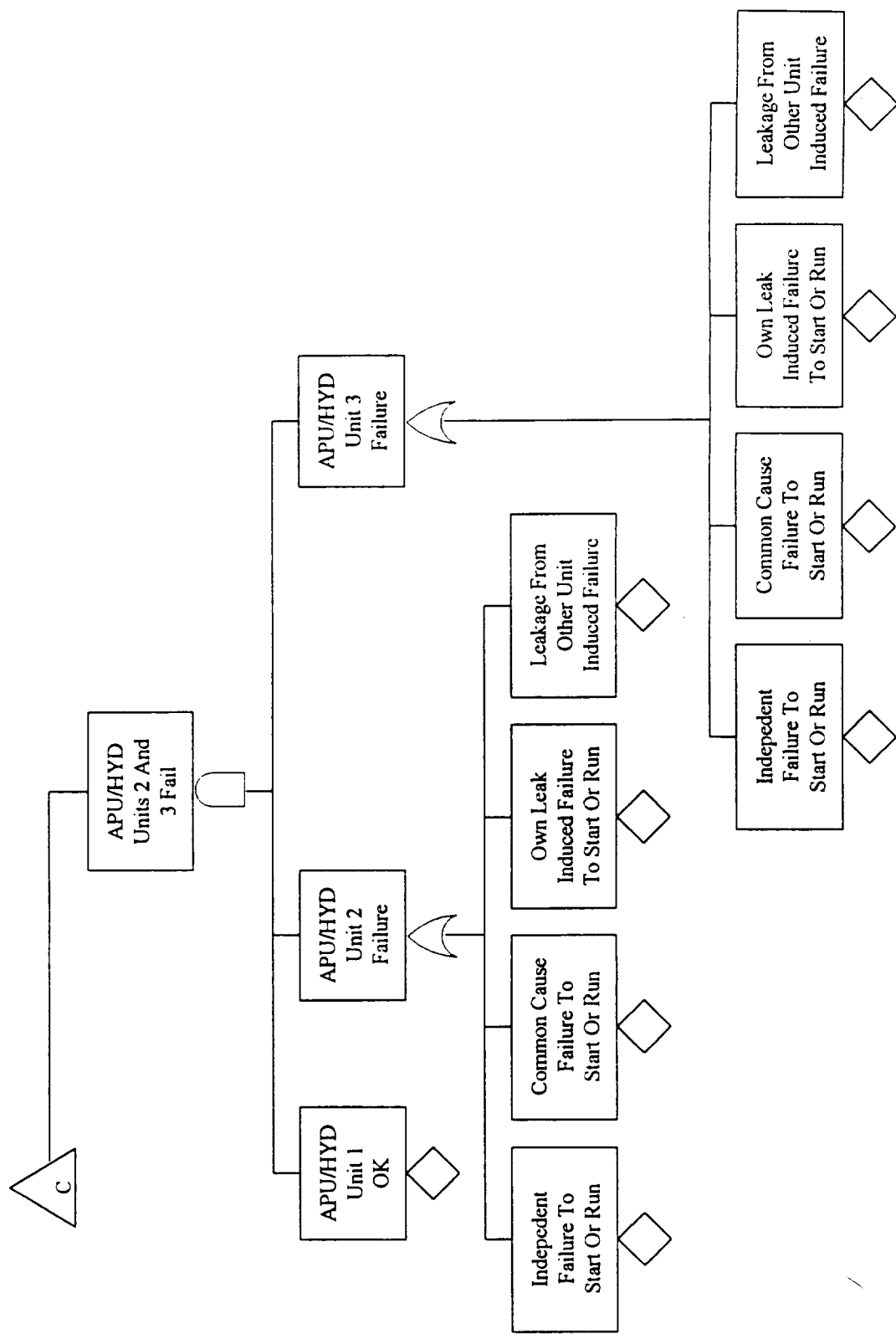
**Fault Tree for Sequence 28 LOV: All Three  
APU/HYD Units Leak Undetected,  
Two APU/HYD Units Fail, Single APU/HYD  
Unit Landing Unsuccessful (Continued)**



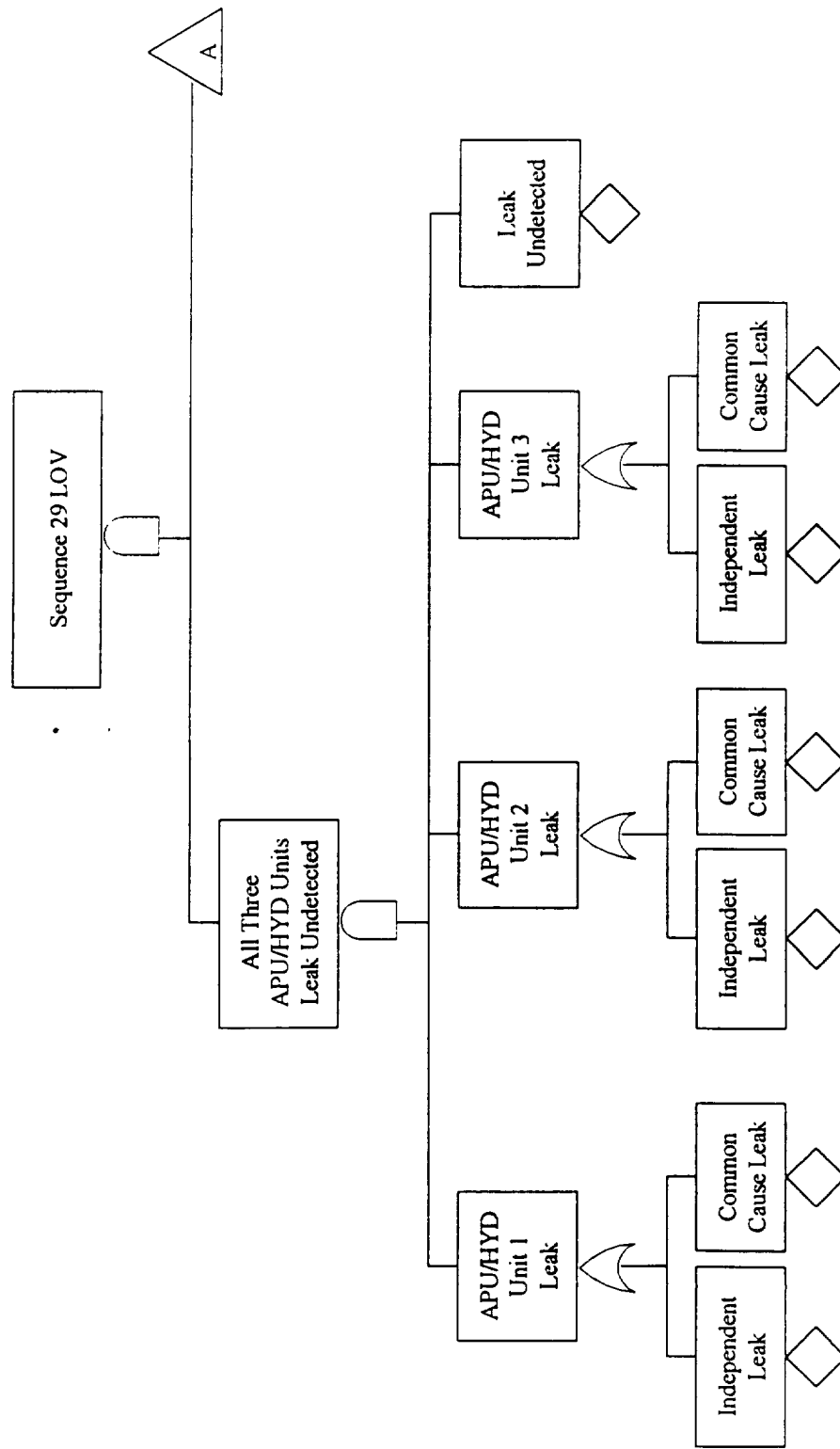
**Fault Tree for Sequence 28 LOV: All Three  
APU/HYD Units Leak Undetected,  
Two APU/HYD Units Fail, Single APU/HYD  
Unit Landing Unsuccessful (Continued)**



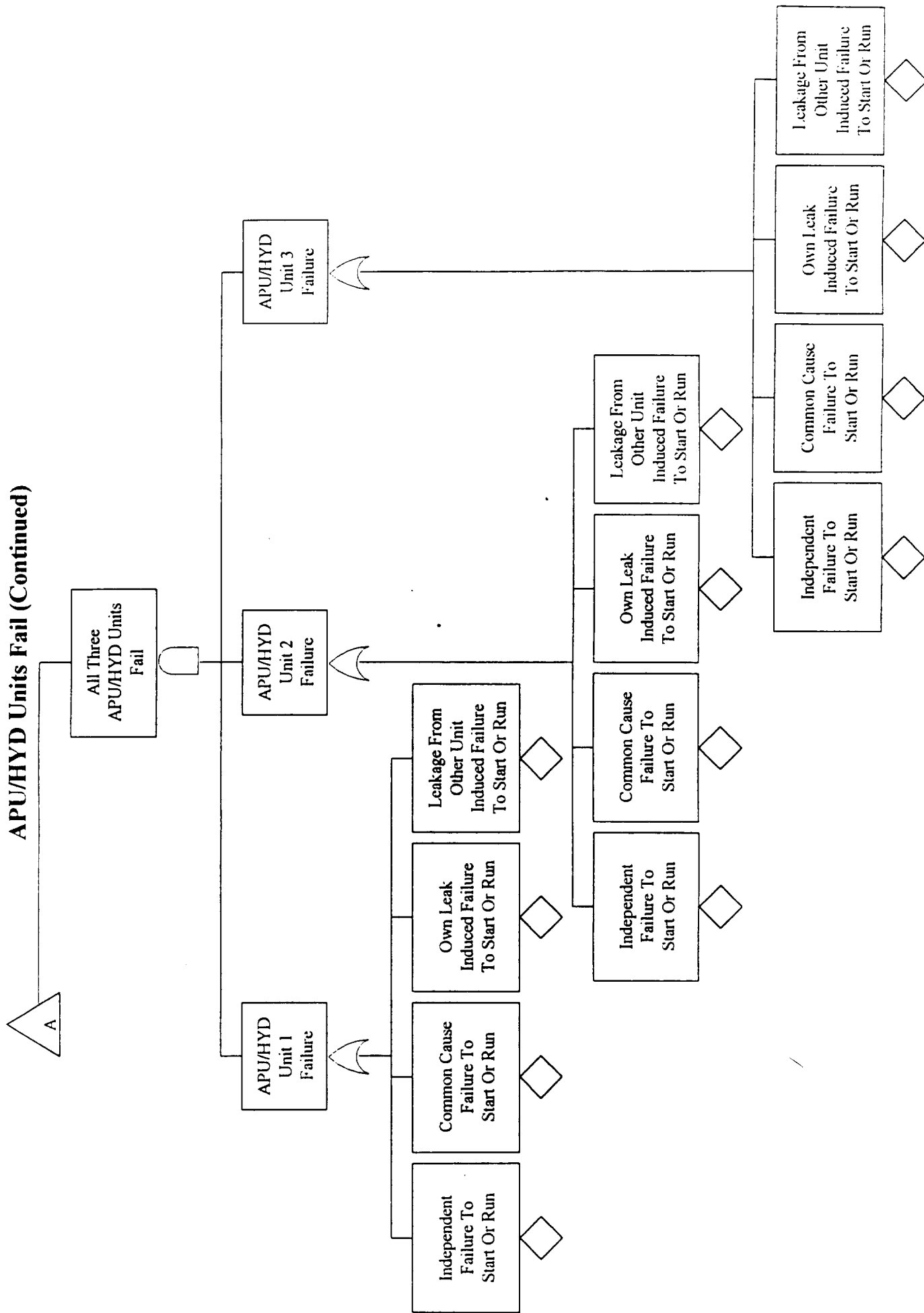
**Fault Tree for Sequence 28 LOV: All Three  
APU/HYD Units Leak Undetected,  
Two APU/HYD Units Fail, Single APU/HYD  
Unit Landing Unsuccessful (Continued)**



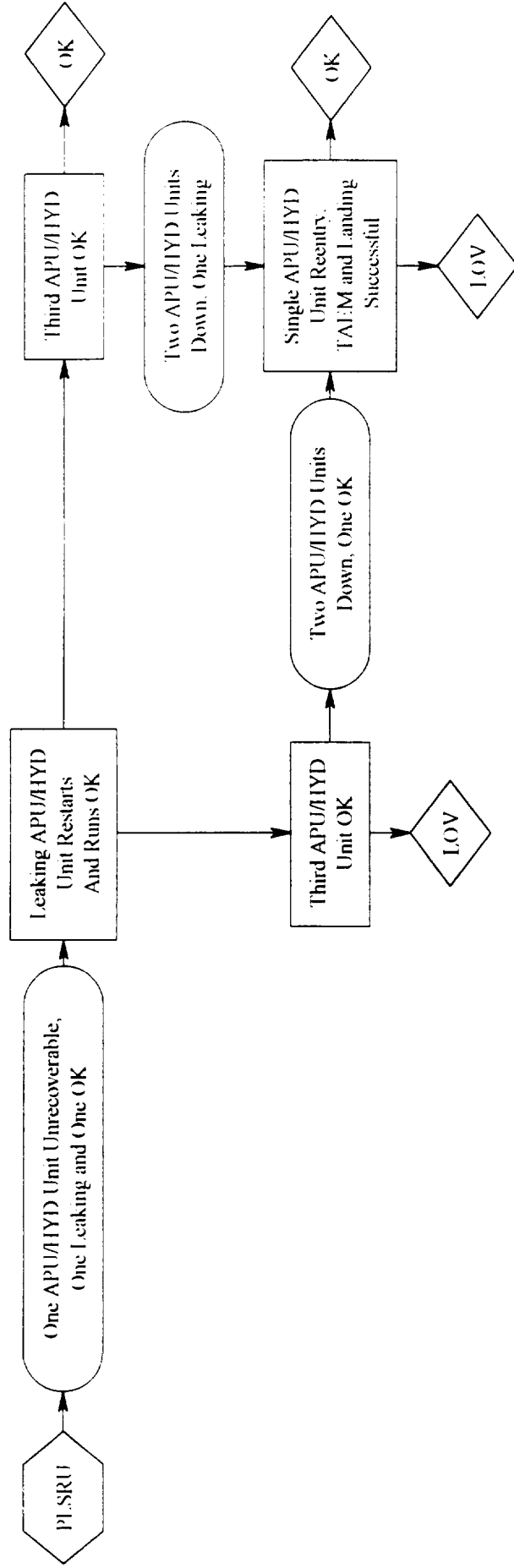
**Fault Tree for Sequence 29 LOV: All Three  
APU/HYD Units Leak Undetected and all Three  
APU/HYD Units Fail**



# **Fault Tree for Sequence 29 LOV: All Three APU/HYD Units Leak Undetected and all Three APU/HYD Units Fail (Continued)**



# **Event Sequence Diagram for a PLSRU State During Reentry, TAEM and Landing**

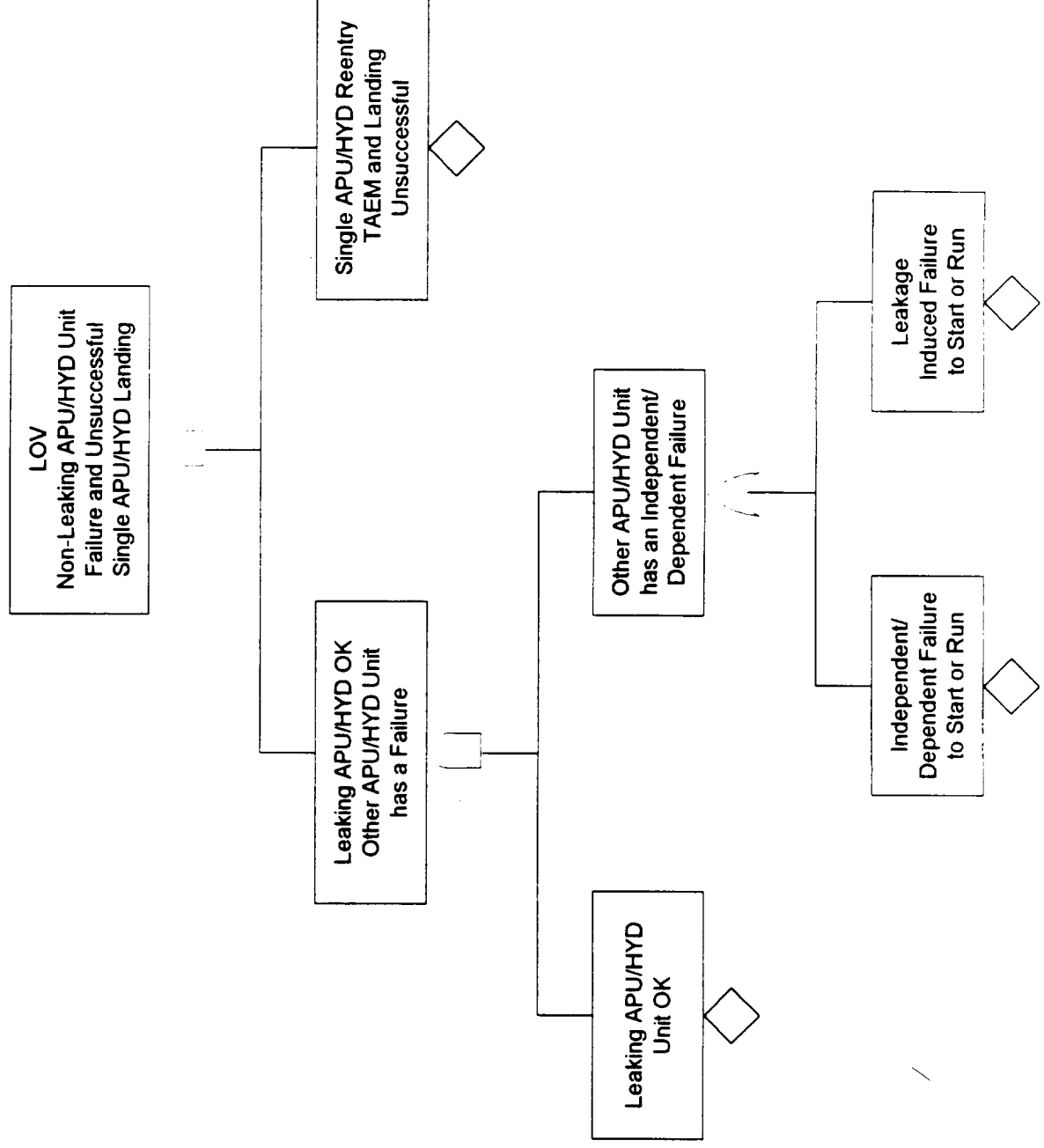


EVENT TREE OF A PLSRU INITIATING EVENT DURING REENTRY, TAEM AND LANDING

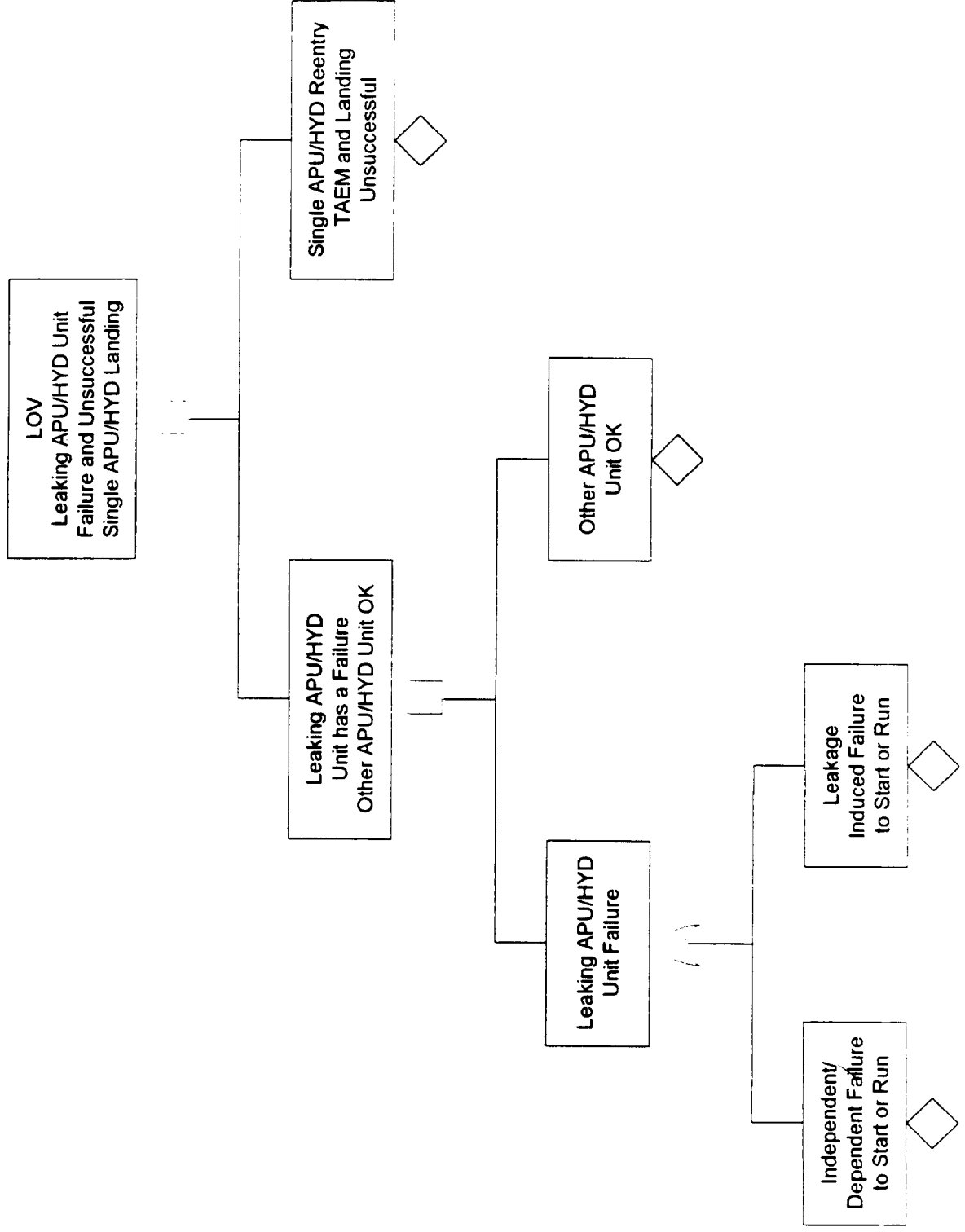
RU	UR	3F	UL	SEQUENCE		STATE
				NUMBER	DESCRIPTION	
				1	RU	OK
				2	RU3F	OK
				3	RU3FUL	LOV
				4	RUUR	OK
				5	RUURUL	LOV
				6	RUUR3F	LOV



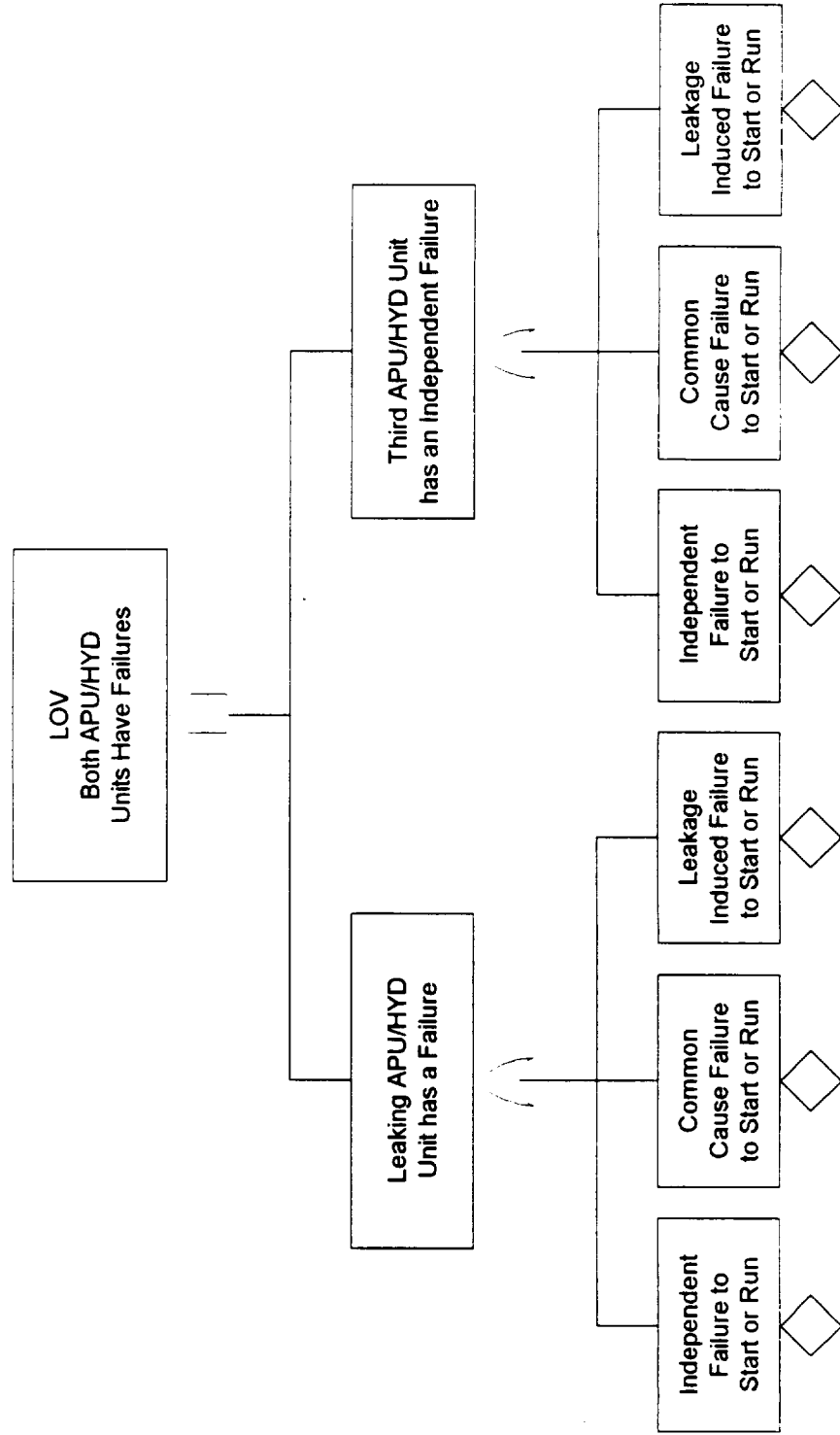
# Fault Tree For Sequence 3 LOV State With PLSRU Initiating Event During Reentry, TAEM and Landing



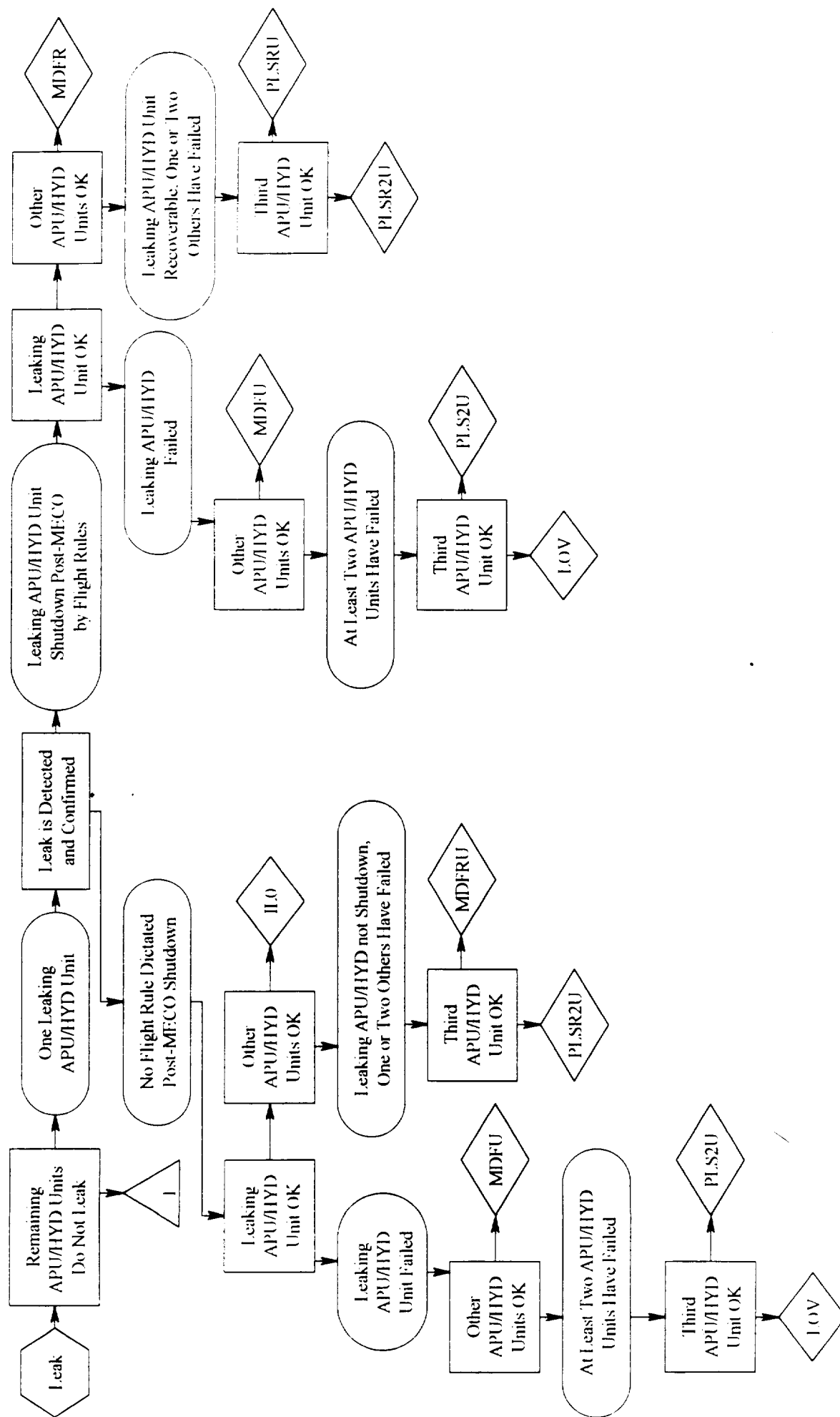
**Fault Tree For Sequence 5 LOV  
State With PLSRU Initiating Event  
During Reentry, TAEM and Landing**



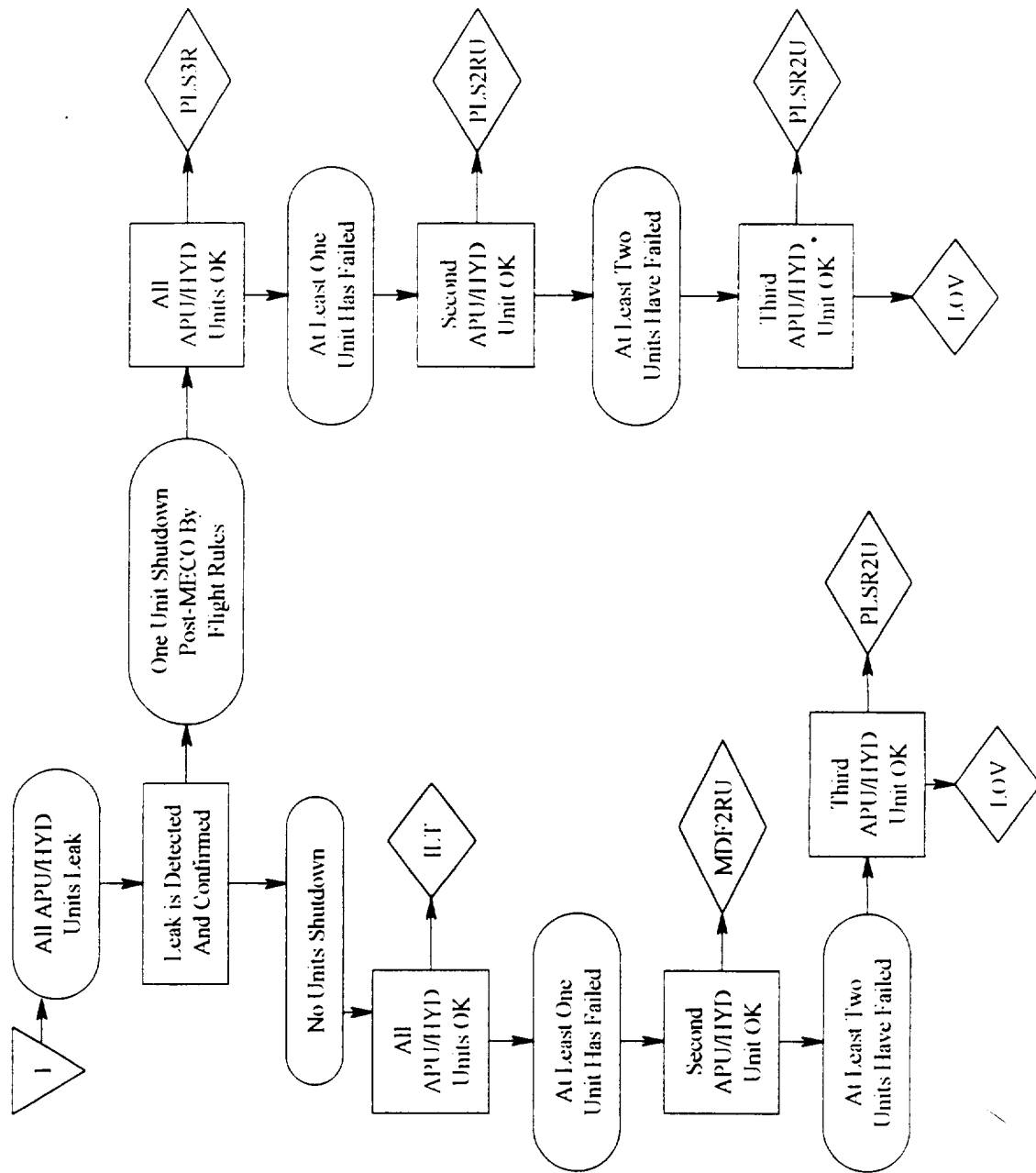
**Fault Tree For Sequence 6 LOV  
State With PLSRU Initiating Event  
During Reentry, TAEM and Landing**



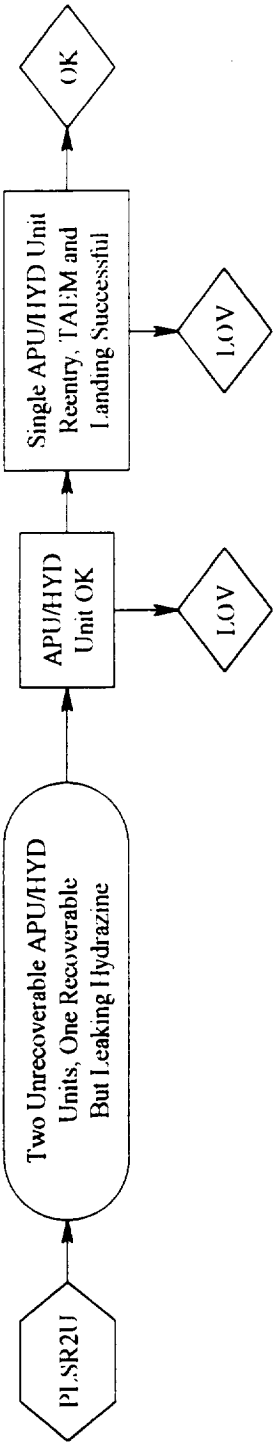
# **Event Sequence Diagram of APU/HYD Hydrazine Leaks During Ascent**



# **Event Sequence Diagram of APU/HYD Hydrazine Leaks During Ascent (Continued)**



**Event Sequence Diagram for  
a PLSR2U State During Reentry,  
TAEM and Landing**

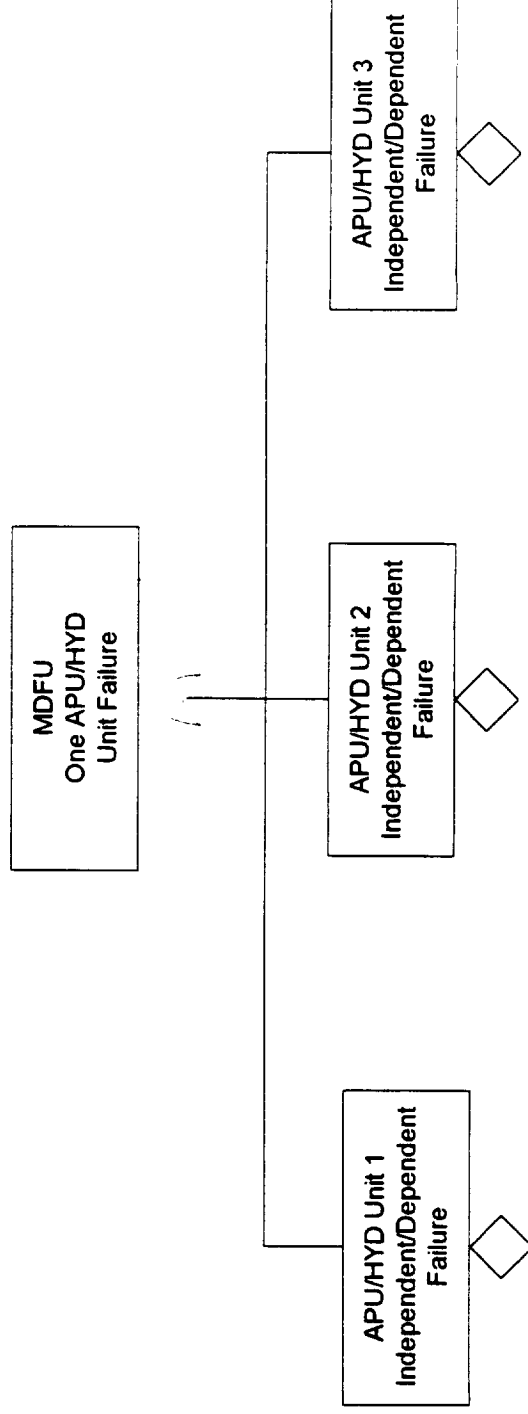


Assumption  
Assuming remaining  
APU/HYD unit restarted  
before reentry.

EVENT TREE OF A PLSR2U INITIATING EVENT DURING REENTRY, TAEM AND LANDING

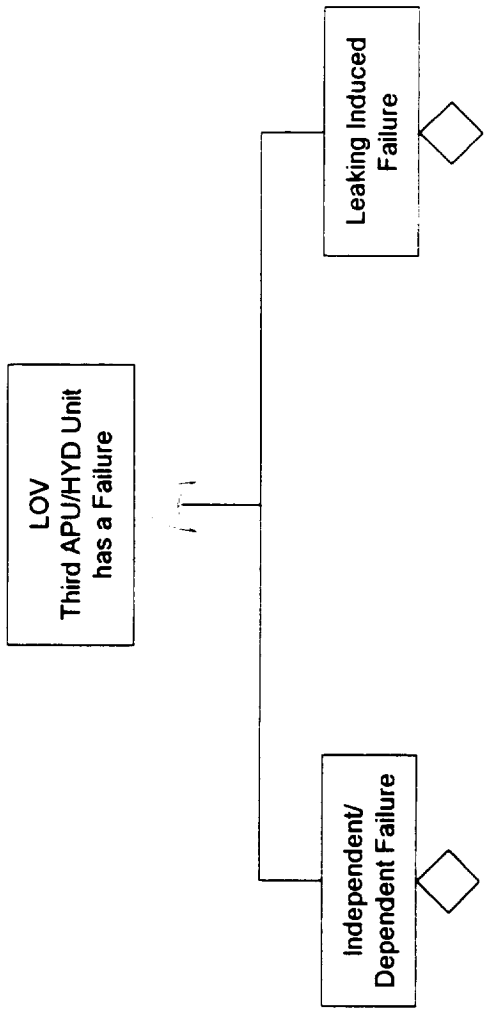
2U	SEQUENCE		SEQUENCE		STATE
	3F	UL	NUMBER	DESCRIPTION	
<div></div>	<div></div>	<div></div>	1	2U	OK
			2	2UUL	LOV
		<div></div>	3	2U3F	LOV

**Fault Tree For Sequence 2 MDFU  
State From OK Start Without A  
Hydrazine Leak During Ascent**





**Fault Tree For Sequence 3 LOV  
State With PLSR2U Initiating Event  
During Reentry, TAEM and Landing**

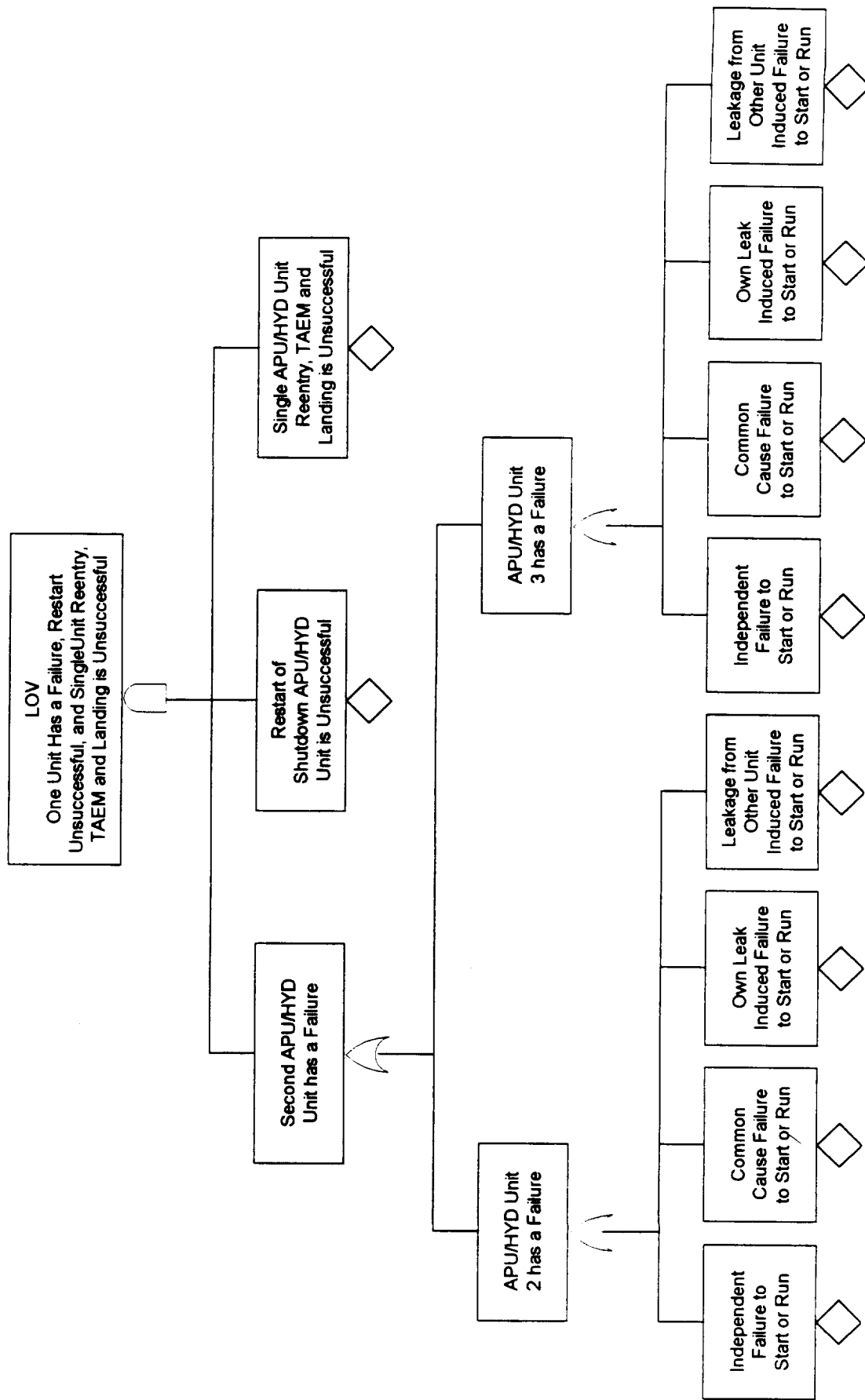


```
graph TD
    PLS3R{{PLS3R}} --> Rule1([Flight Rules Dictate  
That One APU/HiYD  
Unit Will Be Shutdown])
    Rule1 --> Box1[Both Remaining APU/HiYD  
Units OK For Reentry,  
TAEM And Landing]
    Box1 --> OK1{OK}
    Box1 --> Box2([One APU Unit Shutdown,  
One APU Unit Failed])
    Box2 --> Box3[Third APU/HiYD Unit  
OK for Reentry,  
TAEM and Landing]
    Box3 --> OK2{OK}
    Box3 --> Box4[Successful Restart  
of Shutdown  
APU/HiYD Unit]
    Box4 --> Box5[One APU/HiYD  
Unit Landing  
Successful]
    Box5 --> OK3{OK}
    Box4 --> LOV1{LOV}
    Box5 --> LOV2{LOV}
```

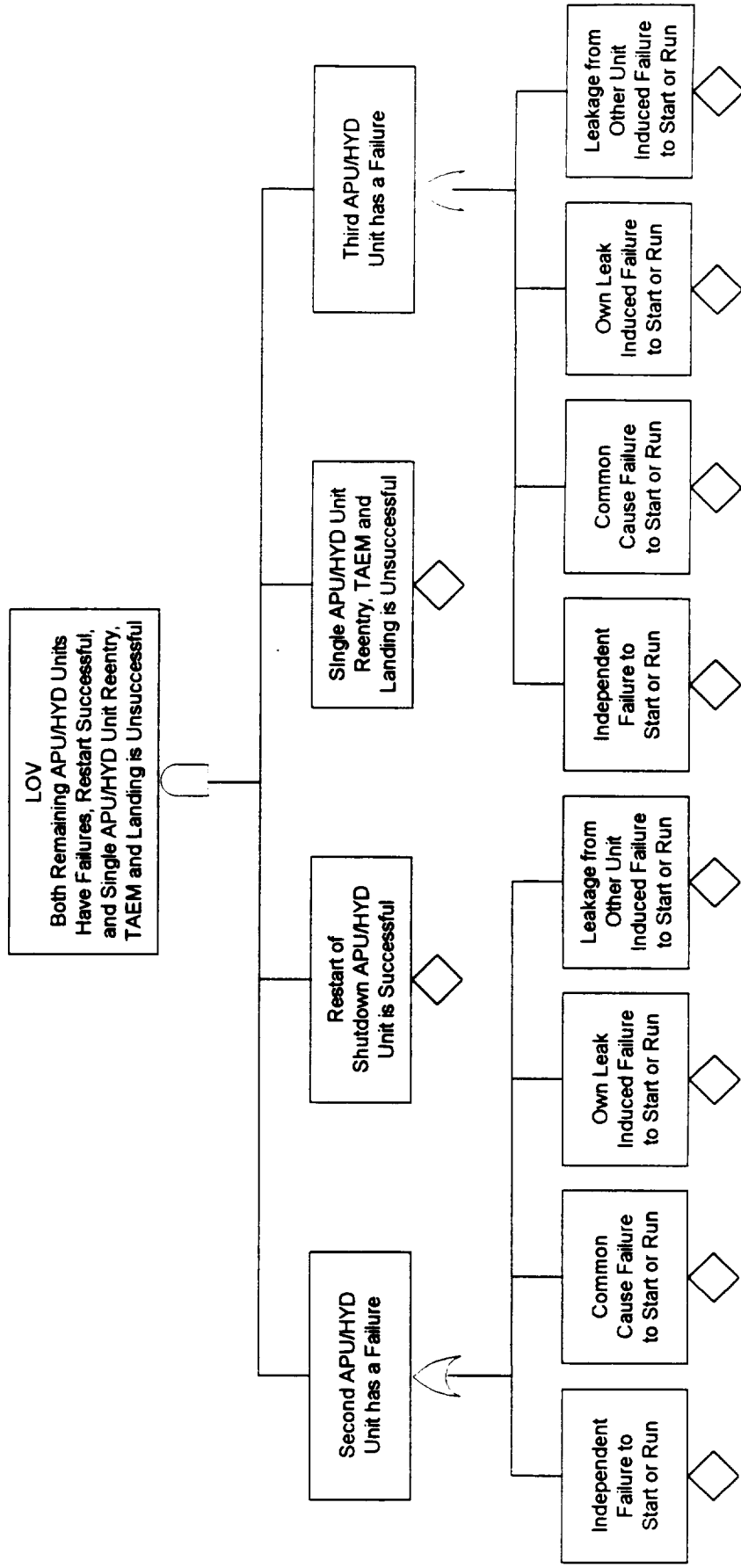
# EVENT TREE OF A PLS3R INITIATING EVENT DURING REENTRY, TAEM AND LANDING

3L	2F	3F	UR	UL	SEQUENCE NUMBER	SEQUENCE DESCRIPTION	STATE
					1	3L	OK
					2	3L2F	OK
					3	3L2FUR	OK
					4	3L2FURUL	LOV
					5	3L2F3F	OK
					6	3L2F3FUL	LOV
					7	3L2F3FUR	LOV

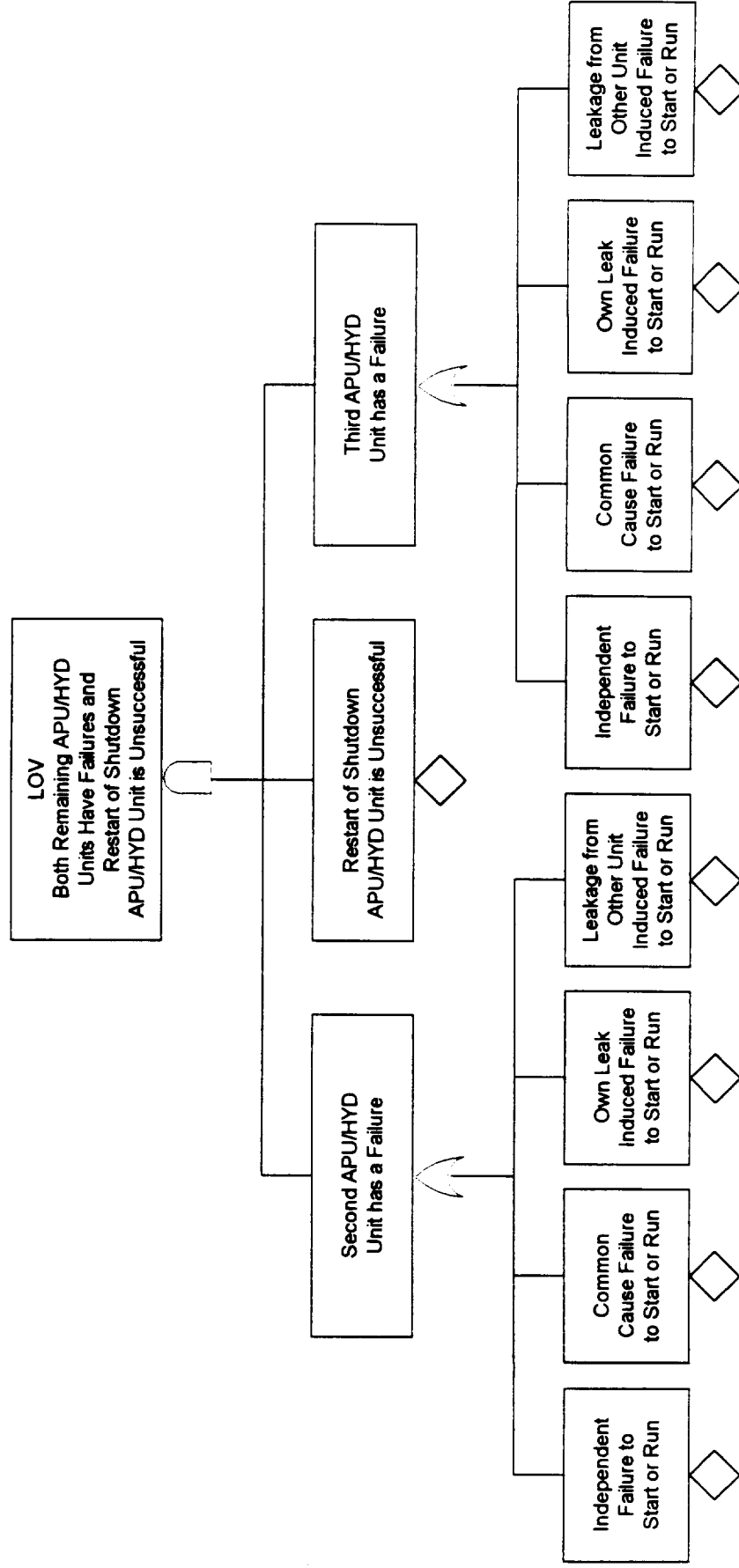
# **Fault Tree For Sequence 4 LOV State With A PLS3R Initiating Event During Reentry, TAEM and Landing**



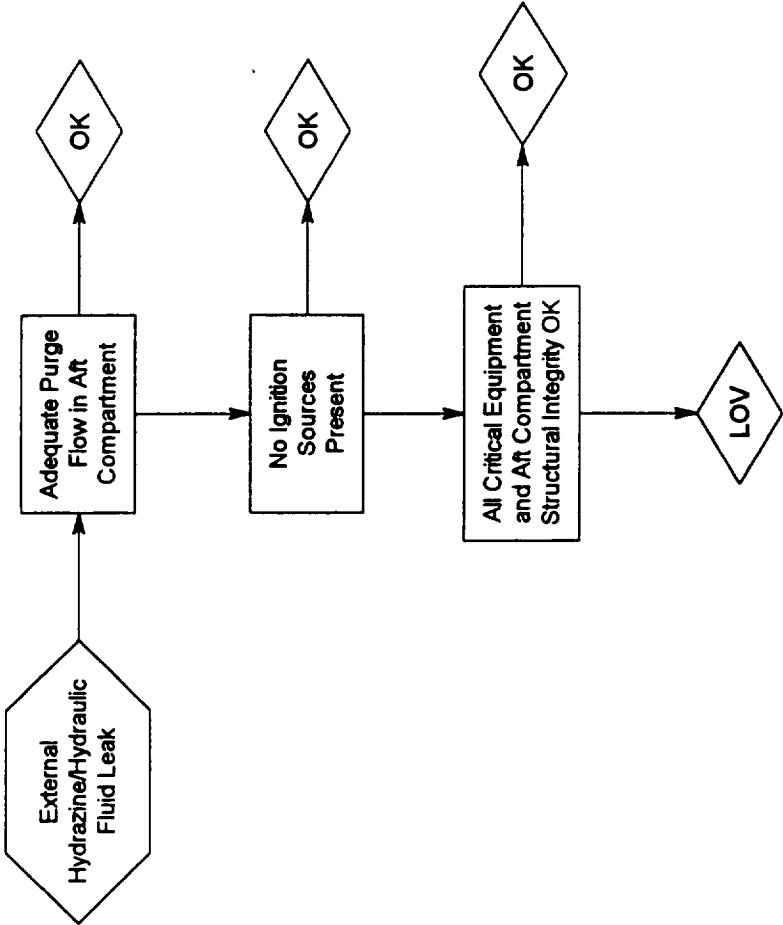
# **Fault Tree For Sequence 6 LOV State With A PLS3R Initiating Event During Reentry, TAEM and Landing**



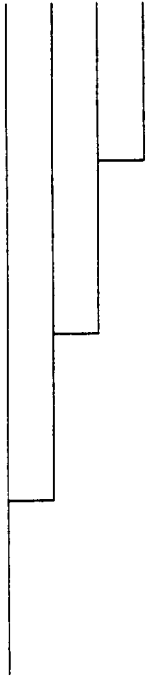
# **Fault Tree For Sequence 7 LOV State With A PLS3R Initiating Event During Reentry, TAEM and Landing**



**Event Sequence Diagram for an External  
Hydrazine or Hydraulic Fluid Leak**



# EVENT TREE OF AN EXTERNAL HYDRAZINE OR HYDRAULIC FLUID LEAK

EL	PF	IS	EI	SEQUENCE		STATE
				NUMBER	DESCRIPTION	
				1	EL	OK
				2	ELPF	OK
				3	ELPFIS	OK
				4	ELPFISEI	LOV





<p align="center"><b>ORBITER ELECTRIC POWER SYSTEM:</b>  <b>EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.</b>  *See last page for key assumptions and risk classifications.</p>					
<b>System failure</b>	<b>Failure sequence</b>	<b>Initiator or cause</b>	<b>Estimated sequence and state conditional probability/mission</b>	<b>Basis of screening conditional probability estimate</b>	<b>Risk class*</b>
<b>ELECTRIC POWER SYSTEM FUNCTIONAL FAILURE SEQUENCES:</b>					
1. No or insufficient dc power to critical systems.	1.1.1. Shrapnel, jet impingement, or pipe whip causes either reactant manifold rupture or multiple reactant system ruptures and suddenly depletes one or both reactants for 2 fuel cells.	1.1. Violent rupture of reactant tank, piping, or valve.	2E-06	1.1.1. [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-2 for severe consequential damage] = 1.7e-6/mission	Low
Same	1.1.2. Shrapnel, jet impingement, or pipe whip disables 2 of 3 main distribution or mid power controller assemblies.	Same	2E-07	1.1.2 [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-3 for severe consequential damage] = 1.7e-7/mission	Very low
Same	1.2. 2 out of 3 fuel cells fail suddenly and concurrently (complete outage or insufficient voltage).	1.2.1. Undetected pre-flight fuel cell processing error.	1E-07	1.2.1. [1e-2 for processing error]*[1e-3 for failure to detect before launch]*[1e-2 for failure progressing too fast for recovery or abort] = 1e-7/mission.	Very low
Same	Same	1.2.2. Concurrent unrecoverable loss of ECLSS freon loops 1 and 2 (disables fuel cell cooling).	2E-06	2.1.2. See note 2.	Low
Same	1.3. Severe sustained overload fails one fuel cell; crew transfers load to another cell, which also fails on overload.	1.3. Severe sustained electrical overload.	1E-08	1.3. [1e-3 for severe sustained overload]*[1e-2 for crew transferring overload to second cell]*[1e-3 for failing to notice and correct in time] = 1e-8/mission.	Negligible
Same	1.4. One (or both) fuel cell reactants is depleted before detection and isolation.	1.4.1. Severe spontaneous external leak or rupture of reactant manifold or associated valves, etc.	1E-08	1.4.1. [1e-6/hr for severe leak or rupture]* [168hrs for typical mission]* [1e-2 for failure to detect and isolate in time] = 1e-8/mission.	Negligible
Same	Same	1.4.2. Relief valve on isolated reactant manifold section spontaneously fails closed, causing overpressure and undetected rupture; isolation valve is then opened.	8E-07	1.4.2. [2e-6/hr for relief valve failure]*[168hrs for typical mission]*[0.5 for leak or rupture on overpressure]*[1e-2 for failure to detect]*[0.5 for opening isolation valve] = 8e-7/mission.	Very low

# ORBITER ELECTRIC POWER SYSTEM:

## EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.

\*See last page for key assumptions and risk classifications.

System failure	Failure sequence	Initiator or cause	Estimated sequence and state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*	Comments
Same	Same	1.4.3. Multiple reactant tank relief valves fail open due to undetected pre-flight processing or pressure set-point error.	1E-05	1.4.3. [1e-3 for processing or set-point error]*[1e-2 for failure to detect before launch] = 1e-5/mission.	Moderate	
Same	Same	1.4.4. Severe sustained electrical overload depletes reactants before detection of overload or low reactant level.	1E-10	1.4.4. [1e-3 for severe overload]*[1e-4 for failure to detect overload before reactant depletion]*[1e-3 for failure to detect depletion in time] = 1e-10/mission	Negligible	Low P(failure to detect overload) because overload this severe would cause symptoms obvious to crew.
Same	1.5. 2 of 3 fuel cells or main busses turned off and not restored.	1.5. Crew error.	1E-09	1.5. [1e-5 for turning off FCs, main busses, or essential busses]*[1e-4 for failing to notice and correct] = 1e-9/mission.	Negligible	
Same	1.6. 2 of 3 dc distribution trains fail open.	1.6.1. Undetected, unrecoverable pre-flight processing error (e.g. failure to restore after testing, RPC setpoint error) in 2	1E-06	1.6.1. [1e-3 for unrecoverable processing error]*[1e-3 for failure to detect open before launch] = 1e-6/mission	Low	
Same	Same	1.6.2. Short circuit in one train propagates to second before interruption.	1E-11	1.6.2. [4e-4 for short circuit]*[1e-2 for vulnerable components of another train being close enough to allow propagation]*[5e-6 for failure to trip in time to prevent propagation] = 1e-11/mission	Negligible	See note 3 for basis of estimate of short circuit probability. P(failure to trip)=P(CB f.t. open on command)+P(prot. relay f.t. close)
Same	Same	1.6.3. Concurrent unrelated spontaneous failures of 2 trains.	6E-07	1.6.3. [8e-4 for failure of 1st train]*[8e-4 for failure of 2nd train] = 6e-7/mission.	Very low	Same basis of estimate as 1.5.2 except all failure modes considered.
2. No or insufficient ac power to critical systems.	2.1. 2 of 3 inverter sets fail suddenly (complete outage or unacceptable voltage, frequency, or waveform).	2.1.1. Undetected pre-flight processing error.	1E-06	2.1.1. [1e-2 for processing error]*[1e-4 for failure to detect before launch] = 1e-6/mission.	Low	

ORBITER ELECTRIC POWER SYSTEM: EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE. *See last page for key assumptions and risk classifications.						
System failure	Failure sequence	Initiator or cause	Estimated sequence and state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*	Comments
Same	Same	2.1.2. Concurrent unrevocable loss of ECLSS H <sub>2</sub> O cooling loops 1 and 2 disables inverter cooling.	2E-06	2.1.2. See note 2.	Low	See note 2.
Same	2.2. Mid-deck power components of 2 or 3 trains overheat and fail.	2.2. Concurrent unrevocable loss of ECLSS freon cooling loops 1 and 2 disables mid-deck power component cooling.	2E-06	2.1.2. See note 2.	Low	See note 2.
Same	2.3. 2 of 3 inverters or ac busses turned off and not restored.	2.3. Crew error.	1E-09	2.3. [1e-5 for turning off inverters or busses]*[1e-4 for failing to notice and correct] = 1e-9/mission.	Negligible	
Same	2.4. Shrapnel, jet impingement, or pipe whip disables 2 or 3 trains of mid-deck power components.	2.4. Violent rupture of reactant tank, piping, or valve.	2E-07	2.4. [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-3 for severe consequential damage] = 1.7e-7/mission	Very low	
Same	2.5. 2 of 3 ac distribution trains fail open.	2.5.1-2.5.3. Analogous to 1.6.1-1.6.3 above.	2E-07	2.5.1-2.5.3. 1.6e-7/mission.	Very low	Estimated by analogy to 1.6.1-1.6.3 above. Note: short circuit propagation is impossible because inverters lack necessary short circuit capacity.

ORBITER ELECTRIC POWER SYSTEM: EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE. *See last page for key assumptions and risk classifications.					
System failure	Failure sequence	Initiator or cause	Estimated sequence end state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*
<b>SEQUENCES INITIATED BY ELECTRIC POWER SYSTEM</b>					
3. Electrical fire damage to other systems.	3. Electrical short circuit or component overheating initiates uncontrolled fire that unrecoverably disables other critical system(s).	3.1. Undetected pre-flight processing error.	5E-12	3.1. [1e-2 for fire-initiating processing error]*[1e-2 for failure to detect before launch]*[1e-3 for failure to trip]*[1e-3 for presence of nearby combustibles when O2 is available]*[0.5 for ignition]*[0.1 for failure of fire suppression] = 5e-12/mission	Negligible
Same	Same	3.2. Spontaneous component failure.	5E-11	3.2. [1e-3 for fire-initiating component failure]*[1e-3 for failure to trip]*[1e-3 for presence of nearby combustibles when O2 is available]*[0.5 for ignition]*[0.1 for failure of fire suppression] = 5e-11/mission	Negligible
4. Crew is disabled by fire suppression system response to electrical fire.	4. Electrical short circuit or component overheating initiates Halon flood of crew compartment; Halon exposure disables crew.	4.1. Undetected pre-flight processing error.	1E-12	4.1. [1e-2 for fire-initiating processing error]*[1e-2 for failure to detect before launch]*[1e-3 for failure to trip]*[1e-3 for crew susceptibility to Halon]*[1e-2 for failure to don breathing apparatus in time] = 1e-12/mission	Negligible
Same	Same	4.2. Spontaneous component failure.	1E-11	4.2. [1e-3 for fire-initiating component failure]*[1e-3 for failure to trip]*[1e-3 for crew susceptibility to Halon]*[1e-2 for failure to don breathing apparatus in time] = 1e-11/mission	Negligible
5. Critical systems are disabled by fire suppression system response to electrical fire.	5. Electrical short circuit or component overheating initiates Halon flood of affected compartment; presence of Halon or its decomposition products damages critical components or disables equipment cooling.	5.1. Undetected pre-flight processing error.	1E-12	5.1. [1e-2 for fire-initiating processing error]*[1e-2 for failure to detect before launch]*[1e-3 for failure to trip]*[1e-3 for crew susceptibility to low Halon concentration]*[1e-2 for failure to don breathing apparatus in time] = 1e-12/mission	Negligible

ORBITER ELECTRIC POWER SYSTEM: EVALUATION OF FAILURE MODES AND SEQUENCES POTENTIALLY SIGNIFICANT TO LOSS OF VEHICLE.					
*See last page for key assumptions and risk classifications.					
System failure	Failure sequence	Initiator or cause	Estimated sequence end state conditional probability /mission	Basis of screening conditional probability estimate	Risk class*
Same	Same	5.2. Spontaneous component failure.	1E-11	5.2. [1e-3 for fire-initiating component failure]*[1e-3 for failure to trip]*[1e-3 for crew susceptibility to Halon]*[1e-2 for failure to don breathing apparatus in time] = 1e-11/mission	Negligible
6. Orbiter structural failure.	6. Severe leak or rupture of fuel cell reactant tanks or associated piping and valves overpressurizes confined space leading to structural failure.	6. Rupture or severe external leak of tank, piping, or valve.	2E-06	6. [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-2 for severe consequential damage] = 1.7e-6/mission	Low
7. Mechanical damage to other systems.	7. Shrapnel, jet impingement, or pipe whip unrecoverably disables other nearby critical system(s).	7. Rupture or severe external leak of tank, piping, or valve.	2E-06	7. [1e-6/hr for violent rupture]*[168hrs for typical mission]*[1e-2 for severe consequential damage] = 1.7e-6/mission	Low
Total end-state conditional probabilities of all sequences listed			3E-05		

#### NOTES:

- Key assumptions: (1) probability estimates are based on IEEE Std 500-1984, IEEE Std 493-1990, and conservative (high) SAIC engineering estimates; (2) typical exposure is one-week (168-hour) mission time; (3) per PRA ground rules, only catastrophic failures leading to loss of vehicle (not abort) are considered; (4) loss of 2 of 3 power trains causes LoV.
- Concurrent ECLSS freon loop failures: zero failures in 55 flights implies mean failure frequency is 3.03e-3 per flight per loop (using 1/3 failure approximation to zero). Assume 50% of failures are common cause/common mode. Double concurrent failure frequency is therefore 4.6e-6 per flight. Assuming 50% are recoverable, unrecoverable rate is 2.3e-6.
- Estimate of probability of short circuit in distribution system: Assume each train comprises 6 equivalent circuit breakers, 1000 circuit feet of wire with 30 connections and splices, bare bars equivalent to 50 CB units. IEEE 493 App. A mean failure rates per unit/year: LV fixed CB=0.0035, LV cable=0.00141/1000ft, LV cable connection=0.000127, LV bus=0.00034 per equiv. CB unit. Assume 50% of failures are short circuits.  $P(\text{short circuit})=0.50 \cdot (168\text{hrs}/\text{mission})/(8766\text{hrs}/\text{yr})$  [6\*0.0035+1\*0.00141+30\*0.000127+50\*0.00034]=4e-4 per mission.

P(sequence end state equivalent to LoV)

#### DEFINITIONS OF RISK CLASSES:

Severe	$P > 1e-2$
Very high	$1e-3 < P < 1e-2$
High	$1e-4 < P < 1e-3$
Moderate	$1e-5 < P < 1e-4$
Low	$1e-6 < P < 1e-5$
Very low	$1e-7 < P < 1e-6$
Negligible	$P < 1e-7$